

APPENDIX A
HYDROLOGY REPORT

Table of Contents

| <u>Section</u> | <u>Page</u> |
|--|--------------------|
| A.1.0 BACKGROUND | 1 |
| A.2.0 DATA SOURCES | 3 |
| A.3.0 WATERSHED DELINEATION | 5 |
| A.3.1 Method Overview..... | 5 |
| A.3.2 Watershed Delineation, Central Region | 5 |
| A.3.3 Watershed Delineation, East Side Region..... | 6 |
| A.3.4 Watershed Delineation, Mission Valley Region | 6 |
| A.3.5 Watershed Delineation, Northeast Region | 7 |
| A.3.6 Watershed Delineation, Northwest Region | 7 |
| A.3.7 Watershed Delineation, West Central Region | 8 |
| A.4.0 CURVE NUMBER ESTIMATION..... | 9 |
| A.4.1 Method Overview..... | 9 |
| A.4.2 Curve Number Estimation, Central Region..... | 10 |
| A.4.3 Curve Number Estimation, East Side Region..... | 10 |
| A.4.4 Curve Number Estimation, Mission Valley Region | 10 |
| A.4.5 Curve Number Estimation, Northeast Region..... | 10 |
| A.4.6 Curve Number Estimation, Northwest Region | 10 |
| A.4.7 Curve Number Estimation, West Central Region | 11 |
| A.5.0 LAG TIME ESTIMATION | 13 |
| A.5.1 Method Overview..... | 13 |
| A.5.2 Lag Time Estimation, Central Region | 13 |
| A.5.3 Lag Time Estimation, East Side Region | 14 |
| A.5.4 Lag Time Estimation, Mission Valley Region..... | 14 |
| A.5.5 Lag Time Estimation, Northeast Region | 14 |
| A.5.6 Lag Time Estimation, Northwest Region | 14 |
| A.5.7 Lag Time Estimation, West Central Region..... | 14 |
| A.6.0 HYDROLOGIC ROUTING | 15 |
| A.6.1 Method Overview..... | 15 |
| A.6.2 Hydrologic Routing, Central Region | 15 |
| A.6.3 Hydrologic Routing, East Side Region..... | 16 |
| A.6.4 Hydrologic Routing, Mission Valley Region | 16 |
| A.6.5 Hydrologic Routing, Northeast Region | 16 |
| A.6.6 Hydrologic Routing, Northwest Region..... | 16 |
| A.6.7 Hydrologic Routing, West Central Region | 17 |
| A.7.0 MODELING OF SIGNIFICANT DETENTION STRUCTURES | 19 |
| A.7.1 Method Overview..... | 19 |

| | | |
|--------|---|----|
| A.7.2 | Significant Detention Structures, Central Region | 19 |
| A.7.3 | Significant Detention Structures, East Side Region..... | 34 |
| A.7.4 | Significant Detention Structures, Mission Valley Region | 35 |
| A.7.5 | Significant Detention Structures, Northeast Region | 39 |
| A.7.6 | Significant Detention Structures, Northwest Region | 44 |
| A.7.7 | Significant Detention Structures, West Central Region | 46 |
| A.8.0 | MODELING OF SMALL PONDS | 47 |
| A.8.1 | Method Overview..... | 47 |
| A.8.2 | Small Ponds, Central Region | 47 |
| A.8.3 | Small Ponds, East Side Region..... | 48 |
| A.8.4 | Small Ponds, Mission Valley Region | 48 |
| A.8.5 | Small Ponds, Northeast Region | 48 |
| A.8.6 | Small Ponds, Northwest Region | 48 |
| A.8.7 | Small Ponds, West Central Region | 49 |
| A.9.0 | ESTIMATION OF RAINFALL..... | 51 |
| A.10.0 | ASSEMBLY OF HYDROLOGIC MODELS | 53 |
| A.10.1 | Method Overview..... | 53 |
| A.10.2 | Hydrologic Model, Central Region | 53 |
| A.10.3 | Hydrologic Model, East Side Region | 55 |
| A.10.4 | Hydrologic Model, Mission Valley Region..... | 57 |
| A.10.5 | Hydrologic Model, Northeast Region | 59 |
| A.10.6 | Hydrologic Model, Northwest Region | 60 |
| A.10.7 | Hydrologic Model, West Central Region | 60 |
| A.11.0 | MODEL RESULTS | 61 |

LIST OF TABLES

| | | |
|------------|--|----|
| Table A-1 | Data Sources Utilized in Hydrologic Analysis | 65 |
| Table A-2 | Hydrologic Soil Groups in the El Paso Region..... | 66 |
| Table A-3 | Runoff Curve Numbers for Urban Areas | 67 |
| Table A-4 | Runoff Curve Numbers for Arid and Semi Arid Rangelands | 67 |
| Table A-5 | Land Use Categories for Urban Areas..... | 68 |
| Table A-6 | Land Use Categories for Rural Areas | 68 |
| Table A-7 | Curve Number Summary for the Central Region | 69 |
| Table A-8 | Curve Number Summary for the East Side Region | 71 |
| Table A-9 | Curve Number Summary for the Mission Valley Region | 73 |
| Table A-10 | Curve Number Summary for the Northeast Region | 75 |
| Table A-11 | Curve Number Summary for the Northwest Region..... | 77 |
| Table A-12 | Curve Number Summary for the West Central Region | 79 |
| Table A-13 | Summary of Lag Times for the Central Region..... | 81 |

| | | |
|-------------|--|-----|
| Table A-14 | Summary of Lag Times for the East Side Region | 85 |
| Table A-15 | Summary of Lag Times for the Mission Valley Region..... | 87 |
| Table A-16 | Summary of Lag Times for the Northeast Region | 89 |
| Table A-17 | Summary of Lag Times for the Northwest Region | 91 |
| Table A-18 | Summary of Lag Times for the West Central Region..... | 95 |
| Table A-19a | Muskingum-Cunge Routing Inputs for the Central Region..... | 97 |
| Table A-19b | Lag Routing Inputs for the Central Region..... | 99 |
| Table A-20a | Kinematic Wave Routing Inputs for the East Side Region | 101 |
| Table A-20b | Kinematic Wave Routing Inputs (Conduits) for the East Side Region.... | 101 |
| Table A-21a | Muskingum-Cunge Routing Inputs for the Mission Valley Region | 103 |
| Table A-21b | Lag Routing Inputs for the Mission Valley Region | 105 |
| Table A-22a | Muskingum-Cunge Routing Inputs for the Northeast Region..... | 107 |
| Table A-22b | Lag Routing Inputs for Northeast Region..... | 111 |
| Table A-23 | Routing Inputs for the Northwest Region | 113 |
| Table A-24 | Routing Inputs for the West Central Region..... | 119 |
| Table A-25 | Adjusted Curve Numbers for the Central Region..... | 121 |
| Table A-26 | Adjusted Curve Numbers for the East Side Region | 121 |
| Table A-27 | Adjusted Curve Numbers for the Mission Valley Region..... | 121 |
| Table A-28 | Adjusted Curve Numbers for the Northeast Region | 122 |
| Table A-29 | Adjusted Curve Numbers for the Northwest Region | 122 |
| Table A-30 | Adjusted Curve Numbers for the West Central Region..... | 122 |
| Table A-31 | Estimation of Rainfall Depth by Annual Exceedance Probability | 123 |
| Table A-32 | Central Region Complete HEC-HMS Results for 10 - 100-Year Storms | 125 |
| Table A-33 | East Side Region Complete HEC-HMS Results for 10 - 100-Year Storms | 129 |
| Table A-34 | Mission Valley Region Complete HEC-HMS Results for 10 - 100- Year Storms..... | 133 |
| Table A-35 | Northeast Region Complete HEC-HMS Results for 10 - 100-Year Storms | 137 |
| Table A-36 | Northwest Region Complete HEC-HMS Results for 10 - 100-Year Storms | 141 |
| Table A-37 | West Central Region Complete HEC-HMS Results for 10 - 100-Year Storms | 145 |

LIST OF FIGURES

| | | |
|------------|---|-----|
| Figure A-1 | Project Area | 149 |
| Figure A-2 | Watershed Delineation - Central Region..... | 150 |
| Figure A-3 | Watershed Delineation - East Side Region..... | 151 |
| Figure A-4 | Watershed Delineation - Mission Valley Region | 152 |
| Figure A-5 | Watershed Delineation - Northeast Region..... | 153 |
| Figure A-6 | Watershed Delineation - Northwest Region | 154 |
| Figure A-7 | Watershed Delineation - West Central Region | 155 |

| | | |
|-------------|--|-----|
| Figure A-8 | Hydrologic Soil Groups Map - Central Region | 156 |
| Figure A-9 | Land Use Map - Central Region | 157 |
| Figure A-10 | Hydrologic Soil Groups Map - East Side Region | 158 |
| Figure A-11 | Land Use Map - East Side Region..... | 159 |
| Figure A-12 | Hydrologic Soil Groups Map - Mission Valley Region..... | 160 |
| Figure A-13 | Land Use Map - Mission Valley Region | 161 |
| Figure A-14 | Hydrologic Soil Groups Map - Northeast Region | 162 |
| Figure A-15 | Land Use Map - Northeast Region | 163 |
| Figure A-16 | Hydrologic Soil Groups Map - Northwest Region..... | 164 |
| Figure A-17 | Land Use Map - Northwest Region..... | 165 |
| Figure A-18 | Hydrologic Soil Groups Map - West Central Region | 166 |
| Figure A-19 | Land Use Map - West Central Region | 167 |
| Figure A-20 | Longest Flowpaths - Central Region..... | 168 |
| Figure A-21 | Longest Flowpaths - East Side Region..... | 169 |
| Figure A-22 | Longest Flowpaths - Mission Valley Region | 170 |
| Figure A-23 | Longest Flowpaths - Northeast Region..... | 171 |
| Figure A-24 | Longest Flowpaths - Northwest Region | 172 |
| Figure A-25 | Longest Flowpaths - West Central Region..... | 173 |
| Figure A-26 | Routing Reaches - Central Region | 174 |
| Figure A-27 | Routing Reaches - East Side Region | 175 |
| Figure A-28 | Routing Reaches - Mission Valley Region..... | 176 |
| Figure A-29 | Routing Reaches - Northeast Region | 177 |
| Figure A-30 | Routing Reaches - Northwest Region..... | 178 |
| Figure A-31 | Routing Reaches - West Central Region | 179 |
| Figure A-32 | Location Map - Modeled Detention Structures..... | 180 |
| Figure A-33 | Location Map - Small Ponds | 181 |
| Figure A-34 | Government Hills System - HEC-HMS Model Layout - Central Region | 182 |
| Figure A-35 | Government Hills System - HEC-HMS Model Table - Central Region... | 183 |
| Figure A-36 | Cebada System - HEC-HMS Model Layout - Central Region | 184 |
| Figure A-37 | Cebada System - HEC-HMS Model Table - Central Region..... | 185 |
| Figure A-38 | Dallas System - HEC-HMS Model Layout - Central Region..... | 186 |
| Figure A-39 | Dallas System - HEC-HMS Model Table - Central Region | 187 |
| Figure A-40 | Modesto, Channel 108, and Paisano Systems - HEC-HMS Model Layout - Central Region | 188 |
| Figure A-41 | Modesto, Channel 108, and Paisano Systems - HEC-HMS Model Table - Central Region..... | 189 |
| Figure A-42 | HEC-HMS Model Layout - East Side Region..... | 190 |
| Figure A-43 | HEC-HMS Model Layout for Referenced Study - East Side Region | 191 |
| Figure A-44 | High Mesa (Closed Basins) - HEC-HMS Model Layout - East Side Region | 192 |
| Figure A-45 | High Mesa (Closed Basins) - HEC-HMS Model Table - East Side Region | 193 |
| Figure A-46 | HEC-HMS Model Layout - Mission Valley Region | 194 |
| Figure A-47 | HEC-HMS Model Table - Mission Valley Region | 195 |

| | | |
|-------------|---|-----|
| Figure A-48 | HEC-HMS Model Layout - Northeast Region..... | 196 |
| Figure A-49 | HEC-HMS Model Table - Northeast Region | 197 |
| Figure A-50 | Doniphan & Montoya Drain Systems - HEC-HMS Model Layout & Table - Northwest Region | 198 |
| Figure A-51 | Enchanted Hills System - HEC-HMS Model Layout & Table - Northwest Region | 199 |
| Figure A-52 | Flow Paths System - HEC-HMS Model Layout & Table - Northwest Region | 200 |
| Figure A-53 | Keystone Dam System - HEC-HMS Model Layout - Northwest Region | 201 |
| Figure A-54 | Keystone Dam System - HEC-HMS Model Table - Northwest Region .. | 202 |
| Figure A-55 | Oxidation Dam System - HEC-HMS Model Layout & Table - Northwest Region | 203 |
| Figure A-56 | West Central System - HEC-HMS Model Layout & Table - West Central Region..... | 204 |

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A.1.0 BACKGROUND

A hydrologic analysis was performed for each of the six study regions to estimate peak storm flows that would occur for extreme storm events. The analysis consisted of the following steps:

- Watersheds boundaries were delineated;
- Curve Numbers were estimated for each watershed;
- Lag Times were estimated for each watershed;
- Routing parameters were estimated for each flowpath;
- Large detention structures were analyzed;
- The effect of small ponds was analyzed;
- Precipitation was estimated; and
- Hydrologic models were developed for each study area.

Detailed descriptions of the steps, assumptions, and results of the analysis are presented in this Appendix. Summaries of pertinent data, calculations, tables, and figures are located at the end of this Appendix. An overview of the project area is provided on Figure A-1.

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A.2.0 DATA SOURCES

Table A-1 lists the sources used in the hydrologic analysis, as well as the specific calculation(s) each source was used for.

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A.3.0 WATERSHED DELINEATION

A.3.1 Method Overview

Watershed boundaries were delineated for much of the Stormwater Master Plan (SMP) study area as part of the *Drainage On-Call Services, Work Order 1: Drainage System Evaluation and Audit* (URS Corporation [URS], 2007), and the *Drainage On-Call Services, Work Order 3: Dam Analysis Report* (URS, 2008). These watershed delineations were utilized where available and modified as appropriate to correspond to the scope of the SMP.

The purpose of the SMP is to develop projects to improve the performance of the El Paso Drainage Infrastructure in flood events up to the 100-year event. To accomplish this task, the Work Order 1 and Work Order 3 watersheds were modified to estimate the peak flows at the downstream end of each El Paso Water Utilities (EPWU) identified reach. For “Priority Reaches” identified in the SMP, Task 2: Regional Analysis Staging/Prioritization, additional watersheds were delineated at locations of significant changes in channel slope or channel bottom width or at confluence points. For the purposes of identifying significant changes in channel geometry, channel dimensions were obtained from a variety of sources including the Work Order 1 Study, the EPWU drainage shapefile, and site visits.

SMP watershed delineations and modifications were digitized utilizing ArcView, Version 9.2, based on 3-foot contours generated from 2004 Texas Department of Transportation (TxDOT) topography. In addition to the contours, the City of El Paso Engineering Department Flood Control System Base Maps (City of El Paso, 1987) were utilized to identify flowpaths along drainage infrastructure. Each watershed polygon was assigned a unique name based on the downstream element or primary flowpath. Successive watersheds for the same element were labeled with a number at the end of the name. For example, the watershed contributing to Range Dam was labeled as A_Range Dam, which denotes that it is the area tributary to Range Dam. If there were two watersheds contributing to Range Dam, then they would be named A_Range Dam_1 and A_Range Dam_2.

A.3.2 Watershed Delineation, Central Region

Many of the watersheds in the Central Region were previously delineated in Work Order 3. Five of the watersheds delineated in Work Order 3 were subdivided into smaller watersheds or modified to incorporate flows that result from the 10-, 25-, 50-, and 100-year storms, as opposed to the probable maximum flood (PMF), which is what was analyzed in Work Order 3. The remaining watersheds in the Central Region were delineated based on 3-foot contours generated from TxDOT topography, drainage inlet locations, storm sewers, channels, and site investigations.

South of Interstate Highway 10 (IH-10), the Central Region is very flat and the land use is primarily urban, making the storm sewers and drainage inlets the primary factors when determining watershed boundaries. All watersheds were checked using boundaries delineated in the S_HydroBasin_CoEP.shp file, which was generated during Work Order 1. Previous reports, such as the *Dallas St. Pump and Drainage System Preliminary Engineering Report* by Moreno Cardenas Inc. (MCi) (MCi, 2007), were also used to assist with the watershed delineations south of IH-10. Figure A-2 shows the final watershed delineations for the Central Region.

A.3.3 Watershed Delineation, East Side Region

The watershed delineation completed for Work Order 1 was analyzed further for the purposes of this master plan. Areas within the City limits were analyzed at the subdivision level, bringing their individual ponding areas into consideration and identifying areas built within a closed basin, in turn, breaking up the Work Order 1 watersheds. In areas where it was unclear where flows were concentrated because of existing structures and very flat terrain on the high Mesa, field visits were conducted and photos were taken. Site visits were useful in getting existing drainage condition information. Each basin system polygon was assigned a unique name based on the stream element at the south end of the system. Each watershed was then named based on the basin system it was within followed by a number. The numbers progress from smallest to largest from north to south. For example, the watershed at the farthest north within the Lomaland Basin System is labeled as A_Lomaland_0. Figure A-3 shows a map of the project watersheds within the East Region.

A.3.4 Watershed Delineation, Mission Valley Region

Only Work Order 1 watersheds were significantly modified for the Mission Valley study area, as the previous Work Order 3 scope did not include this region of El Paso. Also, watersheds delineated for the 2007 North Loop Study (MCi, 2007) were utilized in this analysis. The hydrologic approach for Mission Valley differed from the other five areas due to the flat terrain below the escarpment zone in the lower valley region and the resulting local flooding issues. The approach taken for Mission Valley was to focus on large-scale problems and appropriate solutions for handling the total volume of water generated by the various storms, but most importantly the 100-year event. The main problems addressed were increasing the capacity of the interceptor system and reversing the negative slope to the Basin G pump station to alleviate local flooding issues upstream. Therefore, the hydrologic analysis was performed using large-scale watersheds below the major dams to capture the flow into the three main drains (Mesa, Middle, and Franklin Drains), the interceptor channels, as well as Basin G. The advantage of using these larger watersheds is that the need for detailed delineation to capture, for instance, the presence of stormwater pipes crossing or emptying to the main drains is eliminated. This simplifying model approach was taken to reduce the complexity of the model while still obtaining valuable flow information to analyze Mesa, Middle, Franklin, and Playa Drains. Figure A-4 shows the watershed delineations for

the Mission Valley study area. The TxDOT topography, City of El Paso *Engineering Department Flood Control System Base Map* (City of El Paso, 1987), and ArcView, Version 9.2 discussed above were utilized for delineating Mission Valley Watersheds. Additionally, the naming convention described above for watersheds was utilized.

A.3.5 Watershed Delineation, Northeast Region

Watershed delineations in the Northeast Region were originally taken from the Work Order 3 Study, but were modified in a number of areas due to the assumptions used in the Work Order 3 Hydrology. Work Order 3 involved modeling to analyze the dams to Texas Commission on Environmental Quality (TCEQ) standards, which include passing the PMF, a storm much larger than the 500-year frequency storm. This study is concerned with more frequent floods, and targets the 100-year storm. Assumptions made during the Work Order 3 modeling included assuming that all local drainage infrastructure in the Northeast Region would likely be overwhelmed due to the extremely high PMF flows, and flowpaths would travel over land based on topography and not be conveyed along the channels in the area. Watersheds were modified as part of the SMP analysis where deemed appropriate to more accurately model the flooding scenarios and flowpaths that would occur in more frequent floods. Additionally, watersheds were further subdivided to estimate flows at all of the priority channels and critical features identified in meetings with the EPWU. Figure A-5 shows the watershed delineations for the Northeast Region.

A.3.6 Watershed Delineation, Northwest Region

Where available, watershed delineations from Work Orders 1 and 3 were used for the Northwest Region. The existing delineations were modified as necessary to cover the differences in study areas and limits. The watershed modifications and new watershed delineations were delineated by hand using the 3-foot contour data from TxDOT topography and available orthophotography.

The watershed for the Nemexas Drain only includes the area that will have an effect on the politically defined areas of the City of El Paso in its route to the drain, i.e. the area east of the Rio Grande. The watershed crosses the state boundary of New Mexico and Texas. In order to delineate the watershed outside the City of El Paso, topography data of Doña Ana County, New Mexico was used. The whole Nemexas Drain Watershed is not included in this analysis. It was assumed that backwater pressure from flood waters east of the Rio Grande would effectively block excess flow from the siphon crossing of the Rio Grande. The excess flow would be discharged to the Rio Grande via the overflow weir structure on the west banks of the Rio Grande.

The watersheds that were used for the “Vinton” Channels were delineated as part of the Federal Emergency Management Agency (FEMA) update and analysis of the Flood Insurance Rate Maps (FIRMs) and Flood Insurance Study (FIS) for El Paso County.

These watersheds were not modified. Figure A-6 shows the watershed delineations for the Northwest Region.

A.3.7 Watershed Delineation, West Central Region

The West Central Region Watersheds were delineated primarily by hand. The watershed delineation was based on the 3-foot contour data from TxDOT topography and available orthophotography. Watersheds from Work Orders 1 and 3 covered only a portion of a few channels. Those watersheds were modified as needed to cover the entire channel. The watersheds were delineated assuming that the runoff remains within that watershed and is not diverted. Figure A-7 shows the watershed delineations for the West Central Region.

A.4.0 CURVE NUMBER ESTIMATION

A.4.1 Method Overview

Runoff losses were modeled in Hydrologic Engineering Center's Hydraulic Modeling System (HEC-HMS) by selecting the Soil Conservation Service (SCS) Curve Number Loss Method. This method requires the user to input the SCS Curve Number, Percent Impervious Cover, and Initial Abstraction. SCS Type II Curve Numbers were assigned based on the combination of hydrologic soil groups (HSGs) and land use cover description according to the El Paso Drainage Design Manual (DDM), Tables 4-9 and 4-10 (City of El Paso, 2008); which is summarized in Tables A-3 and A-4.

When entering the curve number parameters into the HEC-HMS Model, the percent impervious cover was left as 0 percent (%) because it is already accounted for in the Curve Number Calculation Method described below. The initial abstraction parameter defines the amount of rainfall that must fall before surface runoff occurs. This value was left blank, and by default, HEC-HMS calculates it as 0.2 times the potential retention.

HSGs were determined using the soil type shapefile for El Paso County available from the Soil Survey Geographic Database (SSURGO) (United States Department of Agriculture [USDA], 2004). The SSURGO soil shapefile delineates soil according to soil types, which were correlated to HSG based on a key code also available from SSURGO, summarized in Table A-2. Soils were classified as Soil Group A, B, C, D, Water, or Sink. Sinks are areas such as landfills or quarries that collect water and are thus not included in runoff calculations.

Land use types were estimated using 2006 Orthophotography (City of El Paso, 2006) and hand delineated in ArcMap. Polygons were digitized according to the land use cover categories provided in the DDM. Each polygon was assigned a Land Use Cover Type text attribute and a Land Use Identification (ID) numerical attribute corresponding to Tables A-5 and A-6 at the end of this Appendix.

A curve number shapefile was created by combining the land use and soils shapefiles using the ArcMap Union tool. The curve number shapefile contained both the HSG and Land Use ID for each polygon. Curve numbers were then assigned according to the DDM for each soil group-land use combination. Finally, a union was created between the curve number shapefile and the watershed boundary shapefile, and the area-weighted average curve number for each watershed was calculated using the following equation:

$$CN_{avg} = \frac{\sum Area \times CN}{\sum Area \text{ Sum}}$$

A.4.2 Curve Number Estimation, Central Region

Results for the Central Region curve number estimation are given in Table A-7. A map of soil types is provided on Figure A-8, and a map showing Land Use categories delineated is provided on Figure A-9, found at the end of this Appendix.

A.4.3 Curve Number Estimation, East Side Region

Land use types were estimated using 2006 Orthophotography and delineated in ArcMap. With the delineated polygons in ArcMap and site visit analysis, land use cover types and hydrologic conditions were assigned to areas throughout the East Side Region study area. Using information gathered above, and Tables A-3 and A-4, curve numbers were assigned to each respective area. Table A-4 was used for undeveloped desert shrub areas surrounding the urbanized East Side Region. Table A-3 was used for curve numbers for developed areas, i.e. residential ¼-acre lot, commercial, industrial, and open space. Based on site visits, residential ¼-acre lot was used. The site visits were also referenced when assigning a curve number to open space and easements based on vegetation cover. A map of soil types is provided on Figure A-10, and a map showing Land Use categories delineated is provided on Figure A-11.

A.4.4 Curve Number Estimation, Mission Valley Region

Results for the Mission Valley Region curve number estimation are given in Table A-9. A map of soil types is provided on Figure A-12, and a map showing Land Use categories delineated is provided on Figure A-13, found at the end of this Appendix.

A.4.5 Curve Number Estimation, Northeast Region

Results for the Northeast Region curve number estimation are given in Table A-10. A map of soil types is provided on Figure A-14, and a map showing Land Use categories delineated is provided on Figure A-15, found at the end of this Appendix.

A.4.6 Curve Number Estimation, Northwest Region

The curve number estimation for the Northwest Region was found using the process described above, where the appropriate data were available. As mentioned in the watershed delineation section, the Nemexas Drain Watershed crosses the state boundary between New Mexico and Texas. The only data used to determine the curve number that was affected by this is the Soil Type shapefile. The Soil Type shapefile used for the area of Doña Ana County is from the National Resources Conservation Service (NRCS) in Geographic Information Systems (GIS) format. The "Vinton" channels were not included in this process because the hydrology was already completed by the FEMA update and analysis of the FIRMs and FIS for El Paso County.

Results for the Northwest Region curve number estimation are given in Table A-11. A map of soil types is provided on Figure A-16, and a map showing Land Use categories delineated is provided on Figure A-17, found at the end of this Appendix.

A.4.7 Curve Number Estimation, West Central Region

Results for the West Central Region curve number estimation are given in Table A-12. A map of soil types is provided on Figure A-18, and a map showing Land Use categories delineated is provided on Figure A-19, found at the end of this Appendix.

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A.5.0 LAG TIME ESTIMATION

A.5.1 Method Overview

The lag time was calculated for each modeled watershed using the modified Snyder Method developed for the FIS for Northeast and Central El Paso conducted by US Army Corp of Engineers (USACE) in 1978 (USACE, February 1978). The methodology for the Snyder calculation is shown below:

$$T_{lag} = C_T (L_L * L_{CA})^{0.3}$$

where: T_{lag} = Lag Time (hrs);
 C_T = Regional Coefficient (Plate A-3, USACE, February 1978);
 L_L = Length of longest flow path (mi);
 L_{CA} = Length from longest flow path centroid to outlet of watershed (mi).

The regional coefficient, C_T , was estimated according to equivalent slope based on the curves for undeveloped areas and urban areas found in Plate A3 of the USACE 1978 Report (USACE, February 1978). Equivalent slope was assumed to be the slope between the 10% and 85% marker elevations, traveling upstream along the longest flow path.

The Snyder peaking coefficient, c_p , was defined according to the following guidelines:

$$640c_p = 430 \text{ if } slope\left(\frac{ft}{ft}\right) < 0.015$$

$$640c_p = 392 \text{ if } slope\left(\frac{ft}{ft}\right) > 0.015$$

The longest flowpath was digitized by referencing 2004 TxDOT Contours (TxDOT, 2004). A polyline was created in ArcMap connecting the furthest upstream point in the watershed to the watershed outlet, while following a path of decreasing elevation. Physical barriers that were visible in the 2006 Orthophotography (City of El Paso, 2006) were taken into account while estimating the longest flow path for each watershed.

A.5.2 Lag Time Estimation, Central Region

Lag Times for the Central Region were estimated using the method above and are summarized in Table A-13. Longest flowpaths for the Central are shown on Figure A-20 located at the end of this Appendix.

A.5.3 Lag Time Estimation, East Side Region

Lag Times for the East Side Region were estimated using the method described above and are summarized in Table A-14. Longest flowpaths for the East Side Region are shown on Figure A-21 located at the end of this Appendix.

A.5.4 Lag Time Estimation, Mission Valley Region

Lag Times for the Mission Valley Region were estimated using the method described above and are summarized in Table A-15. Longest flowpaths for the Mission Valley Regions are shown on Figure A-22 located at the end of this Appendix.

A.5.5 Lag Time Estimation, Northeast Region

Lag Times for the Northeast Region were estimated using the method described above and are summarized in Table A-16. Longest flowpaths for the Northeast Region are shown on Figure A-23 located at the end of this Appendix.

A.5.6 Lag Time Estimation, Northwest Region

Lag Times for the Northwest Region were estimated using the method described above and are summarized in Table A-17. Longest flow paths for the Northwest Region are shown on Figure A-24 located at the end of this Appendix. The “Vinton” Channels were not included in this estimation because the hydrology used was taken from the FEMA update and analysis of the FIRMs and FIS for El Paso County.

A.5.7 Lag Time Estimation, West Central Region

Lag Times for the West Central Region were estimated using the method described above and are summarized in Table A-18. Longest flow paths for the West Central Region are shown on Figure A-25 located at the end of this Appendix.

A.6.0 HYDROLOGIC ROUTING

A.6.1 Method Overview

Once watershed delineations were completed, flowpaths were identified and the HEC-HMS model was constructed. A routing shapefile was digitized in ArcView containing the reaches corresponding to the HEC-HMS Model. When generating the routing schematic, the assumption was made that flow would be conveyed along the drainage infrastructure and would not be diverted due to insufficient capacity and overtopping. The HEC-HMS Muskingum-Cunge Method of routing was selected for all open channel reaches. In this method, the user first enters the channel shape. If “trapezoid” is selected, the user enters a channel slope, and Manning’s Roughness Coefficient and channel bottom width. If “eight point” is selected, then the X-Y coordinates for the channel cross-section are entered into the paired-data editor, along with the Manning’s Roughness Coefficient.

For routing through conduits, either the Muskingum-Cunge Method or the Lag Method of Routing was used. The Muskingum-Cunge Method is suitable for representing a free water surface inside a pipe, and should not be used for pressure flow or pipe networks. For pressure flow or other conduit scenarios, the Lag Method was used, where lag was calculated based on conduit length and estimated velocity.

Several data sources were available for the estimation of cross-section geometry. The first source utilized was the Bentley FlowMaster Reports included in the Work Order 1 Report (URS, 2008). In some cases, a corresponding Work Order 1 cross-section could not be located for the routing segment modeled in HEC-HMS, or the Work Order 1 geometry did not match other data sources. In these cases, the EPWU drainage feature shapefiles (EPWU, 2008) were examined to see if geometry could be found for the reach in question. If not, the TxDOT 2004 Topography (TxDOT, 2004) was used to approximate a simple eight-point cross-section or a field visit was performed. In several instances, water is routed through City streets. In such cases, the cross-section used for routing purposes is that of a street itself.

A.6.2 Hydrologic Routing, Central Region

The routing for open channels in the Central Region Watershed was estimated using the method described above. In addition to open channel routing, 29 conduits were modeled in HEC-HMS using the Lag Method. For 15 of these conduits, the conduit length was divided by an assumed velocity in order to estimate a routing lag time. The velocities were only assumed if they were not available in Work Order 1 or if the velocities provided in Work Order 1 seemed unreasonable. If Work Order 1 provided multiple velocities for different sections of the same conduit, then lag times were calculated based on the length of each section and added together to determine the total lag time for the conduit. Channel Routing Inputs for the Central Region are

provided in Table A-19a and Conduit Routing Inputs for the Central Region are provided in Table A-19b. Figure A-26 shows the routing reaches for the Central Region.

A.6.3 Hydrologic Routing, East Side Region

The routing for open channels in the East Side Region Watershed was estimated using the Kinematic Wave Method. In addition to open channel routing, several conduit routing pathways under IH-10 were modeled in HEC-HMS using the Lag Method. For these conduits, an estimated velocity was multiplied by the conduit length in order to estimate a routing lag time. The lag times across IH-10 were rounded and entered into HEC-HMS as one minute. Figure A-27 shows the routing reaches for the East Side Region.

A.6.4 Hydrologic Routing, Mission Valley Region

Routing for the Mission Valley Region open channels was estimated using the method described above. In addition to open channel routing, two conduit routing pathways were modeled in HEC-HMS using the Lag Method. For these conduits, the conduit length was divided by an estimated velocity to estimate a routing lag time. Channel routing inputs for Mission Valley are provided in Table A-21a and Conduit routing inputs for Mission Valley are provided in Table A-21b. Figure A-28 shows the routing reaches for the Mission Valley Region.

A.6.5 Hydrologic Routing, Northeast Region

Routing for the Northeast Region open channels was estimated using the method described above. In addition to open channel routing, three conduit routing pathways were modeled in HEC-HMS using the Lag Method. For these conduits, the conduit length was divided by an estimated velocity to estimate a routing lag time. Velocity estimates were obtained from Work Order 1. Channel routing inputs for the Northeast are provided in Table A-22a and Conduit routing inputs for Northeast are provided in Table A-22b. Figure A-29 shows the routing reaches for the Northeast Region.

A.6.6 Hydrologic Routing, Northwest Region

Routing for the Northwest region open channels was estimated using the method described above. Channel routing inputs for the Northwest Region are provided in Table A-23. The "Vinton" Channels were not included in this process because the hydrology was completed with the FEMA update and analysis of the FIRMs and FIS for El Paso County. Figure A-30 shows the routing reaches for the Northwest Region.

A.6.7 Hydrologic Routing, West Central Region

Routing for the West Central Region open channels was estimated using the method described above. Channel routing inputs for the West Central Region are provided in Table A-24. Figure A-31 shows the routing reaches for the Northwest Region.

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A.7.0 MODELING OF SIGNIFICANT DETENTION STRUCTURES

A.7.1 Method Overview

Significant detention structures were modeled in HEC-HMS using one of two methods. Either a stage-storage-discharge relationship was entered into the HEC-HMS model, or the dam was modeled using the Outflow Structures method.

A stage-storage-discharge relationship was developed previously for each dam modeled in Work Order 3 (URS, 2008), and utilized in this study when available. This relationship dictated how upstream flow was attenuated by reservoirs and associated dam structures. The relationship consists of a stage elevation versus a storage volume versus a dam discharge, starting at the bottom elevation of the dam's storage reservoir and increasing to the top elevation of the dam embankment. This relationship is defined by the components of the dam, its storage basin, its embankment size and height, and its outflow structures.

For dams that did not have a stage-storage-discharge curve developed, the Outflow Structures method was used. When using the Outflow Structures method, information is entered into the HEC-HMS model to represent individual components of the outlet works. Both outlets and spillways can be modeled using this method. "Outlets" as defined in the HEC-HMS manual typically represent structures near the bottom of the dam that allow water to exit in a controlled manner. Inputs entered to model outlets include method (orifice or culvert), number of barrels, size, length, and invert elevations. "Spillways" typically represent structures at the top of the dam that allow water to go over the dam top in a controlled manner. When modeling a spillway structure in HEC-HMS, there are three different methods available: broad-crested, ogee, and use specified. Inputs entered to model spillways include elevation, length, and spillway coefficient. A map of the significant detention structures is provided on Figure A-32.

A.7.2 Significant Detention Structures, Central Region

Altura Avenue Dam

Previous reports and data gathered from multiple site visits were used to accurately model Altura Dam. The dam is located on the east side of the Franklin Mountains, south of Memphis Drive Dam (Lower) and northwest of the intersection of Scenic Drive and Kentucky Street. Altura Avenue Dam has a tributary area of 0.12 square miles. The drainage area is comprised of two landuse types. The first and most abundant is desert shrub. The second is residential which is scarce and is located upstream of the dam.

The area of the basin is 0.9 acres and it has a capacity of 2.1 acre-feet. The reservoir is 15 feet high from the outer toe to the top of the embankment. In this analysis, the top of the dam is considered to be the southeast side of the dam, which is approximately

95 feet long. The emergency spillway is on the south side of the dam and is 40 feet wide. The spillway overflows into a separate stilling basin that has a rock wall on the downstream side and a concrete channel that flows underneath the wall. The concrete channel is also the discharge location for the principal spillway, which is drop inlet connected to a 36-inch reinforced concrete pipe (RCP). The flow from the principal spillway is directed south, under Scenic Drive, and eventually discharges into Kentucky Dam (Upper). Altura Avenue Dam was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event.

Cemex Spillway

Previous reports and data gathered from multiple site visits were used to accurately model Cemex Spillway. The spillway is located at the foot of the Franklin Mountains, south of McKelligon Dam and west of Van Buren Dam. Cemex Spillway has a tributary area of 0.92 square miles. The upstream side of the drainage area is the Franklin Mountains, consisting of desert shrub, and the downstream end of the watershed is a large quarry, which was classified with newly graded or commercial and business land use types.

The area of the basin is 1.1 acres and it has a capacity of 6.1 acre-feet. The reservoir is 15 feet high from the outer toe to the top of the embankment. The top of the dam consists of a concrete crest control structure and is 125 feet long. The emergency spillway is also concrete and is 75 feet wide with energy dissipators on the downstream side. The spillway flows into the Van Buren Ditch, which conveys overflow to Van Buren Dam. Cemex Spillway does not have a principal spillway and was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event.

Campbell Reservoir

The reservoir is of sufficient size to hold enough water to let the peak of a large storm pass before beginning to pump into Dallas Reservoir. Therefore, the reservoir was not modeled in HEC-HMS for this analysis. The basin is located on the western side of the Central Region, just south of IH-10. Campbell Reservoir has a tributary area of 0.26 square miles. The drainage area is urban and consists of residential housing as well as commercial and business land use types. The basin also captures stormwater from the adjacent IH-10 Highway.

The footprint of the basin is 2 acres and it has a capacity of 25 acre-feet. The maximum capacity was determined to occur at the elevation just before the pump structure becomes inundated. The pump discharges flow through a 12-inch line towards Dallas Reservoir. The concrete reservoir is approximately 30 feet deep and has a perimeter of 1,357 feet.

Cebada Reservoir

Data were gathered from TxDOT plans and through multiple site visits to accurately model Cebada Reservoir. Cebada Reservoir is located at the intersection of Cebada Road and Gateway Boulevard. The reservoir was originally intended to collect street flow through drop inlets on adjacent streets and along Gateway Boulevard. The stormwater would then be discharged to the Rio Grande through two 6-foot by 6.5-foot box conduits. The two box conduits outfall into the Cebada Pump Station. The Pump station then releases the stormwater into the Rio Grande. The purpose of this structure is to pass all water north of IH-10 downstream without affecting the Highway.

Many watersheds contribute to the total flow entering the structure. A large portion of the water travels down the watershed as concentrated street flow until entering the surrounding drop inlets and discharging into Cebada Reservoir. A portion of the total volume enters Cebada Reservoir through a 48-inch conduit, which is the discharge structure for Copia Channel. Stormwater also enters through a 60-inch conduit, which conveys water from the drainage inlet at the intersection of Magnolia Street and Gateway Boulevard.

The area of the reservoir is 1.6 acres and it has a capacity of 7.2 acre-feet. Cebada Reservoir is 7 feet deep and has a perimeter of 2,632 feet. The two 6-foot by 6.5-foot box outflow conduits are crossed at multiple locations by various utility lines, which reduce the overall discharge capacity. The two existing outlet conduits were modeled using CulvertMaster, which produced an elevation-discharge curve for the reservoir. The elevation-discharge curve produced in CulvertMaster and the elevation-storage curve produced by GIS were used as the input parameters to model the reservoir in HEC-HMS.

Dam No. 8

Dam No. 8 is a flood and debris control dam, maintained and operated by EPWU. The dam was constructed in 1948 by the City of El Paso. The dam is not used to retain water on a regular basis. Therefore, there is typically little to no water in the reservoir. The dam is located at the foot of the east side of the Franklin Mountains, northeast of the intersection of Tremont Avenue and Cotton Street. The dam has a tributary area of 0.05 square miles, most of which is undeveloped mountainous desert terrain with uncontrolled flow. The dam is an earth-filled structure and is classified as a downstream urban environment. Dam No. 8 is approximately 600 feet long and 12 feet high from the outer toe to the top of the embankment. The dam has a principal drop spillway, which is connected to a 112-foot-long, 36-inch diameter corrugated metal pipe (CMP).

The principal spillway tower was located by a survey crew and invert elevations were given for the 36-inch CMP. However, the discharge location was not located by the survey crew and no invert elevation was recorded to mark the outlet of the conduit. Furthermore, it was not obvious from the aerial photographs or 2003 retrofitting plans exactly where the outlet to the principal spillway is located. Therefore, it is assumed

that the discharge location is 112 feet from the drop spillway, in the southeast direction. The discharge runs south, down Cotton Street, until it reaches the named Cotton Yandell storm drain where it is directed to the Dallas Reservoir. There is no auxiliary spillway for Dam No. 8. If the dam overtops, excess discharge will continue on the same route as the principal spillway discharge.

The total stage-area-discharge table produced for Dam No. 8 by MCI in the *Dallas St. Pump and Drainage System Preliminary Engineering Report* (MCI, 2007) was the input used to model the dam in HEC-HMS for this study. The elevations were adjusted to correlate with the datum used by URS for other dams in this analysis.

Dam No. 9

Dam No. 9 is a flood and debris control dam, maintained and operated by EPWU. The dam was constructed in 1948 by the City of El Paso. The dam is not used to retain water on a regular basis. The dam is located at the foot of the east side of the Franklin Mountains, north of the intersection of Denver Avenue and Idaho Street. Dam No. 9 has a tributary area of 0.03 square miles, most of which is undeveloped mountainous desert terrain with uncontrolled flow. However, there are also 4.9 acres of commercial development in the drainage area, which flows across Murchison Street and into the reservoir. There is potential for an even larger drainage area for the dam because 2003 retrofitting plans indicate that drainage inlets on the north and south sides of Detroit Street were proposed to be installed, as well as a ramp, which would direct flow from Detroit Street into the dam reservoir. These proposed structures were not marked by the survey crew and are not visible from the 2006 Orthophotography (City of El Paso, 2006) obtained; so it is assumed that currently they do not exist.

The dam is an earth-filled structure and has a downstream urban environment. Dam No. 9 is approximately 270 feet long and 21 feet high from the outer toe to the top of the embankment. The dam has a principal drop spillway, which is connected to a 104-foot-long, 36-inch CMP.

The principal outlet discharges into a 10-foot-wide earthen channel located southeast of the dam. The 50-foot-long channel leads directly to Denver Avenue. The discharge will continue to flow in the southeast direction until it reaches Cotton Street, where it will turn south and head towards the storm system. Once the flow has reached the storm drain system, it will eventually discharge into the Dallas Reservoir. There is no auxiliary spillway for Dam No. 9. If the dam overtops, excess discharge will continue on the same route as the principal spillway discharge.

The total stage-area-discharge table produced for Dam No. 9 by MCI in the *Dallas St. Pump and Drainage System Preliminary Engineering Report* (MCI, 2007) was the input used to model the dam in HEC-HMS for this study. The elevations were adjusted to correlate with the datum used by URS for other dams in this analysis.

Dam No. 10

Dam No. 10 is a City of El Paso dam for which original construction plans were unavailable, but it was included in the dam improvement project of 1948. The dam is located at the southern base of the Franklin Mountains, at the intersection of Wright Avenue and Grandview Avenue. The dam has a tributary area of 0.07 square miles, about 45% of which is residential; the rest is steep, undeveloped, mountainous desert terrain of the Franklin Mountains. The site consists of one detention basin with a 15-foot-high embankment structure, approximately 260 feet in length. The principal outlet is a 3-foot by 3-foot concrete drop structure that flows into a 3-foot by 3-foot concrete culvert conduit. Dam No. 10 has no auxiliary spillway, and overflow is expected to run over the entire breadth of the dam.

Dam No. 10 was modeled in the Water Resources Site Analysis Program (SITES) as part of the Work Order 3 analysis, which used information from survey data, the 1948 construction plan information, and the TxDOT contours. The total stage-storage-discharge table produced by SITES was the input used to model the dam in HEC-HMS for this study.

Dallas Reservoir

Data were gathered from TxDOT plans and through multiple site visits to accurately model Dallas Reservoir. The Dallas Reservoir is located at the intersection of IH-10 and Cotton Street. The Highway is elevated and the Reservoir is located beneath it. The Dallas Reservoir includes an east and a west reservoir, which are hydraulically connected and fill up simultaneously. These discharge conduits flow into different storm sewer systems. The two gravity box conduits (6-foot by 5-foot on the west and 7-foot by 5-foot on the east) discharge water into the Rio Grande. There is currently no pump to discharge water into the Rio Grande when the water surface elevation of the river is at flood levels. There are several drainage areas that contribute to the inflow of the reservoir. The landuse types of those drainage areas vary from desert shrub at the southern base of the Franklin Mountains to commercial and business immediately upstream of the reservoir.

The total area of the basin is 7.8 acres and it has a capacity of 39 acre-ft. The reservoir is 11 feet deep and has a perimeter of 2,363 feet. The two existing outlet conduits were modeled separately using CulvertMaster, which produced an elevation-discharge curve for each conduit. The outflows at each elevation were added together to produce a total elevation-discharge curve for the reservoir. The total elevation-discharge curve and the elevation-storage curve produced by GIS were used as the input parameters to model the reservoir.

Fort Boulevard Reservoir

Fort Boulevard Reservoir is a flood and debris control dam, maintained and operated by EPWU. The dam was constructed in 1948 by the City of El Paso. The dam is not used to retain water on a regular basis. The dam is located at the foot of the east side of the Franklin Mountains, west of the intersection of Nations Avenue and Morehead Avenue.

The dam has a tributary area of 0.22 square miles, all of which is undeveloped mountainous desert terrain with uncontrolled flow. The dam is an earth-filled structure and has a downstream urban environment. The crest of Fort Boulevard Reservoir is 226 feet long and 28 feet high from the outer toe to the top of the embankment. The dam has an emergency spillway, but no evidence of a principal spillway.

Retrofitting plans from 2003 indicate that an outlet tower was proposed to be built for Fort Boulevard Reservoir. An outlet tower and discharge location were not located by the survey crew, and it is not obvious from the aerial photographs exactly where these structures are relative to the dam. Therefore, it is assumed that the proposed drop spillway, which was supposed to connect to an existing 12-inch diameter steel pipe, has not been constructed yet. If the principal outlet is constructed, it will discharge into the same drainage path as the auxiliary spillway.

The auxiliary spillway is 50 feet wide with concrete crest control. Flow leaving the spillway will travel east, into a 50-foot-wide earthen channel and then proceed east onto Fort Street. Eventually, the flow will drain southeast and then south, into Copia Ditch.

Kentucky Dam (Lower)

Kentucky Dam (Lower) is a City of El Paso dam that was also included in the storm and drainage control improvement project of 1948. The dam is located south of Kentucky Dam (Upper), between Kentucky Street and Alabama Avenue, at the southeastern base of the Franklin Mountains. Kentucky Dam (Lower) has a cumulative tributary area of 0.3 square mile and is directly downstream of Kentucky Dam (Upper), which discharges flow into the dam from its principal outlet, a 60-inch CMP.

Kentucky Dam (Lower) consists of a 9-foot-high masonry embankment structure, approximately 240 feet in length. The principal outlet of the downstream basin is a 4-foot by 4-foot masonry drop structure that flows into a 3.5-foot by 2-foot masonry box conduit which outlets into a stilling basin at the base of the auxiliary spillway drop structure. The auxiliary spillway of the downstream basin is a masonry drop structure approximately 40 feet wide. The stilling basin discharges directly into the Wheeling Street and Alabama Avenue intersection. The Kentucky Dam (Lower) modeled in SITES for Work Order 3 was the input used to model the dam in HEC-HMS.

Kentucky Dam (Upper)

Kentucky Dam (Upper) is a City of El Paso dam that was also included in the storm and drainage control improvement project of 1948. The dam is located south of Memphis Dam (Lower), between Kentucky Street and Alabama Avenue, at the southeastern base of the Franklin Mountains. Kentucky Dam (Upper) has a cumulative tributary area of 0.18 square mile and is directly upstream of Kentucky Dam (Lower).

The principal outlet of Kentucky Dam (Upper) is a 4-foot by 4-foot drop inlet structure that flows to a 60-inch conduit which outlets to the downstream Kentucky Dam (Lower) detention basin. The basin has no auxiliary spillway, although the south side

embankment will act as an auxiliary spillway in a major flood event in which the dam is overtopped.

Kentucky Dam (Upper) is a rectangular basin-type pond, excavated into the existing terrain, rather than an embankment-type dam. There is currently no mechanism in place for releasing large flows. Floodwater overtops the dam crest on the south side. The south side embankment between Kentucky Dam (Upper) and Kentucky Dam (Lower) is approximately 48 feet wide and 265 feet long. The area on top of the embankment is currently being used as a storage area. The east side of the embankment is somewhat lower than the south side of the embankment; however, the 1948 construction plans indicate a wall running along the east side. The presence of the wall was confirmed by aerial photographs and should prevent flow over the east side of the embankment. The condition and exact extent of the wall is unknown. If the wall fails, floodwaters will drain into a residential area. The Kentucky Dam (Upper) was modeled in SITES for Work Order 3 and assumed overtopping on the south side of the embankment only. The total stage-storage-discharge table produced by SITES was the input used to model the dam in HEC-HMS for this study.

Louisiana Drive Dam (Lower)

Louisiana Drive Dam (Lower) is a flood and debris control dam, maintained and operated by EPWU. The dam was constructed in 1948 by the City of El Paso and is not used to retain water on a regular basis. Therefore, there is typically little to no water in the reservoir. The dam is located northeast of the intersection of Louisiana Street and Nashville Avenue and has a cumulative drainage area of 0.18 square mile. The land cover over which the runoff flows consists of undeveloped mountainous desert terrain with uncontrolled flow in the western section of the drainage area, and changes to runoff through residential neighborhoods in the eastern section of the drainage area. Louisiana Drive Dam (Upper) is directly upstream and drains into Louisiana Drive Dam (Lower) via two 48-inch culverts.

The earth-filled embankment is approximately 285 feet long and 18 feet high from the outer toe to the top of the embankment (Nashville Avenue). The dam has a drop spillway, which is connected to a 166-foot-long, 60-inch diameter CMP.

The principal outlet discharges into a 25-foot wide earthen channel located south of Nashville Avenue. The 250-foot long, loosely defined channel leads the flow southeast into residential neighborhoods. The discharge will continue to flow south, down Elm Street, eventually reaching Cebada Reservoir. Eucalyptus to Cebada drains northeast into the drainage area of the Cebada Drainage Outfall, a 6-foot by 5-foot concrete box culvert which flows south, into the Rio Grande River. There is no auxiliary spillway for Louisiana Drive Dam (Lower). If the dam overtops, excess discharge will flow over Nashville Avenue and continue on the same route as the principal spillway discharge.

Louisiana Drive Dam (Upper)

Louisiana Drive Dam (Upper) is a flood and debris control dam, maintained and operated by EPWU. The dam was constructed in 1948 by the City of El Paso and is not used to retain water on a regular basis. Therefore, there is typically little to no water in the reservoir. The dam is located northeast of the intersection of Louisiana Street and Mobile Avenue and has a drainage area of 0.14 square mile. The land cover over which the runoff flows consists of undeveloped mountainous desert terrain with uncontrolled flow in the western section of the drainage area. A small ponding area is directly upstream and drains into Louisiana Drive Dam (Upper) through two 48-inch culverts.

The earth-filled embankment is 140 feet long and 12 feet high from the outer toe to the top of the embankment (Mobile Avenue). The dam has two 48-inch concrete culverts, which act as a principal spillway into Louisiana Drive Dam (Lower). There is no auxiliary spillway for Louisiana Drive Dam (Upper). If the dam overtops, excess discharge will flow over Mobile Avenue and into Louisiana Drive Dam (Lower). The Louisiana Drive Dam (Upper) was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event.

Lower Durazno Basin

Lower Durazno Basin was modified in 2007 as part of the TxDOT *Plans of Proposed Highway Routine Maintenance Contract*. The basin is located at the intersection of US 54 (Patriot Freeway) and IH-10 and has a tributary area of 1 square mile. The landuse type of the drainage area is almost entirely urban, but the basin also receives inflow from the US 54 storm sewer as well as discharge from the Upper Durazno principal and emergency spillways.

The area of the basin is 22.8 acres and it has a capacity of 477 acre-feet. The reservoir is approximately 25.5 feet deep and has a perimeter of 6,147 feet. In this analysis, the top of the dam is considered to be the south side of the dam (excluding the spillway), which is approximately 2,270 feet long. The auxiliary spillway is located in the southeast corner of the dam and is lined with concrete. The spillway is 65 feet long and outfalls into a former residential area, which has now been bought by the City of El Paso. The principal spillway for the basin is a drop inlet connected to a 30-inch diameter RCP. The inlet tower has an 18-inch diameter inlet at the base of the tower and a 1.8-foot by 1.8-foot square inlet located on the side of the tower, 6.3 feet from the base. The outlet structure was modeled as an orifice with an inlet at an elevation equal to the elevation at the top of the square inlet. The 30-inch RCP connected to the intake tower directs outflow to the Lincoln Drain. Lower Durazno Basin was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event.

Magnolia Reservoir

Data were gathered from TxDOT plans and through multiple site visits to accurately model Magnolia Reservoir. The reservoir is located south of the intersection of Magnolia Street and Grant Avenue. Magnolia Reservoir has a direct urban tributary area of 0.09 square mile, but also receives discharges from San Diego Dam, Ohio Street Reservoir, and Tremont Reservoir.

The area of the reservoir is 1.4 acres and it has a capacity of 9 acre-feet. The reservoir is approximately 15 feet deep and has a perimeter of 1,139 feet. There is no emergency spillway for Magnolia Reservoir. A principal spillway, which consists of a drop inlet, is connected to a 48-inch conduit and discharges south of the dam onto Magnolia Street. The stormwater travels south as street flow until captured and directed into a 60-inch diameter storm drain known as Eucalyptus to Cebada. Magnolia Reservoir was entered into HEC-HMS using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event.

McKelligon Dam

McKelligon Dam was built 4.5 miles north of downtown El Paso in 1982 by USACE. The dam is owned by the City of El Paso and located northwest of the intersection of McKelligon Canyon Road and Alabama Street. The dam is approximately 105 feet high with a top of embankment elevation of 4,447.8 feet. The drainage area encompasses approximately 2.2 square miles and consists of steeply sloping desert terrain runoff, captured from the east side of the Franklin Mountains. McKelligon Dam has a principal outlet and an auxiliary spillway that discharge into two different stilling basins.

The principal outlet consists of a hooded intake structure that flows into a 620-foot long, 3-foot diameter concrete conduit. The conduit discharges at the southeastern toe of the dam into a 10-foot wide, riprap-lined, earthen channel, which discharges into McKelligon Reservoir A. The auxiliary spillway is formed by McKelligon Canyon Road, which contours show to also release flow into McKelligon Reservoir B. McKelligon Dam was modeled in SITES for Work Order 3. The total stage-storage-discharge table produced by SITES was the input used to model the dam in HEC-HMS for this study.

McKelligon Reservoir A

McKelligon Reservoir A is one of the stilling basins in the McKelligon Dam System, which was built 4.5 miles north of downtown El Paso in 1982 by USACE. McKelligon Reservoir A receives flow from an immediate tributary area of 0.04 square mile as well as from the principal spillway of McKelligon Dam. The area of the basin is 1.8 acres and has a capacity of 7 acre-feet. The reservoir is 35 feet high from the outer toe to the top of the embankment (Davis-Seamon Road), which is approximately 130 feet long. The basin does not have an emergency spillway, but it does have a 2-foot by 2-foot principal drop spillway, which is connected to a 24-inch diameter RCP. The flow from the principal spillway is directed into McKelligon Reservoir B. The basin was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that

the basin is empty at the beginning of the storm event. Outflow from the McKelligon system is modeled to eventually reach Pershing Dam.

McKelligon Reservoir B

McKelligon Reservoir B is one of the stilling basins in the McKelligon Dam System, which was built 4.5 miles north of downtown El Paso in 1982 by USACE. McKelligon Reservoir B receives flow from an immediate tributary area of 0.1 square mile as well as discharge from the principal spillway of McKelligon Reservoir A and the auxiliary spillway of McKelligon Dam. The McK_Srvy.shp file from Work Order 3 was used in GIS to determine the outlet structure's invert elevations.

The area of the basin is 12 acres and it has a capacity of 0.09 acre-feet. The upstream end of the basin is approximately 80 feet higher in elevation than the downstream end of the basin and the embankment is only roughly 12 feet high from the outer toe to the top of the embankment (McKelligon Canyon Road). Therefore, the storage area is relatively small compared to the area of the basin. McKelligon Reservoir B acts more as a localized drainage area to McKelligon Channel than as a reservoir. The basin does not have an emergency spillway, but it does have a 36-inch RCP outlet culvert, which acts as a principal spillway. The flow from the culvert is directed into McKelligon Reservoir C. The basin was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event. Outflow from the McKelligon system is modeled to eventually reach Pershing Dam.

McKelligon Reservoir C

McKelligon Reservoir C is one of the stilling basins in the McKelligon Dam System, which was built 4.5 miles north of downtown El Paso in 1982 by USACE. McKelligon Reservoir C receives flow from an immediate tributary area of only 0.01 square mile, but it receives the majority of its inflow from the principal spillway or overtopping of McKelligon Reservoir B.

The area of the basin is 3 acres and it has a capacity of 7.4 acre-feet. The basin does not have an emergency spillway, but it does have a principal drop spillway with a 2-foot by 2-foot opening on top. The drop spillway is connected to a 36-inch diameter RCP and conveys flow into McKelligon Reservoir D, the final stilling basin in the McKelligon system. McKelligon Reservoir C was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event. Outflow from the McKelligon system is modeled to eventually reach Pershing Dam.

McKelligon Reservoir D

McKelligon Reservoir D is one the final stilling basins in a series of stilling basins that are part of the McKelligon Dam System, which was built 4.5 miles north of downtown El Paso in 1982 by USACE. McKelligon Reservoir D receives flow from an immediate

tributary area of only 0.01 square mile, but it receives the majority of its inflow from the principal spillway or overtopping of McKelligon Reservoir C.

The area of the basin is 1.1 acres and it has a capacity of 1.1 acre-feet. The basin does not have an emergency spillway, but it does have an 18-inch RCP culvert outlet that conveys flow under Alabama Street, and eventually onto Louisiana Street, where it flows south, and eventually discharges into Pershing Dam. The outlet of the 48-inch principal spillway flows through an alley located southwest of the intersection of McKelligon Canyon Road and Louisiana Street. In December 2007, the City of El Paso surveyed the top of the stilling basin profile, which confirmed that flow overtopping the furthest downstream stilling basin would flow out to Alabama Street. Project topography indicated flow would then follow Alabama Street south towards Van Buren Dam. McKelligon Reservoir D was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event.

Memphis Dam (Lower)

Memphis Dam (Lower) is a City of El Paso dam for which original construction plans were unavailable. Improvements to the dam were made by the City of El Paso in 1948 in a project called "Stormwater and Drainage Control Works" in which many of the City's dams were upgraded. Memphis Dam (Lower) is located at the west end of Memphis Avenue at the southeastern base of the Franklin Mountains. The dam has a cumulative tributary area of 0.26 square mile, most of which is the steep, undeveloped, mountainous desert terrain of the Franklin Mountains. A very small portion is residential, less than 5%.

The site consists of one detention basin with an 18-foot high masonry embankment structure, approximately 311 feet in length. The principal outlet, a 12-inch diameter steel standpipe and conduit, was not located during survey of the dam and was therefore not modeled. The auxiliary spillway is a masonry drop structure with a width of approximately 45 feet and a crest arc length of 53 feet. The embankment crest is 3 feet above the auxiliary spillway crest. The structure drops about 24 vertical feet in roughly 16 horizontal feet into a stilling basin that was assessed by URS in November 2006 (Ref 204) to be almost completely filled with sediment. The stilling basin discharges directly into the intersection of Memphis Avenue and Kentucky Street, a densely populated area.

The Memphis Dam (Lower) was modeled in SITES for Work Order 3. The total stage-storage-discharge table produced by SITES was the input used to model the dam in HEC-HMS for this study.

Memphis Dam (Upper)

Data were gathered from TxDOT plans and through multiple site visits to accurately model Memphis Dam. However, there is sufficient topographic data and information from previous reports to model the dam in HEC-HMS. The reservoir is located at the

southeastern base of the Franklin Mountains, northeast and upstream of Memphis Dam (Lower). Memphis Dam (Upper) has a tributary area of 0.25 square mile, all of which is the steep, undeveloped, mountainous desert terrain of the Franklin Mountains.

The area of the reservoir is 0.4 acre and it has a capacity of 12.3 acre-feet. The dam is approximately 22 feet high from the outer toe to the top of the embankment. There is no principal spillway for Memphis Dam (Upper), but there is a 35-foot-wide auxiliary spillway which utilizes concrete crest control. The embankment is approximately 7 feet higher than the emergency spillway elevation and is bounded by a wall on the northeast side of the dam. A residential area exists directly on the other side of that wall. The emergency spillway discharges flow into a 500-foot-long channel, which leads to Memphis Dam (Lower). Memphis Dam Upper was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event.

Ohio Street Reservoir

Ohio Street Reservoir is a flood and debris control dam, maintained and operated by EPWU. URS could not obtain the original plans for the dam; therefore, it is not known when it was constructed or who constructed it. The dam is not used to retain water on a regular basis.

Ohio Street Reservoir is downstream of San Diego Dam and located north of the intersection of Portland Avenue and Ohio Street. The dam has a cumulative drainage area of 0.13 square miles, which is the sum of its relatively small drainage area of 0.01 square miles and San Diego Dam's larger drainage area of 0.12 square miles. Under controlled circumstances, Ohio Street Reservoir receives the majority of its flow from an inlet on the northwest side of the dam. This inlet captures the flow from a 200-foot long channel that conveys drainage from the principal spillway of San Diego Dam. Ohio Street Reservoir is an earth-filled structure. The embankment (Portland Avenue) is approximately 26 feet high from the outer toe to the top of the embankment and it is roughly 400 feet long. The dam has a drop spillway, which is connected to an arch shaped, 110-foot long, 48-inch-equivalent diameter RCP.

The principal outlet discharges on the south side of Portland Avenue, into an undeveloped lot, where it proceeds to drain south, toward a row of houses. There is a 48-inch diameter RCP just north of the houses, which under controlled circumstances should capture the flow coming out of the principal spillway, assuming that the pipe is not clogged with silt or other debris. This 48-inch diameter pipe then carries the water underneath Pittsburgh Street and into Tremont Reservoir. If there is a breach or overtopping of Ohio Street Reservoir and the volume of water is not able to be drained by the 48-inch diameter pipe located north of the houses, it will flow across the row of houses and across Pittsburgh Avenue, into Tremont Reservoir. The total elevation-area-discharge table produced for Ohio Street Reservoir by MCI in the *Dallas St. Pump and Drainage System Preliminary Engineering Report* (MCI, 2007) was the input used

to model the dam in HEC-HMS for this study. The elevations were adjusted to correlate with the datum used by URS for other dams in this analysis.

Pershing Dam

Pershing Dam was designed by USACE in 1975 and completed in 1977. The dam is located at the outlet of the City of El Paso's Central Drainage Area. The upstream corner of the dam is located at the corner of US 54 and Pershing Avenue and it is bounded on the west side by US 54. The cumulative drainage area for Pershing Dam is approximately 4.7 square miles and includes the McKelligon and Van Buren drainage systems. Pershing Dam also receives discharge from the Fort Bliss Sump Outflow Conduit, which was modeled as a source in HEC-HMS. The drainage area immediately upstream of Pershing Dam encompasses approximately 1.1 square miles and consists mostly of developed, residential plots. Flow through this area is considered to be surface flow through streets and neighborhoods.

Pershing Dam is nearly 3,430 feet along the top of its embankment and 48 feet high. The dam was originally constructed with a 21.5-foot wide hood inlet draining to a 16-foot by 14.67-foot culvert serving as the principal and auxiliary spillways. The culvert flows into a concrete-lined stilling basin located across Pershing Avenue. In 1993, USACE completed a spillway modification project (Ref 74) that added a new concrete auxiliary spillway (crest elevation approximately 3,848.5 feet) to allow the dam to safely pass the full PMF. The existing hood inlet continues to function as the principal spillway. Plans and survey data show that both the auxiliary spillway crest and principal outlet inlet have approximately the same elevation. This means that except for outflow through the low-flow port in the intake structure, a significant discharge from Pershing Dam will not occur until the pool elevation is above the auxiliary spillway crest elevation. The concrete auxiliary spillway is approximately 170 feet wide and is located on the southern end of the dam. Starting at the crest of the auxiliary spillway and extending down the steep portion of the spillway channel, 8-foot-wide by 6.5-foot-tall concrete baffles spaced at 15.67 feet center to center were installed across the width of the spillway. Flow from the auxiliary spillway proceeds across Pershing Avenue and into the concrete stilling basin. The concrete stilling basin is drained by the Government Hill Ditch Outlet Conduit, which is 90 inches in diameter.

Pershing Dam was modeled in SITES for Work Order 3. The total stage-storage-discharge table produced by SITES was the input used to model the dam in HEC-HMS for this study.

San Diego Dam

San Diego Dam is a flood and debris control dam, maintained and operated by EPWU. The dam was constructed in 1948 by the City of El Paso. The dam is not used to retain water on a regular basis. Therefore, there is typically little to no water in the reservoir. The dam is located at the foot of the east side of the Franklin Mountains, north of the intersection of Cotton Street and San Jose Avenue. The dam has a tributary area of 0.12 square miles, most of which is undeveloped mountainous desert terrain with

uncontrolled flow. However, within the drainage area, there is a commercial development with an area of approximately 3.9 acres. This development utilizes a culvert to discharge runoff from the property into the dam's reservoir. San Diego Dam is an earth-filled structure and has a downstream urban environment. The dam is approximately 500 feet long and 56 feet high from the outer toe to the top of the embankment. The principal outlet of the dam is a drop spillway, which is connected to an approximately 570-foot-long, 36-inch diameter RCP.

The principal outlet discharges into a 40-foot-wide earthen channel located to the southeast of the dam. The 200-foot-long channel leads directly to the Ohio Street Reservoir. There is no auxiliary spillway for San Diego Dam.

Scenic Drive Dam

There were no plans obtained by URS for Scenic Drive Dam, so it is unknown when it was built and who constructed the reservoir. However, there is sufficient topographic data and information from previous reports to model the dam in HEC-HMS. The reservoir is located at the eastern foot of the Franklin Mountains, south of Scenic Drive and west of the intersection of Indiana Street and Copper Avenue. Scenic Drive Dam has a tributary area of 0.13 square mile, all of which is the steep, undeveloped, mountainous desert terrain of the Franklin Mountains.

The area of the reservoir is 2 acres and it has a capacity of 18.4 acre-feet. The dam is approximately 36 feet high from the outer toe to the top of the embankment, which is about 363 feet long. There is no emergency spillway for Scenic Drive Dam, but there is a 24-inch metal culvert which acts as a principal spillway for the dam. The outlet discharges into a residential area and eventually drains into Cebada Reservoir. Scenic Drive Dam was entered into HEC-HMS as a reservoir using the stage-storage function and the assumption that the basin is empty at the beginning of the storm event.

Tremont Reservoir

Tremont Reservoir is a flood and debris control dam, maintained and operated by EPWU. The dam was constructed in 1948 by the City of El Paso. The dam is not used to retain water on a regular basis. Therefore, there is typically little to no water in the reservoir.

Tremont Reservoir is located northwest of the intersection of Tremont Avenue and Indiana Street. The dam has a cumulative drainage area of 0.14 square miles when its relatively small drainage area of 0.01 square miles is added to Ohio Street Reservoir's cumulative drainage area of 0.13 square miles. The dam receives the majority of its flow from an inlet channel on the northern side of the reservoir. The channel starts at Pittsburgh Street, where it can capture excess flow from the Ohio Street Reservoir. The channel is approximately 100 feet long and flows south into Tremont Reservoir. The dam is an earth-filled structure and has a downstream urban environment. The embankment (Tremont Avenue) is approximately 200 feet long and 20 feet high from

the outer toe to the top of the embankment. The dam has a drop spillway, which is connected to a 90-foot long, 30-inch diameter RCP.

The principal outlet discharges on the south side of Tremont Avenue into a concrete energy dissipator, where it is directed into a drainage ditch flowing east and then south, around a commercial development. The drainage then continues to flow south, across Murchison Drive, onto the property of El Paso Technical High School. TxDOT topography and 2006 Orthophotography suggest that the majority of the high school campus drains east, into an approximately 26-foot-wide channel, which directs flow further east, towards Magnolia Reservoir.

There is no auxiliary spillway for Tremont Reservoir. If the dam is overtopped, water will flow over Tremont Avenue and into the same ditch which carries the discharge from the drop spillway. In the event that the ditch is full, flow will be carried across the commercial development and continue south on the same general route as the principal spillway discharge.

The total elevation-area-discharge table produced for Dam No. 9 by MCi in the *Dallas St. Pump and Drainage System Preliminary Engineering Report* (MCi, 2007) was the input used to model the dam in HEC-HMS for this study. The elevations were adjusted to correlate with the datum used by URS for other dams in this analysis.

Upper Durazno Basin

Upper Durazno Basin was modified in 2007 as part of the TxDOT *Plans of Proposed Highway Routine Maintenance Contract*. The basin is located northeast of the intersection of US 54 and IH-10 and has a tributary area of 1 square mile. The landuse type of the immediate drainage area is urban, but the basin also receives discharge from the Boone Street Basin diversion on the northwest and a flume on the western side, which drains runoff from Concordia Cemetery.

The area of the basin is 6.3 acres and it has a capacity of 73.4 acre-feet. The reservoir is approximately 22.5 feet deep and has a perimeter of 2,073 feet. In this analysis, the top of the dam is considered to be the south side of the dam (excluding the spillway), which is approximately 254 feet long. The auxiliary spillway is located in the center of the southern embankment, at an elevation that is one foot lower than the top of the embankment. The concrete emergency spillway is 46 feet long and outfalls into the Lower Durazno Basin.

A 72-inch RCP that conveys stormwater from US 54 to Lower Durazno runs through the Upper Durazno Basin. The 72-inch storm drain also acts as a principal spillway for Upper Durazno because it is connected to an intake tower that allows water to drain into the storm sewer system. The intake tower is located just north of the emergency spillway and acts as a junction where the 72-inch RCP and the inflow from Upper Durazno discharge through two 6-foot by 6-foot concrete box culverts, into Lower Durazno. Upper Durazno Basin was entered into HEC-HMS as a reservoir using the

elevation-storage function and the assumption that the basin is empty at the beginning of the storm event.

Van Buren Dam

Van Buren Dam is an earthen structure built by the City of El Paso in 1948. The dam is located at the foot of the east side of the Franklin Mountain Range and has a cumulative tributary area of approximately 3.6 square miles. The drainage area consists mostly of undeveloped desert terrain, fair desert shrub, and bare land. A large quarry (Cemex Spillway) is within the cumulative drainage area and is located directly northwest of Van Buren Dam. In this analysis, the McKelligon Dam system also drains into Van Buren Dam. Overflow from McKelligon Dam's downstream stilling basin (McKelligon Reservoir D) flows down Alabama Street and into Van Buren Dam. Van Buren Dam's outflow ultimately flows into Pershing Dam through the Mountain Avenue Conduit.

The top of Van Buren Dam is roughly 25 feet above the embankment toe and the principal outlet consists of a rectangular open top riser. The riser is connected to two corrugated metal conduits, each 72 inches in diameter. The conduits discharge flow into a lightly vegetated channel that discharges into the Mountain Avenue conduit, which has a capacity of 386 cubic feet per second (cfs). All flow in excess of 386 cfs will travel as surface flow through residential neighborhoods until it reaches Pershing Dam.

Van Buren Dam was modeled in SITES for Work Order 3. The total stage-storage-discharge table produced by SITES was the input used to model the dam in HEC-HMS for this study. Although McKelligon-Fillmore Design Plans from 1978 indicate that Van Buren Dam has two auxiliary spillways approximately 6 feet below the top of dam, recent survey data and URS dam inspections found no evidence of a defined auxiliary spillway. The area designated as the auxiliary spillway on general plans is currently at the same elevation as the other top-of-dam sections. Flow in excess of the volume that the dam's principal outlet can discharge and the basin area can store will flow over the top of the embankment. Therefore, to analyze the dam using SITES in Work Order 3, the auxiliary spillway was defined as the top of dam (roughly 900 feet long at an elevation of 4,122.4 feet) with a very mild side slope. The drainage area used in previous studies was approximately 17% smaller than the drainage area delineated for Work Order 3. The discrepancies in drainage area are due in part to the assumption in previous studies that a new dam (Fillmore Dam) would be located below the active quarry currently located in the Van Buren drainage area. In the years after this study, the quarry site expanded to the point where construction of Fillmore Dam was no longer a feasible option.

A.7.3 Significant Detention Structures, East Side Region

Jesuit Basin

Jesuit Basin is located approximately one block north of the Lee Trevino Drive IH-10 intersection. It receives flow from a tributary area of 1.78 square miles of a mixture of

commercial and residential land uses. Jesuit Basin has the capacity to hold 271 acre-feet and the maximum flow leaving the primary 18-inch spillway is 22 cfs. Outflow from Jesuit Basin is connected to the culvert system under IH-10 that empties into Burnham Channel and finally into Lomaland Basin System within Mission Valley Region.

Lafayette Draw Basin

The Lafayette Draw Basin is located just southwest of the intersection of Pellicano Drive and Vista De Oro Drive, within the Carolina Dam Basin System. It receives flow from 0.42 square miles of commercial and residential land use types. The storage capacity of Lafayette Draw Basin is 77 acre-feet and the capacity of the 18-inch outlet pipe is 26 cfs. Outflow from Lafayette Draw Basin is connected to Lafayette Draw Channel under IH-10 into Mission Valley Region and finally into Carolina Dam.

Cielo Vista Basin A

Cielo Vista Basin A is a subterranean basin which lies directly under Cielo Vista Mall. The Cielo Vista Basin A receives flow from a tributary area 0.98 square miles. It has the storage capacity of 120 acre-feet. The 18-inch RCP primary outlet has a maximum capacity of 32 cfs. This flow is released downstream across IH-10 and into Mission Valley Region where it finally drains into the Phelps Dodge System.

Cielo Vista Basin B

Cielo Vista Basin B is located in the parking lot of the Cielo Vista Mall adjacent to the intersection of Montwood Drive and Viscount Boulevard. The tributary area to Cielo Vista B is only 0.06 square miles. Cielo Vista B has a storage capacity of 38 acre-feet and the maximum capacity of the 18-inch RCP primary outlet is 26 cfs. The flow exits the 18-inch RCP and is then routed under IH-10 into Mission Valley Region where it reaches Phelps Dodge System.

A.7.4 Significant Detention Structures, Mission Valley Region

Americas Ten Basin System

Though the construction date of Americas Ten Basin System is unknown, improvements were made to it in 1987 by Faught & Associates Inc. It is currently maintained and operated by EPWU. The basin is located in the Americas Ten Basin drainage system, approximately 4,500 feet south of the intersection of IH-10 and Loop 375. The basin has a tributary area of 2.60 square miles and receives flow from inlets on the north and northeast sides of the dam, which capture drainage from the Mercantile Channel and the RV Channel. The area of the basin is approximately 10 acres and it has a capacity of 198 acre-feet of storage. Americas Ten Basin System is approximately 18 feet deep from the outer toe to the top of the embankment and has a perimeter of approximately 2,600 feet. The dam has an emergency spillway and a principal drop spillway, which is connected to a 30-inch diameter RCP. The auxiliary spillway is 340 feet wide with concrete crest control. The outflow eventually discharges into the Mesa Drain Interceptor to City Limits. The basin was entered into HEC-HMS as

a reservoir using the elevation-storage function with the assumption that the basin is empty at the beginning of the storm event.

Americas Basin System

Americas Basin System was constructed in 1991 by the USACE and is currently maintained and operated by EPWU. The basin is located approximately 2,500 feet west of the intersection of IH-10 and Loop 375 in the Americas Basin drainage system. The basin has a tributary area of 7.9 square miles and receives flow from concrete crest control inlets on the north and northeast sides of the dam. The inlet on the north side of the dam captures flow from Bluff Channel. The area of the basin is approximately 45 acres and it has a capacity of 960 acre-feet of storage. Americas Basin System is approximately 31 feet deep from the outer toe to the top of the embankment and has a perimeter of approximately 5,400 feet. The basin has an emergency spillway and a principal drop spillway, which is connected to a 36-inch diameter RCP. Outflow from Americas Basin System discharges into the Mesa Drain Interceptor, which flows along the south side of Bordeaux Drive and discharges beneath North Loop Drive into Feather Lake. The auxiliary spillway is a 290-foot-wide spillway with concrete crest control. The flow from the auxiliary spillway is directed south, towards Juan de Herrera Lateral Branch B. The basin was entered into HEC-HMS as a reservoir using the elevation-storage function with the assumption that the basin is empty at the beginning of the storm event.

Basin A

Though the construction date of Basin A is unknown, improvements were made to it in 1978. Basin A is part of the Basin A drainage system and is located west of the intersection of Springfield Drive and Ponce Drive, north of Border Highway. The basin receives flow from the Playa Drain, located on the north side of the basin. Flow from the Playa Drain bypasses Basin A through a 42-inch culvert connecting two portions of the Playa Drain just outside Basin A. Flow is also diverted to Basin A through two 10-foot by 10-foot concrete box culverts (CBCs). The area of the basin is approximately 9.6 acres with a perimeter of 2,800 feet. The basin is approximately 10 feet deep from the inside base to the top of the dam and has a capacity of 71 acre-feet of storage. According to a CH2MHILL report Basin A contains three pumps rated at 130 cfs each. The pumps convey stormwater from Basin A into an effluent chamber that is connected to a 78-inch RCP line. The RCP line conveys the stormwater from the effluent chamber, under Border Highway, to an outfall at the Rio Grande River. In addition to the pump station, Basin A has an outlet structure at the northeast end of the basin that releases flow back into the Playa Drain. The outlet structure consists of a rectangular shaped broad crested weir with a length of 170 feet that empties into a 10-foot wide by 7-foot-high concrete box. The structure acts a weir until the outlet area of the box is full and then acts as an orifice. The box structure also has a gate-controlled 2.5-foot by 6-foot opening near its outlet to allow some flow to re-enter the basin while it is filling. The basin was entered into HEC-HMS as a reservoir using the elevation-storage function with the assumption that the basin is empty at the beginning of the storm event.

Basin G

Though the construction date of Basin G is unknown, plans available for proposed enlargements of the basin are dated 1974. Basin G is part of the Basin G drainage system and is located in a rural area in the southwest valley of El Paso. Although it appears that the original intent of the basin was to receive flow from the Playa Drain, the Playa Interceptor Drain, and the interceptor system in Mission Valley, the basin currently receives flow only from the Playa Drain Interceptor under normal storm conditions. The area of the basin is approximately 16.5 acres with a perimeter of 3,500 feet. The basin is approximately 11 feet deep from the base to the top of the dam and has a capacity of 117 acre-feet of storage. The outlet structure for the basin is a pump station located on the west side of the basin that pumps water to the Rio Grande River. Basin G has no auxiliary spillway. The basin was entered into HEC-HMS as a reservoir using the elevation-storage function with the assumption that the basin is empty at the beginning of the storm event.

Carolina Dam

Carolina Dam is part of the Carolina Drive drainage system and is located north of the intersection of Carolina Drive and Lilac Drive. Carolina Dam receives flow from two inlets located on the north-northwest portion of the dam, one of which is the Lafayette Draw Channel. The area of the dam is approximately 12.5 acres with a perimeter of 2,950 feet. The dam is approximately 29 feet deep from the inside base to the top of the dam and has a capacity of 147 acre-feet of storage. Carolina Dam contains a concrete-lined auxiliary spillway 600 feet in length. The principal outlet of the dam is a 3.25-foot RCP conduit line that discharges into the Mesa Drain. The dam was entered into HEC-HMS as a reservoir using the elevation-storage function with the assumption that the dam is empty at the beginning of the storm event.

Feather Lake

Feather Lake basin was constructed in 1969 and is located in the Basin G drainage system, southwest of the intersection of North Loop Drive and Bordeaux Drive. In addition to serving as a detention basin, Feather Lake is also a wildlife sanctuary managed by the El Paso Trans-Pecos Audubon. The basin receives flow from the Mesa Drain Interceptor inlet, located on the northeast side of the dam. The area of the basin is approximately 39 acres, with a perimeter of 5,300 feet. The basin is approximately 14.5 feet deep from the inside base to the top of the dam and has a capacity of 424 acre-feet of storage. The outlet structure consists of two 60-inch RCP culverts on the southwest side of the basin, which convey discharge from the basin to the Mesa Drain Interceptor. A concrete weir is located just before the culvert entrance in order to keep water in the basin for use as a wildlife sanctuary. The basin was entered into HEC-HMS as a reservoir using the elevation-storage function with the assumption that the water surface elevation of the basin is kept at 3,658 feet throughout most of the year (due to the concrete weir just before the culvert entrance).

Lomaland Basin System

Though the construction date of Lomaland Basin System is unknown, USACE basin plans available from an El Paso flood control project are dated 1987. Lomaland Basin System is a part of the Lomaland Basin drainage system, located in between Hillcrest Middle School and Loma Terrace Elementary School. The basin receives flow from the Burnham Channel located on the north-northeast side of the basin as well as from a small local drainage sump from Hillcrest Middle School. Lomaland Basin System has a capacity of 504 acre-feet of storage. The area of the basin is approximately 23 acres and it has a perimeter of approximately 4,600 feet. The basin is approximately 30 feet deep from the inside base to the top of the dam, and it has a 1,050-foot concrete-lined spillway. Outflow from the basin flows through a 36-inch RCP to the Mesa Drain. The basin was entered into HEC-HMS as a reservoir using the stage-storage-discharge function with the assumption that the basin is empty at the beginning of the storm event.

North Loop Detention Basin

The North Loop Detention basin is a part of the Phelps Dodge Drainage System and is located south of the intersection of North Loop Drive, Delta Drive, and Trowbridge Avenue. The basin receives flow from Fort Bliss Spur Drain, located on the north-northeast side of the basin. The North Loop Detention basin is approximately 9.5 feet deep from the inside base to the top of the dam and has a capacity of 42 acre-feet of storage. The area of the basin is approximately 10.3 acres and the perimeter is 2,700 feet. The outlet structure is a 24-inch pipe that eventually discharges into the Playa Drain. This detention basin has no auxiliary spillway. The basin was entered into HEC-HMS as a reservoir using the stage-storage-discharge function with the assumption that the basin is empty at the beginning of the storm event.

Phelps Dodge System

Phelps Dodge System was constructed in 1966 and is located in the Phelps Dodge drainage system. The basin is located south of IH-10, northeast of the intersection of Hawkins Boulevard and Phoenix Street, and northwest of El Paso Community College (EPCC). The basin receives flow from Phelps Dodge Channel, as well as flow from inlets located on the north and northeast sides of the dam. These inlets capture drainage from the ends of Arlington and Yuma Streets. Phelps Dodge System has a capacity of 420 acre-feet of storage and is approximately 24 feet deep from the inside base to the top of the dam. The area of the basin is approximately 27 acres and it has a perimeter of approximately 4,500 feet. The basin has a 560-foot-wide concrete spillway. The outflow from the basin discharges to Phoenix Street, then south, along the east side of EPCC Valle Verde campus to North Loop Road, where it eventually discharges into Mesa Drain. The basin was entered into HEC-HMS as a reservoir using the stage-storage-discharge function with the assumption that the basin is empty at the beginning of the storm event.

A.7.5 Significant Detention Structures, Northeast Region

Amber Basin

Amber Basin was constructed in 1977 as part of the Northeast Drainage Improvements project. The basin is located in the Fort Bliss Sump system in Northeast El Paso approximately 0.85 mile east of the foot of the Franklin Mountains. The basin has a tributary area of 0.25 square mile with approximately 40% undeveloped mountainous desert terrain and 60% developed area consisting of single-family housing. Amber Basin is approximately 30 feet deep from the inside embankment toe to the top of embankment. It encloses approximately one city block in area. The principal outlet of Amber Basin is a 20-inch diameter pipe that transitions to a 30-inch pipe before connecting to the local stormwater collection system. The rating curve for this outlet structure was estimated utilizing Bentley CulvertMaster. The auxiliary spillway is a 250-foot wide, concrete-paved spillway with a 16:1 side slope and flows onto Polaris Street. The basin was entered into the HEC-HMS as a reservoir using the stage-storage-discharge function and the assumption that the basin is empty at the beginning of the storm event. Outflow from Amber Basin is connected downstream to Sunrise Channel.

Fort Bliss Sump

Fort Bliss Sump is a depressed basin that, under non-extreme storm conditions, receives flow from the Range Dam and Mountain Park-Sunrise Dam detention systems and encompasses a total drainage area of over 52 square miles. The drainage area surrounding and draining directly to the sump is over 42 square miles and consists mostly of residential and commercial land. The sump is located in the center of its tributary drainage area and is northeast of the intersection of Fred Wilson Avenue and Railroad Drive, across the street from the George V. Underwood, Jr. golf course.

The primary outlet for Fort Bliss Sump is the Fort Bliss Outfall Conduit, which drains to Pershing Reservoir. The conduit is 78 inches in diameter and approximately 9,000 feet long. The intake structure for the conduit is a concrete headwall located in the southwest corner of the sump. If the storage in Fort Bliss Sump exceeds the elevation of the embankment (at approximately 3,874 feet), the inundation area increases to include a much larger outer region of low lying area surrounding the sump (outer sump).

The modeling approach for the HEC-HMS analysis was to divide the facility into a series of diversions, a sink, and a storage element. The first diversion was used to account for the Fort Bliss Sump Outlet Conduit flow. To represent conduit outflow over the range of stage-storage conditions, 200 cfs to Pershing Dam was assumed. The next diversion directed flow into a sink element representing the inner basin of Fort Bliss Sump and diverted flow up to the maximum storage volume of the inner basin. Flow in excess of the maximum storage volume was directed to the outer sump. The outer sump was represented by a storage element. Under the conditions modeled in the SMP, the Fort Bliss Sump embankment is not overtopped and thus, the maximum outflow is 200 cfs resulting from the Fort Bliss Sump Outlet Conduit.

Fusselman Dam

Fusselman Dam was built by USACE in 1961. The dam is located in the Northgate-Range system in northeast El Paso at the east side of the foot of the Franklin Mountains. The dam has a tributary area of 3.37 square miles consisting of mostly undeveloped mountainous desert terrain. Fusselman Dam is approximately 65 feet high from the upstream embankment toe to the top of embankment and is roughly 1,200 feet across, enclosing the small valley that is its tributary. The principal outlet of Fusselman Dam is a 4-foot by 6-foot drop inlet that flows into a 24-inch RCP which outlets just past the downstream toe. The auxiliary spillway is a 100-foot wide, 6-foot high ogee spillway that flows into a graded earthen channel sloped at about 10%. Both the principal and auxiliary spillways flow into a naturally graded arroyo that carries the flow to Northgate Dam, located roughly 7,500 feet downstream. The dam was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event.

Hondo Pass Basin

Hondo Pass Basin was constructed in 1977 as part of the Northeast Drainage Improvements project. The basin is located in the Fort Bliss Sump system approximately 0.77 mile east of the foot of the east side of the Franklin Mountains. The basin has a tributary area of 0.079 square mile, with approximately 5% undeveloped mountainous desert terrain and 95% developed area consisting of single-family housing and commercial/industrial areas. The mostly urbanized watershed shows no defined channels.

Hondo Pass Basin is approximately 24 feet deep from the inside embankment toe to the top of embankment and encloses approximately one city block in area. The principal outlet of Hondo Pass Basin is a 20-inch diameter pipe that connects to a 33-inch diameter pipe at Neptune Street, presumably part of the stormwater collection system. The dam was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event.

Keltner Dam

Keltner Dam is located at the foot of the east side of the Franklin Mountains, north of the intersection of Alabama Street and Fred Wilson Avenue. Keltner Dam is a City of El Paso structure that was constructed in 1959. The dam has a drainage area of approximately 0.5 square mile and consists of steeply sloping, undeveloped desert shrub. The top of dam is at roughly 4,082.3 feet, and the embankment spans 780 feet. The auxiliary spillway flows out of the northeast portion of the dam, across Alabama Street, and proceeds to flow east along Wickham Avenue. Both the principal and auxiliary spillways flow towards Fort Bliss Sump, located roughly 9,000 feet downstream.

The principal outlet for the dam is a rectangular drop inlet riser that releases into two 21-inch diameter concrete conduits. One of the conduits flows to the southeast, releasing into a residential street. The other conduit flows to the northeast, discharging

into a more recently developed residential street. The dam was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event.

Mountain Park Dam

Mountain Park Dam was constructed in 1974 by USACE and is maintained and operated by the City of El Paso. The basin is located in the Fort Bliss Sump system at the foot of the east side of the Franklin Mountains. The dam has a tributary area of 0.81 square mile and is 99% undeveloped mountainous desert terrain with uncontrolled flow. The remaining 1% is a housing development that is adjacent to the watershed. The dam is an earth-filled structure, approximately 63 feet high from the streambed to the top of embankment and 633 feet long. The principal outlet of the dam is a 376-foot-long, 36-inch diameter RCP pipe that empties into a stilling basin. From the stilling basin, the principal outlet discharge travels underground for approximately 1,420 feet to the Fort Bliss Diversion Channel. The auxiliary spillway is 60 feet wide with concrete crest control and flows for approximately 750 feet on undeveloped area before reaching Zircon Street. The dam was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event.

Northeast Ponding Area

The Northeast Ponding Area consists of six separate ponds: a large pond in the middle with five smaller ponds bordering on the large inner pond's exterior. The Northeast Ponding Area is located in a sump with all nearby surrounding topography draining toward the ponds. The ponds themselves are mostly below grade, so there is little to no embankment rising above the surrounding ground surface. There is no outflow system for the ponds, and the ponds are not connected by any subsurface drains. The majority of the tributary area flows into the large pond from the north through the Greenbelt Levee Channel. The Greenbelt Levee Channel conveys drainage from approximately 24 square miles of mostly undeveloped area north of the City. The Greenbelt Levee Channel also receives flow from the Western Freeway Channel, which conveys outflow from the North Hills Dams. Northeast Channels 1 and 2 also connect to the Greenbelt Levee Channel. The outer ponds receive more localized drainage. With no outflow, the inner pond of the Northeast Ponding Area was modeled in HEC-HMS as a sink with an upstream diversion that stopped routing flow once its top of embankment storage volume was reached. The outer ponds were not identified during the prioritization phase of this analysis and were not modeled individually. The total storage they provide was analyzed to estimate the potential for the large sump area to be overwhelmed and contribute flow to the southern systems. The hydrologic analysis indicates that the Northeast Ponding area would not contribute flow during the 100-year storm, and is hydrologically separate from the rest of the Northeast Region. Any future projects involving the Northeast Ponds will require additional analysis.

Northgate Dam

Northgate Dam was built by USACE in 1971 as a part of the Northgate-Range System. The dam is located on the east side the Franklin Mountains in the alluvial fan, below the foot of the mountains. The dam's embankment is roughly 50 feet tall and spans 2,700 feet, detaining a directly tributary drainage area of 1.45 square miles. In addition to the directly tributary area, the Northgate Diversion Channel and the Northgate Interceptor Channel also discharge into the Northgate Storage Basin. The channels were also constructed as a part of the 1971 project. The Northgate Diversion Channel has a drainage area of 1.29 square miles and is located on the south side of the dam area, directly above a residential neighborhood. Flow is diverted into the Northgate Basin by a 9-foot tall earthen levee that forms the south side of the channel bank. The Northgate Interceptor Channel has a drainage area of 0.60 square mile. The channel is created by a roughly 8-foot tall earthen levee and diverts an area on the north side of Northgate Dam which, without the interceptor channel, would flow over the alluvial fan down to the Patriot Freeway instead of into the Northgate Basin. Northgate Dam also receives the outflow from Fusselman Dam, which flows approximately 9,000 feet from the auxiliary spillway of Fusselman through a naturally defined alluvial channel in the Northgate Dam tributary area and into the Northgate reservoir. All drainage areas tributary to Northgate Dam are undeveloped and are of arid mountain or alluvial fan type terrain. The dam was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event.

Northhills Dams

The Northhills Dams were built in 1987 at the foot of the east side of the Franklin Mountains on the northern edge of El Paso to provide flood protection for downstream residential development. The facility is comprised of two interconnected ponds. The tributary area to the north pond is 2.44 square miles, and the tributary area to the south pond is 3.09 square miles. The principal outlet of the north pond flows through a 30-inch RCP under its shared embankment with the south pond and drains into the south pond. The principal outlet of the south pond flows through a 30-inch RCP to a culvert crossing Martin Luther King, Jr. Boulevard (MLK Blvd.) and into the War Road Channel. The northern pond's 300-foot-wide auxiliary spillway is located on its north side and outflow flows east under (and during high flows over) MLK Blvd. across mostly undeveloped area and into the Western Freeway Channel. The southern pond has three separate auxiliary spillways - 70, 90, and 320 feet wide. The dam was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event.

Range Basin

The construction date of Range Basin is unknown due to lack of available information. The basin is located just downstream of the Northgate-Range system approximately 0.70 mile from the foot of the east side of the Franklin Mountains. The basin has a tributary area of 0.39 square mile, with approximately 15% undeveloped mountainous desert terrain and 85% developed area consisting of a major road (the Patriot Freeway), single-family housing, and commercial/ industrial areas.

Range Basin is approximately 15 feet deep from the inside embankment toe to the top of embankment. It encloses approximately one large city block in area. Through inspection of the survey data points and comparison with similar basins in the northeastern El Paso area (i.e., Amber, Sunrise, and Hondo Pass Basins), Range Basin was assumed to have a 20-inch diameter pipe principal outlet connected to a storm sewer at Rutherford Road. Since other spillways of similarly sized basins have auxiliary spillways 4 feet below the top-of-dam embankment, this value was used as a check of the survey data. The auxiliary spillway was measured as a 130-foot-wide, concrete-paved spillway with a 4:1 side slope that flows onto Rutherford Road. Flow exiting Range Basin was routed to Army Ditch. The dam was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event. The stage-storage-discharge relationship was applied from the Work Order 3.

Range Dam

Range Dam was built in 1971 by USACE as part of the Northgate-Range system. The dam is located on the east side of the Franklin Mountains, just east of the Patriot Freeway, bordering the north side of Diana Drive between Dyer Street and the Patriot Freeway. Range Dam has 3.95 square miles of directly tributary area and also receives flow from the Electric Ditch Diversion Channel (0.64 square mile) and the portion of the outflow from Northgate Dam conveyed by the Northgate Outlet Channel. Range Dam's auxiliary spillway is 150 feet wide and is located on the south side of the embankment. The dam was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event.

Sunrise Basin

Sunrise Basin was constructed in 1977 as part of the Northeast Drainage Improvements project. The basin is located in the Fort Bliss Sump system approximately 0.90 mile from the foot of the east side of the Franklin Mountains. The basin has a tributary area of 0.135 square mile, with 100% developed area consisting of single-family housing and some commercial/ industrial areas. The urbanized watershed contains no defined channels. Note that the watershed was delineated without considering the area contributing to the Sunrise Drain, which collects additional flow between the principal outlet of Amber Basin and Sunrise Basin before terminating at Sunrise Basin.

Sunrise Basin is approximately 20 feet deep from the inside embankment toe to the top of embankment. It encloses approximately one city block in area. The principal outlet of Sunrise Basin is a 20-inch corrugated steel culvert pipe (CSCP), which connects to a 24-inch RCP pipe at Gateway South Boulevard, presumably part of the stormwater collection system. The auxiliary spillway is a 112-foot wide, concrete-paved spillway that flows into Gateway South Boulevard. The basin was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event.

Sunrise Dam

Sunrise Dam was constructed in 1974 by USACE and is maintained and operated by the City of El Paso. The dam is located in the Fort Bliss Sump system at the foot of the east side of the Franklin Mountains. The dam has a tributary area of 0.50 square mile, all of which is undeveloped mountainous desert terrain with uncontrolled flow. The dam is an earth-filled structure and is classified as high-hazard due to the downstream urban environment. Sunrise Dam is approximately 60 feet high from the toe to the top of embankment and is 626 feet long. The principal outlet of the dam is a 368-foot long, 36-inch diameter RCP pipe that empties into a stilling basin. From the stilling basin, the principal outlet discharge travels underground for approximately 790 feet to the upper section of the Fort Bliss Diversion Channel. The auxiliary spillway is 60 feet wide with concrete crest control and flows directly onto Zircon Street. The dam was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the basin is empty at the beginning of the storm event.

TxDOT Pond

This detention pond, located near the intersection of MLK Blvd. and War Road, was constructed in 2005. It is the only structure modeled in the Northeast Region that was not previously analyzed as part of Work Order 3. The MLK Blvd. TxDOT detention pond has a tributary area of approximately 0.6 square miles, and is approximately 17 feet deep. The pond was modeled in HEC-HMS using the stage-storage-discharge function, and the assumption that the detention basin is empty of the beginning of the storm event.

A.7.6 Significant Detention Structures, Northwest Region

Keystone Dam

Keystone Dam is a USACE dam that was constructed in 1983. The direct tributary drainage area is 3.12 square miles. Mulberry, Thorn, and Mesa Dams as well as the Borderland Channel drain to Keystone Dam. Total watershed draining to Keystone Dam is 12.8 square miles. The dam is located south of Mesa Dam, west of IH-10, and east of Doniphan Drive. The majority of the watershed is developed for residential and commercial purposes. The upper portion of the watershed is undeveloped as it is in the Franklin Mountains. Keystone Dam consists of a 66-foot high earth embankment structure at a length of 5,100 feet. The principal outlet structure is a 35-foot by 12-foot hood inlet structure that flows into a 96-inch RCP. The auxiliary spillway is an 80-foot-wide, 7-foot-deep, broad-crested weir that flows into a graded earthen channel sloped at about 1.5%. The dam was entered into HEC-HMS as a reservoir using the stage-storage-discharge function, and assuming that the dam is clean and empty at the beginning of the storm event.

Mesa Dam

Mesa Dam was constructed by the USACE in 1982. The dam is located northwest of the intersection of Mesa Street and Resler Drive. Mesa Dam's 2.88-square-mile tributary drainage area borders the southern side of Thorn Dam's tributary drainage

area. Nearly 100% of the Mesa Dam Watershed is developed, primarily residential. The dam consists of a 45-foot-high earth embankment structure, about 4,230 feet long. The principal outlet of Mesa Dam is a 14-foot by 14-foot hood inlet structure that flows to a 36-inch RCP which outlets just past the downstream toe. The auxiliary spillway is a 200-foot-wide, 7-foot-deep, broad-crested weir located directly opposite the Thorn Dam Spillway. The dam was entered into HEC-HMS as a reservoir using the stage-storage-discharge function, assuming the dam is clean and empty at the beginning of the storm event. Outflow from Mesa Dam converges with the Borderland Channel before being routed to Keystone Dam.

Mulberry Dam

Mulberry Dam was originally built by the City of El Paso in 1957. The USACE constructed improvements to the dam in 1979 to contain the Standard Project Flood (SPF). Mulberry Dam is located northwest of the Resler Drive and E. Redd Road intersection. The tributary drainage area is 4.03 square miles, approximately 70% of which is steep, undeveloped mountainous desert terrain of the Franklin Mountains, and the other 30% is mainly residential. Mulberry Dam consists of four separate embankments between natural hills. The combined length of the four embankments is roughly 1,800 feet with the largest of the embankments having a maximum height of 60 feet. The principal outlet of Mulberry Dam is a 14-foot by 14-foot hood inlet structure that flows into a 36-inch RCP which outlets into Borderland Channel. The auxiliary spillway is a 250-foot-wide, 7-foot-deep, broad-crested weir that flows into an earthen bottom trapezoidal channel. The dam was entered into HEC-HMS as a reservoir using the stage-storage-discharge function, assuming the dam is clean and empty at the beginning of the storm event. The outflow of Mulberry Dam will flow into the Borderland Channel connecting it with the Keystone Dam.

Oxidation Dam

Oxidation Dam was not included in the Work Order 3 Dam Analysis Task conducted in October 2007. Oxidation Dam is located southeast of the IH-10 and Sunland Park Drive intersection. Approximately 70% of the watershed is developed as residential and commercial with the rest being the mountainous desert terrain of the Franklin Mountains. The dam consists of a 73-foot high earth embankment structure. The principal outlet is a 14-foot by 15-foot hooded intake structure that flows into a 36-inch RCP which eventually outlets into the Rio Grande. The auxiliary spillway is a 110-foot-wide, 9-foot-deep, broad-crested weir that flows into a natural channel on the south side of the dam. Oxidation Dam was analyzed by creating a stage-storage-discharge Curve using the dam as-builds, survey data, and TxDOT 2004 contours. Oxidation Dam was entered into HEC-HMS as a reservoir using the stage-storage-discharge function, assuming the dam is clean and empty at the beginning of the storm event.

Thorn Dam

Thorn Dam was built by the City of El Paso in 1957, around the same time as Mulberry Dam. It was also enlarged and improved in 1979 by USACE to contain the SPF. It is

located just south of Mulberry Dam and east of IH-10. The tributary drainage area is 2.91 square miles and is adjacent to the south side of the Mulberry Dam tributary drainage area. Approximately 50% of the watershed is developed as residential; the rest is the mountainous desert terrain of the Franklin Mountains. Thorn Dam consists of a 39-foot-high earth embankment structure about 3,300 feet in length. The principal outlet is a 13.5-foot by 14.5-foot hooded inlet structure that flows into a 36-inch RCP which outlets just past the downstream toe into a natural channel. The auxiliary spillway is a 200-foot-wide, 7-foot-deep, broad-crested weir. Both the principal outlet and the auxiliary spillway flow into separate natural channels, which converge and flow to the Borderland Diversion Channel, where it flows to the Keystone Dam. Thorn Dam was entered into HEC-HMS as a reservoir using the stage-storage-discharge function, assuming the dam is clean and empty at the beginning of the storm event.

A.7.7 Significant Detention Structures, West Central Region

There are no major detention structures within the West Central Region.

A.8.0 MODELING OF SMALL PONDS

A.8.1 Method Overview

In addition to the significant detention structures described in Section A-7, there are a large number of ponds within each Region that would provide additional storage. For these small ponds, the storage provided was accounted for by a reduction in the SCS Curve Number as described below. The locations of these small ponds are shown on Figure A-33.

The location of each pond was determined in ArcMap, using 2006 Orthophotos for the City of El Paso (City of El Paso, 2006) and a shapefile containing points in the vicinities of ponds created as part of Work Order 1 (URS, 2007). TxDOT topography (TxDOT, 2004) data was used to estimate the volume of each pond.

Using the 100-year precipitation depth from the HEC-HMS model using the initial curve number as calculated in Section A.4.0 the watershed runoff was calculated using the following formulas:

$$Q = \frac{(P - 0.2 * S)^2}{(P + 0.8 * S)} \text{ and } S = \frac{1000}{CN} - 10$$

where:

Q = Calculated runoff (inches)
P = Precipitation (inches)
CN = Curve Number

The runoff depth obtained from the initial HEC-HMS run was then adjusted to account for the storage provided by the small ponds within each watershed. The total depth of storage over the watershed was divided by the watershed area to estimate depth of runoff that would potentially be captured. This number was then subtracted from the depth of runoff obtained from the initial run of the HEC-HMS Model with the unadjusted curve numbers to obtain the depth of runoff that might occur with the pond storage accounted for. The curve numbers were then back-calculated using this modified runoff value per the above equations.

A.8.2 Small Ponds, Central Region

The drainage area named A_Ohio_St_Reservoir_DS had a storage depth for the ponding area in the watershed that was greater than the model runoff depth for that particular drainage area. This condition resulted in a negative value for “Goal” cell (Runoff Minus Storage), causing the script not to function properly. Therefore, a Runoff Minus Storage value of 0 was entered into the spreadsheet and was used as the new “Goal” value to adjust the curve number.

Furthermore, drainage areas A_Fonseca and A_Glenwood Street 48-inch RCP have ponding areas within them which do not have storage-elevation curves. However, these drainage areas were located below IH-10 and were not modeled in the HEC-HMS model, so they did not need curve number adjustments. The adjusted curve numbers for the Central Region are provided in Table A-26 at the end of this Appendix.

A.8.3 Small Ponds, East Side Region

There are 131 small retention/detention basins in the East Side Region and all but 13 of them are within the high Mesa. The 117 retention/detention basins within the high Mesa are basins for individual subdivisions within closed watersheds and were analyzed as sumps that do not contribute any flows from the watersheds. The 13 retention/detention basins located within the escarpment zone were analyzed using as-builts for design capacity and discharge values. These small retention/detention basins did not occupy enough of the total area within their respective watersheds to have an effect on the runoff curve number.

A.8.4 Small Ponds, Mission Valley Region

Curve numbers were adjusted for 14 watersheds in the Mission Valley Region due to the capacity provided by the small ponds not modeled as reservoirs in HEC-HMS. Note that for two of the watersheds (A_Carolina Drive Basin and A_Mesa Drain), the method outlined above was altered slightly due to the total estimated pond storage capacity within the watershed being greater than the estimated model runoff storage required using the unadjusted curve numbers. For these sub-watersheds the curve number was adjusted based from a calculated runoff depth of zero, rather than a negative runoff depth. The adjusted curve numbers for Mission Valley are provided in Table A-27 at the end of this Appendix.

A.8.5 Small Ponds, Northeast Region

Curve numbers were adjusted for 12 watersheds in the Northeast Region due to the capacity provided by the small ponds not modeled as reservoirs in HEC-HMS. The adjusted curve numbers for the Northeast Region are provided in Table A-28 at the end of this Appendix.

A.8.6 Small Ponds, Northwest Region

Curve numbers were adjusted for 13 watersheds in the Northwest area due to the capacity provided by the small ponds not modeled as reservoirs in HEC-HMS. The adjusted curve numbers are provided in Table A-29 at the end of this Appendix. The "Vinton" Channels were not included in this process because the hydrology was completed with the FEMA update and analysis of the FIRMs and FIS for El Paso County.

A.8.7 Small Ponds, West Central Region

Curve numbers were adjusted for one watershed in the West Central Region, due to the capacity provided by the small ponds not modeled as reservoirs in HEC-HMS. The adjusted curve numbers are provided in Table A-30 at the end of this Appendix.

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A.9.0 ESTIMATION OF RAINFALL

Precipitation was initially estimated by assuming an SCS 24-Hour Type II-75 Rainfall Distribution as shown in Table 4-15 of the El Paso DDM (City of El Paso, 2008). Total rainfall depths found in Tables 4-1, 4-2 and 4-3 summarized in Table A-31 at the end of this Appendix of the El Paso DDM were applied to the SCS Type II-75 rainfall distribution in order to develop rain-gauge data to input directly into HEC-HMS. All preliminary hydrologic and hydraulic analysis, as well as associated quality control, was performed utilizing the above precipitation data. During the conceptual design phase and associated reviews, it became evident that the SCS Type II-75 rainfall distribution was not appropriate for the watersheds being analyzed and resulted in higher flows than would likely occur. Precipitation was then estimated utilizing the "Frequency Storm" function in HEC-HMS along with the depth-duration-frequency data located in Tables 4-1 through 4-3 of the El Paso Drainage Criteria Manual. Using this method, the user enters the depth of rainfall that occurs for various durations for a given storm. Additional inputs required include the intensity duration, the storm duration and intensity position. As a result of this modified precipitation model, flows decreased in the study areas and conceptual designs were adjusted as appropriate to accommodate the updated flows.

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A.10.0 ASSEMBLY OF HYDROLOGIC MODELS

A.10.1 Method Overview

Hydrologic models were developed for each of the six study areas. These models contained the following elements representing the major contributing drainage features of the project area:

- Watershed Area;
- Flow Diversion;
- Junction;
- Routing Reach; and
- Dam/Basin/Sump.

The Northeast, Northwest, West Central, and East Side Regions are independent and do not receive inflow from any other watersheds. The Central Region receives inflow from the Northeast Region as a source. Similarly, the Mission Valley Region receives input from the East Side Region. The specific approaches and assumptions used to model the various elements can be found in the individual study area descriptions.

A.10.2 Hydrologic Model, Central Region

The Central Region was modeled as three basins in HEC-HMS and is shown on Figures A-34 through A-41 at the end of this Appendix. The three systems are the Cebada, Government Hills, and Dallas Systems. The figures illustrate the HEC-HMS layout of the systems and show all drainage areas, reaches, junctions, diversions, sources, and reservoirs input into HEC-HMS. Additionally, tables are provided listing model elements and 100-year flow results.

Cebada System

The Cebada System consists of twenty-one different drainage areas, one diversion, eight junctions, twelve reaches, and twelve dams or reservoirs. The dams and reservoirs in this system include Altura Avenue Dam, Cebada Reservoir, Fort Blvd Reservoir, Lower Kentucky Dam, Upper Kentucky Dam, Lower Louisiana Drive Dam, Magnolia Reservoir, Lower Memphis Dam, Ohio Street Reservoir, San Diego Dam, Scenic Drive Dam, and Tremont Reservoir.

The diversion in this system is located just north of Houston Elementary School and is labeled D_Houston_Elementary. Street drainage inlets capture flow from north of the school and direct it towards Magnolia Reservoir. The maximum capacity of the storm sewer system is 250 cfs after that capacity is reached, the excess flow is diverted south, towards the Cebada Reservoir.

The outflow from Fort Blvd Reservoir is routed to Copia Ditch through the streets and eventually enters the Cebada Drainage Outfall, south of Memorial Park. The conduit

conveys flow beneath the Cebada Reservoir and into the Cebada Reservoir Outfall Junction.

Dallas System

The Dallas System includes flow directed towards the reservoir located at the intersection of Cotton Street, Dallas Street, and IH-10 (S_Dallas_Reservoir). The HEC-HMS model for this system includes five drainage areas, two diversions, five junctions, three reaches, and four dams or reservoirs. The dams and reservoirs included in this basin model are Dallas Reservoir, Dam No. 8, Dam No. 9, and Dam No. 10.

The Campbell Reservoir, located on the western edge of the Central Region was not incorporated into the HEC-HMS model because it was assumed that Campbell Reservoir would be able to retain all inflow and not release into the Cebada System during the storm event.

The 3708 Diversion was used to divert street drainage which can no longer enter the drainage inlets at the curbs of the streets once the water elevation in the Dallas Reservoir reaches an elevation of 3,708 feet. At this elevation, the reservoir is discharging at a maximum capacity of 530 cfs. The excess street flow is diverted south of IH-10, via Cotton Street, and begins to pool next to the railroad tracks. The destination of this diverted flow is defined as the junction, J_Overflow_3708.

The Dallas Reservoir includes an east and a west reservoir, which are connected and fill up simultaneously, but direct flows into two different storm sewer systems. The east and west storm conduits receiving flow from the Dallas Reservoir are represented by the Diversion Junction and the Dallas West Junction, respectively, in the HEC-HMS model.

Another diversion (D_IH_10_Dallas) is used to distinguish how much outflow leaves the eastern side of the Dallas Reservoir and how much exits from the western side. Flows entering the reservoir are diverted to either the west or the east outlet conduits depending on the elevation of the overall reservoir. The conduit on the west begins to discharge once the water level in the entire Dallas Reservoir reaches an elevation of 3,700 feet. Once the water level reaches an elevation of 3,702 feet, the eastern reservoir begins to discharge.

Government Hills System

The Government Hills System consists of eighteen drainage areas, one diversion, eight junctions, thirteen reaches, ten dams or reservoirs, and one source. The source included is a discharge gauge from the Northeast Region, which conveys flow from Fort Bliss Sump into Pershing Dam. This discharge information was obtained from the output of the Northeast Region's HEC-HMS model. The diversion used in this system is the Boon Street Basin, which conveys flow into the Government Hill Outlet Conduit until the capacity of the conduit (375 cfs) is reached. Then the excess flow is diverted into

the Upper Durazno Basin through an arch-shaped culvert located at a higher elevation than the Government Hill Outlet Conduit. The Upper Durazno Basin drains into the Lower Durazno Basin through two 10-foot by 10-foot box culverts. The Lower Durazno Basin outflows south of IH-10 through a drop spillway and an auxiliary spillway, into a junction labeled J_Lower Durazno_Out on the HEC-HMS model.

The Government Hills System was the only basin model which includes drainage areas south of IH-10. However, only the drainage areas which contribute to flow from the Government Hill Outlet Conduit (A_Concordia_Cemetery and A_Hardesty_to_Shelter) were modeled below IH-10. The Government Hill Outlet Conduit eventually discharges into the Rio Grande, which is symbolized by the junction, J_Gov_Hills_Outfall in the HEC-HMS model.

A.10.3 Hydrologic Model, East Side Region

The East Side Region drainage systems are characterized by three different drainage patterns and land types. The drainage patterns for the East Side Region are very different from those of the rest of the City. They are characterized by the high mesa, the escarpment zone, and the IH-10 corridor. For a majority of the watersheds in the East Side Region, the Work Order 1 watersheds were modified for the drainage characteristics most abundant in the East Side Region, the high Mesa.

The high Mesa is a relatively flat area that consists of many closed drainage systems. These closed systems contain flows that fall within them and percolate into the groundwater system. Most of the flow in this area is routed through the streets into retention basins. The older developments in the area typically have one large retention basin to capture all the flow for a large area. When the area is too large and flow has a long distance to travel over flat terrain, it quickly becomes a problem within the streets. This is typical of the high Mesa west of George Dieter Drive to Central El Paso. East of George Dieter Drive, newer developments have been required to retain the developed flows. This has alleviated flooding of the streets.

The escarpment zone is the area where the terrain steepens and falls away from the high Mesa. The increase in slope causes an increase in velocity; the risk for erosion and flood damage caused by fast moving water also increases. This is the area most likely to see erosion and sediment transport problems.

At about midway down the escarpment zone IH-10 was constructed. IH-10 acts as a drainage barrier for the flows coming down the escarpment zone. This is where the amount of impervious area is in the highest concentration due to the large volume of commercial and industrial sites adjacent to IH-10. In interviews with TxDOT and the City of El Paso, it has been reported that there are many problem areas along the IH-10 Corridor as well as complaints from the public and commercial owners. These areas include the IH-10 corridor intersections from the McRae Boulevard to south of Loop 375.

The East Side Region was modeled as six basins in HEC-HMS and is shown on Figures A-42 through A-45 at the end of this Appendix. These systems include the Phelps Dodge System, Lomaland Basin System, Americas Basin System, Americas Ten Basin System, Carolina Dam Basin System, and the Mesa Drain Downstream System.

Phelps Dodge System

The Phelps Dodge System is characterized with all three of the different zones within the East Side Region: the high Mesa zone, escarpment zone, and IH-10 Corridor. HEC-HMS was used to calculate the peak flows for areas within the high Mesa that are closed basins. This flow was not routed to any structures or to any other watersheds. It was only used to get a peak intensity and volume for each basin. The basins with large localized flooding areas were broken down further to isolate the localized flooding problem areas and potential improvement projects, as requested by EPWU.

The escarpment zone and IH-10 Corridor within the Phelps Dodge System has previously been studied by TxDOT. The flows from the North Loop Drainage Study will be referenced and used with permission from TxDOT in conjunction with the EPWU for this master plan.

Lomaland Basin System

The Lomaland Basin System contains all three zones and is just east of the Phelps Dodge System. HEC-HMS was used to calculate the peak flows for areas within the high Mesa that are closed basins. This flow was not routed to any structures or to any other watersheds. It was only used to get a peak intensity and volume for each basin. The basins with large localized flooding areas were broken down further to isolate the localized flooding problem areas and potential improvement projects, as requested by EPWU, for this master plan.

The escarpment zone in the Lomaland Basin System was analyzed and peak flows are routed under IH-10. There are areas that have localized flooding issues because of the slopes and drainage structures that were not designed for the amount of flow they are receiving. Improvements have been constructed near Lee Trevino Drive and Jesuit Basin to improve the drainage there. Even with the newly implemented improvements, drainage impacts still exist at Lee Trevino Drive and James Watt Drive. There are more drainage impacts as flow travels down Lee Trevino Drive, between Rojas Drive and James Watt Drive, that will be analyzed with greater detail as requested by EPWU. IH-10 and the frontage roads experience localized flooding at Lee Trevino Drive because of flows routed to, and accumulating around crossings, flooding streets, and local businesses.

Americas Basin System and Americas Ten Basin System

The Americas Basin System and the Americas Ten Basin System include all three drainage zones but have a large number of retention ponds built into the urban infrastructure. In the high Mesa, the ponds are numerous and handle flows from the development without any major drainage problems reported. This however, is not the case within the escarpment zone.

The escarpment zone within the Americas Basin System and Americas Ten Basin System has several areas that have frequent flooding. The flows in this area were analyzed using HEC-HMS and routing basins into the large channels and through the IH-10 Corridor. There are three large channels in this area: the Bluff Channel, the RV Channel, and the Mercantile Channel. The Bluff Channel has a large area contributing flows with high velocities. Some of the flows upstream of the Bluff Channel are being impeded and thus cause flooding before entering the channel. These are potential areas for drainage improvements. These areas will be further analyzed as requested by EPWU.

The RV Channel and the Mercantile Channel are large channels that receive flows from large areas upstream beginning in the high Mesa and travel relatively long distances through the escarpment areas increasing in velocity and volume. This large amount of water, traveling at a high rate of speed, causes erosion problems downstream. These are potential areas for drainage improvements to reduce the energy within the flow paths.

Carolina Dam Basin

The IH-10 Corridor, for these two basin systems, was previously studied by TxDOT. The flows from the study *Drainage Study and Report (Existing Conditions) for Interstate Highway 10* (MCi, February 2008) will be referenced in our report with permission from TxDOT in conjunction with EPWU.

The Carolina Dam Basin System starts just north of the IH-10 Corridor within the escarpment area. HEC-HMS was used to analyze the amount of flow from this watershed that enters the Lafayette Draw Channel. This channel crosses under IH-10 into Mission Valley Region.

Mesa Drain Downstream System

The Mesa Drain Downstream System starts within the escarpment zone north of IH-10 and is mostly contained on the south side of IH-10 within Mission Valley Region. HEC-HMS was used to analyze approximately 750 acres contributing flows under IH-10 into Mission Valley Region.

A.10.4 Hydrologic Model, Mission Valley Region

The Mission Valley Region was modeled as one basin model in HEC-HMS and is shown on Figures A-46 and A-47 at the end of this Appendix. These figures illustrate

the HEC-HMS layout of the system and show all drainage areas, reaches, junctions, diversions, sources, and reservoirs input into HEC-HMS. Additionally, tables are provided listing model elements and 100-year flow results. The Mission Valley system consists of thirty different drainage areas, nineteen junctions, twenty-seven reaches, nine dams or basins, four diversions, and nine source inputs. The basins included in the system are Americas Basin System, Americas Ten Basin System, Basin A, Basin G, Carolina Drive Basin, Feather Lake Basin, Lomaland Basin System, North Loop Detention Basin, and Phelps Dodge System.

Lincoln drain, residing in the northwestern region of Mission Valley, receives a source input flow from the Central Region. All eight other source inputs to Mission Valley are from the East Side Region above IH-10. Note that the source inputs from the East Side Region were not routed to the various downstream dams, but were rather input directly to the corresponding downstream dam. This was done for model simplification, as the purpose of the Mission Valley Model was to focus on the main drains (Mesa, Middle, Franklin, and Playa Drains), the Interceptor System, and Basin G. This simplification provides a more conservative estimate of flow into the dams since routing often attenuates the peak flow.

Other modeling points of interest include the configuration of Basin A. At the junction of Basin A with Playa Drain, there is a 42-inch culvert along Playa Drain in the direction of flow. Flow is diverted into the Playa Drain 42-inch culvert based on the water surface elevation of the upstream channel while the remaining flow gets directed into Basin A. Basin A was modeled as having two outlets and three pumps. The pumps' intake elevation is at 3,675 feet and the discharge elevation is at 3,675 feet. The first pump turns on at an elevation of 3,681 feet and shuts off at 3,680 feet. Pump two starts pumping at an elevation of 3,681.5 feet and shuts off at 3,680.5 feet. The third pump turns on at 3,682 feet and shuts off at 3,681 feet.

Three other diversions exist at the junction of Mesa Drain and the Mesa Drain Interceptor: the Middle Drain and Middle Drain interceptor, and at the Playa Drain and Franklin Spur Drain. These first two diversions (Mesa and Middle) are currently place holders to indicate the presence of the 36-inch gated culvert that exists at each of those areas. Since the gates are not to be used as a stormwater control option for the City of El Paso, the gates were assumed closed, meaning all flow transitions to the corresponding interceptor drain (i.e. Mesa Drain to the Mesa Drain Interceptor and Middle Drain to the Middle Drain Interceptor). The "diverted flow," or flow through the gate, was set to zero. The diversion at the Playa Drain and Franklin Spur Drain is also used as a place holder. This diversion is a situation where the slope back to Basin G is negative. Therefore, the main flow continues down the Franklin Spur Drain from the Playa Drain, while no flow is diverted off towards Basin G.

A.10.5 Hydrologic Model, Northeast Region

The Northeast Region was modeled as one basin model in HEC-HMS and is shown on Figures A-48 and A-49 at the end of this Appendix. These figures illustrate the HEC-HMS layout of the system and show all drainage areas, reaches, junctions, diversions, sources, and reservoirs input into HEC-HMS. The Northeast Region consists of fifty-one different drainage areas, thirty-four junctions, twenty-six reaches, nineteen dams or sinks, and five diversions. A model for this region was generated previously as part of the *Drainage On-Call Services: Dam Analysis Report* and served as the basis for the model utilized in this analysis.

The dams included in the Northeast Region area are described in Section A.7.0. The Northeast Region is divided into three drainage systems including the Northeast Ponding System, the Range Dam System, and the Fort Bliss Sump System. A schematic illustrating the HEC-HMS model schematic and tables listing model elements and 100-year flows are provided on Figures A-48 and A-49.

The Northeast Ponding System is the most upstream system and includes the Northhills Dams, the TxDOT Pond, and Northeast Ponding Area. Outflow from the Northhills dams is routed through the Western Freeway Channel, to the Green Belt Levee System, and into the Northeast Ponding Inner Pond. Flows are also routed to the Northeast Inner Pond via Northeast Channels One and Two. The Northeast Ponding Area is modeled in HEC-HMS such that if the storage capacity of the sump is reached, flow would begin contributing to the Fort Bliss Sump System. In the conditions modeled, the Northeast Ponding system does not contribute flow to the southern systems.

The Range Dam System includes Range Dam, Fusselman Dam, and Northgate Dam. Outflow from Fusselman Dam is routed via a natural arroyo to Northgate Dam. Also contributing to Northgate Dam are the Northgate Interceptor Channel and the Northgate Diversion Channel. Outflow from Northgate Dam is routed downstream to Range Dam. Range Dam receives additional flow from its own tributary watershed, as well as the Electric Ditch Diversion Channel.

Outflow from Range Dam enters the Fort Bliss Sump System and is connected downstream to a diversion in order to model the separate flowpaths of the principal and auxiliary spillways. Flow is directed through the principal spillway until the elevation reaches the auxiliary spillway at which point flow is also conveyed through the auxiliary spillway according to the stage-storage-discharge curves generated as part of the *Dam Analysis Report*. Outflow from the auxiliary spillway is routed to Range Basin and outflow from the principal spillway is routed to Range Dam Outlet Channel, which is also called Army Ditch. All outflow from Range Dam is then routed to the Threadgill or Tobin Drain and eventually makes its way down to the Fort Bliss Sump. Fort Bliss Sump receives additional flow from Mountain Park and Sunrise Dam, Keltner Dam, and Hondo Pass Basin, Sunrise Basin and Amber Basin. Outflow from Mountain Park and Sunrise

Dam is conveyed via the Fort Bliss Diversion Channel to Diana Ditch and into Fort Bliss Sump. Outflow from Kelter Dam is routed overland directly to Fort Bliss Sump, and outflow from the small basins included in this system is routed via Sunrise Channel to Fort Bliss Sump. Other channels with hydrologic watersheds analyzed include Johnson Channel, Railroad Drive Channel, and Clearview (a.k.a. Bossworth) Channel. Once in Fort Bliss Sump, a diversion is used to convey flow into the sump until the maximum storage available is reached, and then direct flow into the outer sump area surrounding the sump itself. This diversion was necessary to model the PMF conditions, which was the goal of the *Dam Analysis Report*. However, in the conditions modeled for this study, the capacity of Fort Bliss Sump is sufficient and flow does not enter the outer sump. The only outflow from Fort Bliss Sump is through the Fort Bliss Outlet Conduit.

A.10.6 Hydrologic Model, Northwest Region

The Hydrologic Model for the Northwest Region was assembled in HEC-HMS Version 3.2, using the method described above. The schematics of the HEC-HMS model are provided on Figures A-50 through A-55 at the end of this Appendix. Specific assumptions that were made while assembling the HEC-HMS model are mentioned below with explanations.

Resler Channel is located south of Transmountain Road and north of Artcraft Road. It begins in the Franklin Mountains and terminates at its confluence with Flow Path 38. After the channel exits the foothills it splits into two separate channels; Resler Channel continues in a southwesterly direction and Flow Path 39A goes slightly northwest. As it is not really known which path the runoff will take, and it probably varies from year to year, it was decided to route 100% of the flow from the upstream watershed through both the downstream channels.

Flow Number 39A has a similar situation between Northwestern Drive and Resler Drive. The natural channel flows in a northwesterly direction until it reaches an earthen diversion berm east of the commercial development along Northwestern Drive, where it is redirected almost 90 degrees to the north. The berm has been blown out during previous major storm events. Therefore it was decided to model the flow going through both the diversion channel and the flow path taken if the barrier is blown out.

The "Vinton" Channels were not included in the hydrologic modeling, because the hydrology was completed with the FEMA update and analysis of the FIRMs and FIS for El Paso County.

A.10.7 Hydrologic Model, West Central Region

The Hydrologic Model for the West Central Region was assembled using the method described above. The schematics of the HEC-HMS model are provided on Figure A-56 at the end of this Appendix.

A.11.0 MODEL RESULTS

Model results for each of the six regions studied can be found in Tables A-32 through A-37 located at the end of this Appendix. Figure numbers for the corresponding HEC-HMS schematics and element tables are provided as well.

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TABLES

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Table A-1. Data Sources Utilized in Hydrologic Analysis

| Source | Used For |
|---|---|
| Ashley G. Classen & Associates Consulting Engineers, 1948. Drainage Control Works. | Significant Detention Structures |
| Brock & Bustillos, Inc., 2007. Cebada & IH-10 Preliminary Master Study. | Watershed Delineation |
| City of El Paso, 2008. <i>El Paso Drainage Design Manual (DDM)</i> . | Precipitation |
| City of El Paso, 2006. Orthophotography. | Watershed Delineation Curve Number Lag Time |
| City of El Paso, 1987. Engineering Department Flood Control System, Base Map Series. | Watershed Delineation |
| El Paso Water Utilities (EPWU), 2008. Drainage Shapefile (Incomplete) | Routing |
| ESRI ArcView, Version 9.2 | All Parameters |
| Moreno Cardenas Inc. (MCi), February 2008. Drainage Study and Report (Existing Conditions) for Interstate Highway 10. | |
| MCi, 2007. Northloop Study. | Watershed Delineation |
| MCi, 2007. Dallas St. Pump and Drainage System, Preliminary Engineering Report. | Watershed Delineation |
| Texas Department of Transportation (TxDOT), 2007. Plans of Proposed Highway Routine Maintenance Contract. | Significant Detention Structures |
| TxDOT, 2005. FM 3255 (MLK JR BLVD), Plans for Proposed State Highway Improvement. | Significant Detention Structures |
| TxDOT, 2004. Topography. El Paso Office. | Watershed Delineation Lag Time |
| United States Army Corp of Engineers (USACE), HEC-HMS, V. 3.1.0. | HEC-HMS |
| USACE, March 2000. HEC-HMS Technical Reference Manual. | HEC-HMS |
| USACE, February 1978. Report on Hydrologic Investigations Flood Insurance Study-Northeast and Central El Paso, Texas. Albuquerque District. | Lag Times |
| United States Department of Agriculture (USDA), June 1986. Soil Conservation Service, Engineering Division, Technical Release 55 (TR-55). <i>Urban Hydrology for Small Watersheds</i> . | Curve Number |
| USDA National Resource Conservation Commission (NRCS), 2004. Soil Survey Geographic Database (SSURGO) Soil Data for El Paso County, Texas. | Curve Number |
| URS Corporation (URS), 2008. Electronic Data - Appendix E, Dam Analysis Report, Drainage On-Call Services, Task 3 of Work Order 3. | Significant Detention Structures |
| URS, 2007. Electronic Data-Appendix I, Drainage System Evaluation and Audit Report, Drainage On-Call Services, Work Order 1. | Routing Geometry |

Table A-2. Hydrologic Soil Groups in the El Paso Region

| EL PASO HYDROLOGIC SOIL GROUPS | | |
|--|--------------------------|------------|
| Soil Type | Soil Abbreviation | HSG |
| Hueco-Wink association, hummocky | HW | C |
| Anapra silty clay loam | An | B |
| Brazito loamy fine sand | Br | A |
| Gila fine sandy loam | Ga | B |
| Gila loam | Gc | B |
| Glendale loam | Gd | B |
| Glendale silty clay loam | Ge | B |
| Glendale silty clay | Gs | B |
| Harkey loam | Ha | B |
| Harkey silty clay loam | Hk | B |
| Made land, gila soil material | Mg | B |
| Saneli silty clay loam | Sa | D |
| Saneli silty clay | Sc | D |
| Tigua silty clay | Tg | D |
| Vinton fine sandy loam | Vn | B |
| Turney-Berino association, undulating | TBB | B |
| Agustin association, undulating | AGB | B |
| Badlands | BA | D |
| Bluepoint association, rolling | BPC | A |
| Bluepoint gravelly association, rolling | BUC | A |
| Delnorte-Canutio association, undulating | DCB | D |
| Delnorte-Canutio association hilly | DCD | D |
| Dune land | DU | A |
| Igneous rock land | IG | D |
| Igneous rockland-Brewster association | IN | D |
| Rock outcrop-Lozier association | LM | D |
| Lozier association, hilly | LOD | D |
| Mimbres association, level | MBA | B |
| Pajarito association, level | PAA | B |
| Simona association, undulating | SMB | D |
| Wink association, level | WKA | B |
| Water | W | W |
| Urban land, sanitary landfill | SLF | SINK |
| Pits, gravel | GP | SINK |

Table A-3. Runoff Curve Numbers for Urban Areas

| Hydrologic Soil Group | | A | B | C | D |
|--------------------------------|------|----|----|----|----|
| Open Space | Poor | 68 | 79 | 86 | 89 |
| | Fair | 49 | 69 | 79 | 84 |
| | Good | 39 | 61 | 74 | 80 |
| Commercial and Business | NA | 89 | 92 | 94 | 95 |
| Industrial | NA | 81 | 88 | 91 | 93 |
| Residential (1/8 acre or less) | NA | 77 | 85 | 90 | 92 |
| Residential (1/4 acre) | NA | 61 | 75 | 83 | 87 |
| Residential (1/2 acre) | NA | 54 | 70 | 80 | 85 |
| Residential (1 acre) | NA | 51 | 68 | 79 | 84 |
| Newly graded areas | NA | 77 | 86 | 91 | 94 |
| Highway | NA | 98 | 98 | 98 | 98 |

Table A-4. Runoff Curve Numbers for Arid and Semi Arid Rangelands

| Hydrologic Soil Group | | A | B | C | D |
|-----------------------|------|----|----|----|----|
| Herbaceous | Poor | | 80 | 87 | 93 |
| | Fair | | 71 | 81 | 89 |
| | Good | | 62 | 74 | 85 |
| Oak-aspen | Poor | | 66 | 74 | 79 |
| | Fair | | 48 | 57 | 63 |
| | Good | | 30 | 41 | 48 |
| Pinyon-juniper | Poor | | 75 | 85 | 89 |
| | Fair | | 58 | 73 | 80 |
| | Good | | 41 | 61 | 71 |
| Sage-grass | Poor | | 67 | 80 | 85 |
| | Fair | | 51 | 63 | 70 |
| | Good | | 35 | 47 | 55 |
| Desert Shrub | Poor | 63 | 77 | 85 | 88 |
| | Fair | 55 | 72 | 81 | 86 |
| | Good | 49 | 68 | 79 | 84 |

Table A-5. Land Use Categories for Urban Areas

| Land Use Description | Hydrologic Condition | Land Use ID |
|--|-------------------------------|-------------|
| Open Space (lawns, parks, golf courses, cemeteries) | Poor (grass cover <50%) | 1 |
| | Fair (grass cover 50% to 75%) | 2 |
| | Good (grass cover >75%) | 3 |
| Commercial and Business | NA | 10 |
| Industrial | NA | 20 |
| Residential (1/8 acre or less, townhouses) | NA | 30 |
| Residential (1/4 acre) | NA | 31 |
| Residential (1 acre) | NA | 33 |
| Residential (2 acres) | NA | 34 |
| Newly graded areas (no vegetation, pervious area only) | NA | 40 |
| Highway | NA | 99 |

Table A-6. Land Use Categories for Rural Areas

| Land Use Cover Type | Hydrologic Condition | Land Use ID |
|---|----------------------|-------------|
| Herbaceous: mixture of grass, weeds, and low-growing brush, with brush the minor element | Poor | 50 |
| | Fair | 51 |
| | Good | 52 |
| Oak-aspen: mountain brush mixture of oak brush, aspen, mountain mahogany, bitter brush, maple, and other brush | Poor | 60 |
| | Fair | 61 |
| | Good | 62 |
| Pinyon-juniper: pinyon, juniper, or both: grass understory | Poor | 70 |
| | Fair | 71 |
| | Good | 72 |
| Sagebrush with grass understory | Poor | 80 |
| | Fair | 81 |
| | Good | 82 |
| Desert shrub: major plants include saltbush, greasewood, creosote brush, black brush, bursage, palo verde, mesquite, and cactus | Poor | 90 |
| | Fair | 91 |
| | Good | 92 |

Table A-7. Curve Number Summary for the Central Region

| CENTRAL REGION - CURVE NUMBER SUMMARY | | |
|--|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| A_Alameda Avenue | 0.30 | 83 |
| A_Altura_Ave_Dam | 0.12 | 84 |
| A_Blanco Avenue | 0.09 | 90 |
| A_Boone_St_Basin | 0.40 | 83 |
| A_Border_Hwy_Overpass | 0.37 | 92 |
| A_Cebada Drainage Outfall | 0.27 | 84 |
| A_Cebada_Reservoir | 0.70 | 86 |
| A_Cemex_Spillway | 0.92 | 89 |
| A_Channel 108 Discharge | 0.03 | 86 |
| A_Comanche Avenue | 0.14 | 85 |
| A_Concordia_Cemetery | 0.31 | 84 |
| A_Copia_Ditch_DS | 0.16 | 92 |
| A_Copia_Ditch_US | 0.41 | 91 |
| A_Cotton_Dallas_DS | 0.37 | 92 |
| A_Cotton_Dallas_US | 1.05 | 91 |
| A_Dallas, San Antonio and Lee | 0.18 | 91 |
| A_Dam_No_10 | 0.07 | 88 |
| A_Dam_No_8 | 0.05 | 85 |
| A_Dam_No_9 | 0.03 | 89 |
| A_Delta Drive | 0.08 | 82 |
| A_El Paso Paisano to Ninth Outfall | 0.16 | 92 |
| A_Eucalyptus_to_Cebada | 0.23 | 94 |
| A_Fonseca | 0.26 | 82 |
| A_Fort_Blvd_Reservoir | 0.22 | 84 |
| A_Franklin_Campbell | 0.26 | 94 |
| A_Glenwood Street | 0.06 | 75 |
| A_Hardesty to Shelter | 0.02 | 88 |
| A_Hills Delta to Ninth | 0.09 | 87 |
| A_Houston_Elementary | 0.50 | 91 |
| A_Kentucky_Dam_Lower | 0.12 | 85 |
| A_Kentucky_Dam_Upper | 0.06 | 87 |
| A_Louisiana_Dr_Dam_Lower | 0.05 | 89 |
| A_Louisiana_Dr_Dam_Upper | 0.14 | 85 |
| A_Lower_Durazno | 1.04 | 71 |
| A_Magnolia_Reservoir | 0.09 | 67 |
| A_McKelligon_Dam | 2.17 | 86 |
| A_McKelligon_Reservoir_A | 0.04 | 87 |
| A_McKelligon_Reservoir_B | 0.10 | 87 |
| A_McKelligon_Reservoir_C | 0.01 | 84 |
| A_McKelligon_Reservoir_D | 0.01 | 93 |
| A_Memorial_Park | 0.15 | 90 |

Table A-7. Curve Number Summary for the Central Region (Continued)

| CENTRAL REGION - CURVE NUMBER SUMMARY | | |
|--|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| A_Memphis_Dam_Lower | 0.01 | 84 |
| A_Memphis_Dam_Upper | 0.25 | 84 |
| A_Modesto Ditch | 0.12 | 82 |
| A_Mountain_Ave_Outlet_Conduit | 0.88 | 91 |
| A_Nixon Cypress to Central | 0.05 | 87 |
| A_Noble Myrtle to San Antonio | 0.03 | 91 |
| A_Octavia Texas to Magoffin | 0.07 | 92 |
| A_Ohio_St_Reservoir_DS | 0.00 | 89 |
| A_Ohio_St_Reservoir_US | 0.01 | 88 |
| A_Olive & Cebada takes flow ponds at IH-10 | 0.46 | 90 |
| A_Overland Mesa to El Paso | 0.01 | 92 |
| A_Paisano and Delta Stanton to Tays | 0.20 | 91 |
| A_Paisano Ditch | 0.22 | 83 |
| A_Paisano San Francisco to El Paso | 0.15 | 91 |
| A_Pera to Cebada | 0.23 | 91 |
| A_Pershing_Dam | 0.19 | 81 |
| A_Pollard_Ditch | 0.11 | 93 |
| A_Pollard_Sacramento | 0.02 | 92 |
| A_Robert Alva Channel | 0.44 | 78 |
| A_Russel_Ditch_DS | 0.12 | 91 |
| A_Russel_Ditch_US | 0.43 | 92 |
| A_San Antonio Hills to Lee | 0.15 | 89 |
| A_San Antonio Mesa to El Paso | 0.08 | 93 |
| A_San_Diego_Dam | 0.12 | 85 |
| A_Scenic_Dr_Dam | 0.13 | 84 |
| A_Seventh and Hills Park to Ninth | 0.34 | 89 |
| A_Seventh Chihuahueta to St Vrain East | 0.15 | 90 |
| A_Seventh Chihuahueta to St Vrain West | 0.07 | 89 |
| A_Tremont_Reservoir | 0.01 | 90 |
| A_Upper_Durazno | 0.02 | 79 |
| A_Van_Buren_Dam | 0.28 | 91 |
| A_Van_Buren_Ditch | 0.12 | 87 |

Table A-8. Curve Number Summary for the East Side Region

| EAST SIDE REGION - CURVE NUMBER SUMMARY | | |
|--|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| A_PHELPSDODGE-1 | 0.038 | 84 |
| A_PHELPSDODGE-2 | 0.149 | 94 |
| A_PHELPSDODGE-3 | 0.093 | 83 |
| A_PHELPSDODGE-4 | 0.037 | 76 |
| A_PHELPSDODGE-5 | 0.082 | 85 |
| A_PHELPSDODGE-6 | 0.133 | 82 |
| A_PHELPSDODGE-7 | 0.047 | 82 |
| A_PHELPSDODGE-8 | 4.475 | 81 |
| A_PHELPSDODGE-9 | 6.086 | 81 |
| A_PHELPSDODGE-10 | 1.915 | 81 |
| A_Lomaland-1 | 0.038 | 83 |
| A_Lomaland-2 | 0.206 | 74 |
| A_Lomaland-3 | 0.035 | 75 |
| A_Lomaland-4 | 0.107 | 83 |
| A_Lomaland-5 | 0.055 | 84 |
| A_Lomaland-6 | 0.082 | 84 |
| A_Lomaland-7 | 0.456 | 83 |
| A_Lomaland-8 | 0.053 | 70 |
| A_Lomaland-9 | 0.080 | 77 |
| A_Lomaland-10 | 0.034 | 88 |
| A_Americas-1 | 0.176 | 82 |
| A_Americas-2 | 0.819 | 82 |
| A_Americas-3 | 0.174 | 83 |
| A_Americas-4 | 0.016 | 82 |
| A_Americas-5 | 0.096 | 85 |
| A_Americas-6 | 0.144 | 61 |
| A_Americas-7 | 0.016 | 65 |
| A_Americas-8 | 0.052 | 80 |
| A_Americas-9 | 0.157 | 70 |
| A_Americas-10 | 0.032 | 79 |
| A_Americas-11 | 0.086 | 69 |
| A_Americas-12 | 0.047 | 82 |
| A_AmTen-1 | 0.075 | 84 |
| A_AmTen-2 | 0.307 | 87 |
| A_AmTen-3 | 0.095 | 83 |
| A_AmTen-4 | 0.502 | 85 |
| A_AmTen-5 | 0.064 | 84 |
| A_AmTen-6 | 1.503 | 82 |
| A_AmTen-7 | 2.317 | 82 |

Table A-8. Curve Number Summary for the East Side Region (Continued)

| EAST SIDE REGION - CURVE NUMBER SUMMARY | | |
|--|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| A_CarolinaDam-1 | 0.354 | 65 |
| A_MesaDrain-1 | 0.097 | 68 |
| A_MesaDrain-3 | 0.202 | 89 |
| A_Sunmount | 0.029 | 82 |
| A_MesaDrain_UP | 0.022 | 87 |
| A_RLH_2 | 0.013 | 78 |
| A_Lomaland_4a | 0.010 | 83 |
| A_CarolinaDam-2 | 0.102 | 89 |
| A_LOMALAND_8A | 0.036 | 77 |
| A_MesaDrain_2 | 0.100 | 75 |
| A_MesaDrain_4 | 0.072 | 76 |
| A_PhelpsDodge_1a | 0.016 | 88 |

Table A-9. Curve Number Summary for the Mission Valley Region

| MISSION VALLEY REGION - CURVE NUMBER SUMMARY | | |
|---|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| A_Americas Basin | 0.50 | 71 |
| A_Americas Ten Basin | 0.26 | 56 |
| A_Americas Ten NonContribute | 0.09 | 50 |
| A_Basin A | 1.42 | 75 |
| A_Basin G | 0.36 | 87 |
| A_Below Basin G to Cty Limit | 1.88 | 80 |
| A_Below Carolina Dam | 1.02 | 76 |
| A_Below Featherlake Basin | 0.15 | 69 |
| A_Below Phelps Dodge Basin | 1.39 | 49 |
| A_Carolina Drive Basin | 0.29 | 38 |
| A_Feather Lake Basin | 0.70 | 44 |
| A_Franklin Drain A | 0.67 | 86 |
| A_Franklin Drain B | 0.91 | 81 |
| A_Franklin Drn to City Limit | 2.88 | 76 |
| A_Franklin Spur Drain | 0.11 | 80 |
| A_Lincoln Drain | 2.33 | 78 |
| A_Lomaland Basin | 0.66 | 62 |
| A_Mesa Drain A | 0.66 | 38 |
| A_Mesa Drain B | 0.74 | 63 |
| A_Mesa Drain C | 3.18 | 58 |
| A_Mesa Drain to City Limit | 0.80 | 72 |
| A_Middle Drain A | 4.31 | 69 |
| A_Middle Drain B | 0.12 | 88 |
| A_Middle Drain Spur A | 0.05 | 85 |
| A_Middle Drain Spur B | 0.07 | 87 |
| A_Middle to City Limit | 1.01 | 80 |
| A_North Loop Detention Basin | 1.13 | 44 |
| A_Phelps Dodge Basin | 1.08 | 72 |
| A_Playa Drain A | 0.57 | 79 |
| A_Playa Drain B | 5.84 | 70 |

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Table A-10. Curve Number Summary for the Northeast Region

| NORTHEAST REGION - CURVE NUMBER SUMMARY | | |
|--|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| A_Amber Basin | 0.25 | 87 |
| A_Army Ditch | 0.42 | 82 |
| A_Bossworth Ch D/S | 0.12 | 87 |
| A_Bossworth Ch U/S | 0.42 | 86 |
| A_Diana Ditch D/S | 1.86 | 83 |
| A_Diana Ditch U/S Sunrise Ch | 0.96 | 83 |
| A_E Fwy Ch | 1.67 | 72 |
| A_Electric Ditch | 0.63 | 82 |
| A_Fairbanks Drive | 1.11 | 81 |
| A_Fort Bliss Diversion Ch | 0.17 | 88 |
| A_Ft Bliss Diversion Channel D/S | 24.62 | 83 |
| A_Ft Bliss Diversion Channel U/S | 0.15 | 86 |
| A_Fusselman Dam | 3.37 | 83 |
| A_Green Belt Levee D/S | 0.97 | 76 |
| A_Green Belt Levee U/S | 14.30 | 78 |
| A_Hondo Pass Basin | 0.08 | 87 |
| A_Hondo Pass Ch | 0.05 | 84 |
| A_Johnson Ch | 0.08 | 91 |
| A_Keltner Dam | 0.49 | 87 |
| A_Mtn Park Dam | 0.81 | 86 |
| A_NE Pond Outer | 3.20 | 81 |
| A_NE Ponding | 3.13 | 75 |
| A_Northgate Dam | 1.47 | 77 |
| A_Northgate Div Ch | 1.29 | 85 |
| A_Northgate Int Ch | 0.60 | 66 |
| A_Northgate Out Ch | 0.47 | 73 |
| A_Northhills Dam N | 2.45 | 84 |
| A_Northhills Dam S | 3.09 | 85 |
| A_PSB Ch 1 D/S | 0.46 | 83 |
| A_PSB Ch 1 U/S Fannin Elem | 1.80 | 81 |
| A_PSB Ch 1 U/S Gateway | 0.24 | 79 |
| A_PSB Ch 1 U/S PSB 2 Jct | 0.70 | 81 |
| A_PSB Ch 2 D/S | 0.99 | 76 |
| A_PSB Ch 2 U/S Gateway | 1.37 | 79 |
| A_PSB Ch 2 U/S Rushing | 0.80 | 75 |
| A_Railroad Drain D/S | 0.05 | 61 |
| A_Railroad Drain U/S Statler Ditch | 0.15 | 73 |
| A_Railroad Drain U/S Tobin Drain | 9.88 | 78 |
| A_Range Basin | 0.39 | 78 |
| A_Range Dam | 2.21 | 81 |
| A_Statler Ditch | 0.45 | 77 |

Table A-10. Curve Number Summary for the Northeast Region (Continued)

| NORTHEAST REGION - CURVE NUMBER SUMMARY | | |
|--|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| A_Sunrise Basin | 0.14 | 87 |
| A_Sunrise Ch | 0.32 | 85 |
| A_Sunrise Dam | 0.50 | 86 |
| A_Tobin Drain U/S Army Ditch | 0.50 | 85 |
| A_Tobin Drain U/S Irvin High | 2.19 | 80 |
| A_Tobin Drain U/S RR Drain | 0.50 | 76 |
| A_TXDOT Pond | 0.61 | 80 |
| A_W Fwy Ch D/S | 1.34 | 72 |
| A_W Fwy Ch U/S | 1.03 | 76 |
| A_War Road Ch | 0.52 | 76 |

Table A-11. Curve Number Summary for the Northwest Region

| NORTHWEST REGION - CURVE NUMBER SUMMARY | | |
|--|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| Arroyo 1A (A1A) | 1.04 | 84 |
| Arroyo 4 (A4_1) | 0.97 | 89 |
| Arroyo 5 (A5_1) | 0.79 | 87 |
| Bandolero Channel_1 (BC_1) | 0.38 | 86 |
| Bandolero Channel_2 (BC_2) | 0.86 | 87 |
| Belvidere Channel (BDC_1) | 0.99 | 88 |
| Borderland Channel_1 (BLC_1) | 0.21 | 92 |
| Borderland Channel_2 (BLC_2) | 0.23 | 82 |
| Borderland Channel_3 (BLC_3) | 0.30 | 71 |
| Borderland Heights Ponds (BHP) | 0.45 | 70 |
| Buena Vista Channel_1 (BVC_1) | 0.02 | 87 |
| Buena Vista Channel_2 (BVC_2) | 0.71 | 87 |
| Coronado Channel (CC_1) | 0.16 | 91 |
| Doniphan Ditch_1 (DD_1) | 1.53 | 81 |
| Doniphan Ditch_3 (DD_3) | 0.16 | 86 |
| Easy Channel (EC_1) | 0.13 | 60 |
| Flow Path Number 38_1 (FPN38_1) | 0.50 | 84 |
| Flow Path Number 38_3 (FPN38_3) | 0.27 | 87 |
| Flow Path Number 38_4 (FPN38_4) | 1.49 | 85 |
| Flow Path Number 38A (FPN38A) | 1.72 | 84 |
| Flow Path Number 38B (FPN38B) | 0.67 | 86 |
| Flow Path Number 39A_1 (FPN39A_1) | 0.06 | 91 |
| Flow Path Number 39A_2 (FPN39A_2) | 0.69 | 85 |
| Flow Path Number 40_1 (FPN40_1) | 0.14 | 93 |
| Flow Path Number 40_2 (FPN40_2) | 0.21 | 85 |
| Flow Path Number 40_3 (FPN40_3) | 2.63 | 84 |
| Flow Path Number 41_1 (FPN41_1) | 0.13 | 85 |
| Flow Path Number 41_2 (FPN41_2) | 1.83 | 84 |
| Flow Path Number 41A (FPN41A) | 1.87 | 84 |
| Flow Path Number 42 (FPN42) | 1.20 | 84 |
| Flow Path Number 42 Trib 1_1 (FPN42T1_1) | 0.11 | 84 |
| Flow Path Number 42 Trib 1_2 | 0.44 | 84 |
| Flow Path Number 42A (FPN42A) | 0.11 | 84 |
| Flow Path Number 43 (FPN43) | 1.12 | 84 |
| Granero Channel (GC_1) | 0.34 | 87 |
| High Ridge_1 (HR_1) | 0.54 | 87 |
| High Ridge_2 (HR_2) | 0.39 | 86 |
| High Ridge_3 (HR_3) | 0.29 | 84 |
| Highway Diversion Channel (HDC) | 0.99 | 88 |
| Keystone Dam (KD1) | 0.14 | 77 |
| Mace (Arroyo 1) (M1 (A1_2)) | 0.16 | 74 |

Table A-11. Curve Number Summary for the Northwest Region (Continued)

| NORTHWEST REGION - CURVE NUMBER SUMMARY | | |
|--|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| Mesa Dam (MeD1) | 0.31 | 83 |
| Mesa Dam Outlet (MDO_1) | 0.04 | 83 |
| Mesa Hills Channel (MHC_2) | 1.07 | 88 |
| Montoya Drain_1 (MD_1) | 1.36 | 83 |
| Montoya Drain_2 (MD_2) | 1.43 | 74 |
| Montoya Drain_3 (MD_3) | 3.33 | 77 |
| Mulberry Dam (MD1) | 0.41 | 87 |
| Mulberry Dam Outlet (MBDO_1) | 0.25 | 85 |
| Nemexas Drain (NeD1) | 1.29 | 74 |
| Ojo de Agua_1 (ODA_1) | 1.29 | 88 |
| Ojo de Agua_2 (ODA_2) | 0.52 | 84 |
| Oxidation Dam (OD) | 0.24 | 87 |
| Oxidation Outlet (OO_1) | 0.19 | 82 |
| Resler Channel_1 (RC_1) | 1.47 | 85 |
| Resler Channel_2 (RC_2) | 1.75 | 84 |
| Ridge View (RV_1) | 1.30 | 85 |
| Silver Springs Channel_1 (SSC_1) | 0.64 | 85 |
| Silver Springs Channel_2 (SSC_2) | 0.74 | 84 |
| Spring Crest Channel (SCC_1) | 0.32 | 85 |
| Thorn Dam (ThoD1) | 0.46 | 84 |
| Thorn Dam Outlet (TDO_1) | 0.07 | 60 |
| Thunderbird Valley (TBV_1) | 0.89 | 86 |
| Unknown 1 (UN01) | 0.24 | 84 |
| Unknown 2_1 (UN02_1) | 0.05 | 84 |
| Unknown 2_2 (UN02_2) | 0.03 | 84 |
| Unknown 24 (UN024_1) | 0.07 | 84 |
| Unknown 3 (UN03) | 0.16 | 84 |
| Unnamed Stream 23_1 (UN23_1) | 0.81 | 75 |
| Unnamed Stream 23_2 (UN23_2) | 0.05 | 85 |
| Unnamed Stream 23_3 (UN23_3) | 0.13 | 86 |
| Unnamed Stream 23A (UN23A) | 0.03 | 84 |
| Unnamed Stream 24A Trib 1 (UN24AT1) | 0.03 | 84 |
| Unnamed Stream 24A_1 (UN24A1) | 0.10 | 84 |
| Unnamed Stream 24A_2 (UN24A2) | 0.07 | 84 |
| Unnamed Stream 24B (UN24B) | 0.19 | 84 |
| Unnamed Stream 24C (UN24C) | 0.06 | 85 |
| Unnamed Stream 24D (UN24D) | 0.02 | 86 |
| Via Serena (VS_1) | 0.70 | 84 |
| West of Rio Grande (WRG) | 14.56 | 66 |
| West_Montoya (WM) | 1.46 | 78 |
| White Spur Drain_1 (WSD_1) | 0.08 | 78 |
| White Spur Drain_2 (WSD_2) | 0.21 | 90 |

Table A-12. Curve Number Summary for the West Central Region

| WEST CENTRAL REGION - CURVE NUMBER SUMMARY | | |
|---|--|------------------------------|
| Watershed Name and HEC-HMS ID | Watershed Area (mi²) | Weighted Curve Number |
| Border Canal (Bcanal) | 0.80 | 91 |
| Canterbury Channel (CBC_1) | 0.89 | 87 |
| Flow Path Number 20_1 (FPN20_1) | 0.21 | 89 |
| Flow Path Number 20_2 (FPN20_2) | 1.32 | 87 |
| Flow Path Number 21_1 (FPN21_1) | 0.24 | 90 |
| Flow Path Number 21_2 (FPN21_2) | 1.41 | 87 |
| Flow Path Number 23 (FPN23_1) | 1.85 | 88 |
| Industrial 1 (Ind1) | 1.38 | 86 |
| Paragon Channel (PC_1) | 1.55 | 88 |

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Table A-13. Summary of Lag Times for the Central Region

| CENTRAL REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| A_Alameda Avenue | 3901 | 0.74 | 1937 | 0.37 | 0.001 | 0.50 | 0.3 | 0.34 | 20.3 | 0.6719 |
| A_Altura_Ave_Dam | 4348 | 0.82 | 1938 | 0.37 | 0.164 | 0.31 | 0.3 | 0.22 | 13.0 | 0.6125 |
| A_Blanco Avenue | 2508 | 0.47 | 860 | 0.16 | 0.001 | 0.50 | 0.3 | 0.23 | 13.9 | 0.6719 |
| A_Boone_St_Basin | 8094 | 1.53 | 4028 | 0.76 | 0.012 | 0.29 | 0.3 | 0.30 | 18.2 | 0.6719 |
| A_Border_Hwy_Overpass | 2753 | 0.52 | 330 | 0.06 | 0.004 | 0.37 | 0.3 | 0.13 | 7.9 | 0.6719 |
| A_Cebada Drainage Outfall | 6852 | 1.30 | 2342 | 0.44 | 0.000 | 0.50 | 0.3 | 0.42 | 25.4 | 0.6719 |
| A_Cebada_Reservoir | 7584 | 1.44 | 2517 | 0.48 | 0.033 | 0.25 | 0.3 | 0.22 | 13.4 | 0.6125 |
| A_Cemex_Spillway | 7319 | 1.39 | 3885 | 0.74 | 0.163 | 0.31 | 0.3 | 0.31 | 18.7 | 0.6125 |
| A_Channel 108 Discharge | 1605 | 0.30 | 679 | 0.13 | 0.001 | 0.50 | 0.3 | 0.19 | 11.3 | 0.6719 |
| A_Comanche Avenue | 2952 | 0.56 | 1789 | 0.34 | 0.001 | 0.50 | 0.3 | 0.30 | 18.2 | 0.6719 |
| A_Concordia_Cemetery | 7919 | 1.50 | 1353 | 0.26 | 0.007 | 0.34 | 0.3 | 0.26 | 15.3 | 0.6719 |
| A_Copia_Ditch_DS | 4873 | 0.92 | 2065 | 0.39 | 0.039 | 0.24 | 0.3 | 0.18 | 10.6 | 0.6125 |
| A_Copia_Ditch_US | 7532 | 1.43 | 3960 | 0.75 | 0.051 | 0.23 | 0.3 | 0.23 | 14.1 | 0.6125 |
| A_Cotton_Dallas_DS | 6862 | 1.30 | 2672 | 0.51 | 0.084 | 0.21 | 0.3 | 0.19 | 11.1 | 0.6125 |
| A_Cotton_Dallas_US | 10938 | 2.07 | 4469 | 0.85 | 0.056 | 0.23 | 0.3 | 0.27 | 16.3 | 0.6125 |
| A_Dallas, San Antonio and Lee | 5878 | 1.11 | 3300 | 0.62 | 0.001 | 0.50 | 0.3 | 0.45 | 26.9 | 0.6719 |
| A_Dam_No_10 | 2943 | 0.56 | 1235 | 0.23 | 0.194 | 0.21 | 0.3 | 0.11 | 6.8 | 0.6125 |
| A_Dam_No_8 | 2047 | 0.39 | 1285 | 0.24 | 0.371 | 0.25 | 0.3 | 0.12 | 7.4 | 0.6125 |
| A_Dam_No_9 | 2320 | 0.44 | 1057 | 0.20 | 0.286 | 0.27 | 0.3 | 0.13 | 7.8 | 0.6125 |
| A_Delta Drive | 2057 | 0.39 | 589 | 0.11 | 0.001 | 0.50 | 0.3 | 0.20 | 11.7 | 0.6719 |
| A_El Paso Paisano to Ninth Outfall | 5515 | 1.04 | 2697 | 0.51 | 0.001 | 0.50 | 0.3 | 0.41 | 24.8 | 0.6719 |
| A_Eucalyptus_to_Cebada | 4122 | 0.78 | 2484 | 0.47 | 0.018 | 0.27 | 0.3 | 0.20 | 12.0 | 0.6125 |
| A_Fonseca | 4197 | 0.79 | 1950 | 0.37 | 0.004 | 0.38 | 0.3 | 0.26 | 15.8 | 0.6719 |
| A_Fort_Blvd_Reservoir | 5043 | 0.96 | 2435 | 0.46 | 0.233 | 0.28 | 0.3 | 0.22 | 13.1 | 0.6125 |
| A_Franklin_Campbell | 3615 | 0.68 | 1299 | 0.25 | 0.045 | 0.23 | 0.3 | 0.13 | 8.1 | 0.6125 |
| A_Glenwood Street | 2565 | 0.49 | 1411 | 0.27 | 0.003 | 0.41 | 0.3 | 0.22 | 13.3 | 0.6719 |

Table A-13. Summary of Lag Times for the Central Region (Continued)

| CENTRAL REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|------|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| A_Hardesty to Shelter | 1418 | 0.27 | 817 | 0.15 | 0.002 | 0.48 | 0.3 | 0.18 | 11.1 | 0.6719 |
| A_Hills Delta to Ninth | 2855 | 0.54 | 828 | 0.16 | 0.001 | 0.50 | 0.3 | 0.24 | 14.3 | 0.6719 |
| A_Houston_Elementary | 6588 | 1.25 | 2530 | 0.48 | 0.044 | 0.50 | 0.23 | 0.44 | 26.7 | 0.6125 |
| A_Kentucky_Dam_Lower | 5902 | 1.12 | 3424 | 0.65 | 0.178 | 0.31 | 0.3 | 0.28 | 16.9 | 0.6125 |
| A_Kentucky_Dam_Upper | 2661 | 0.50 | 1271 | 0.24 | 0.188 | 0.21 | 0.3 | 0.11 | 6.7 | 0.6125 |
| A_Louisiana_Dr_Dam_Lower | 2024 | 0.38 | 1047 | 0.20 | 0.191 | 0.21 | 0.3 | 0.10 | 5.8 | 0.6125 |
| A_Louisiana_Dr_Dam_Upper | 4271 | 0.81 | 1934 | 0.37 | 0.138 | 0.21 | 0.3 | 0.15 | 8.7 | 0.6125 |
| A_Lower_Durazno | 10823 | 2.05 | 5784 | 1.10 | 0.010 | 0.31 | 0.3 | 0.40 | 23.7 | 0.6719 |
| A_Magnolia_Reservoir | 3088 | 0.58 | 1421 | 0.27 | 0.064 | 0.22 | 0.3 | 0.13 | 7.6 | 0.6125 |
| A_McKelligon_Dam | 14585 | 2.76 | 5872 | 1.11 | 0.084 | 0.36 | 0.3 | 0.50 | 30.2 | 0.6125 |
| A_McKelligon_Reservoir_A | 2334 | 0.44 | 784 | 0.15 | 0.380 | 0.25 | 0.3 | 0.11 | 6.6 | 0.6125 |
| A_McKelligon_Reservoir_B | 2810 | 0.53 | 891 | 0.17 | 0.265 | 0.27 | 0.3 | 0.13 | 7.9 | 0.6125 |
| A_McKelligon_Reservoir_C | 732 | 0.14 | 270 | 0.05 | 0.038 | 0.24 | 0.3 | 0.05 | 3.3 | 0.6125 |
| A_McKelligon_Reservoir_D | 915 | 0.17 | 413 | 0.08 | 0.059 | 0.22 | 0.3 | 0.06 | 3.6 | 0.6125 |
| A_Memorial_Park | 5940 | 1.12 | 2384 | 0.45 | 0.039 | 0.24 | 0.3 | 0.20 | 11.8 | 0.6125 |
| A_Memphis_Dam_Lower | 760 | 0.14 | 464 | 0.09 | 0.087 | 0.37 | 0.3 | 0.10 | 6.0 | 0.6125 |
| A_Memphis_Dam_Upper | 4999 | 0.95 | 2493 | 0.47 | 0.248 | 0.28 | 0.3 | 0.22 | 13.2 | 0.6125 |
| A_Modesto Ditch | 2413 | 0.46 | 723 | 0.14 | 0.005 | 0.36 | 0.3 | 0.16 | 9.4 | 0.6719 |
| A_Mountain_Ave_Outlet_Conduit | 8615 | 1.63 | 4681 | 0.89 | 0.037 | 0.24 | 0.3 | 0.27 | 16.1 | 0.6125 |
| A_Nixon Cypress to Central | 1838 | 0.35 | 1026 | 0.19 | 0.000 | 0.50 | 0.3 | 0.22 | 13.4 | 0.6719 |
| A_Noble Myrtle to San Antonio | 1816 | 0.34 | 915 | 0.17 | 0.002 | 0.50 | 0.3 | 0.21 | 12.9 | 0.6719 |
| A_Octavia Texas to Magoffin | 2638 | 0.50 | 1450 | 0.27 | 0.003 | 0.41 | 0.3 | 0.23 | 13.6 | 0.6719 |
| A_Ohio_St_Reservoir_DS | 214 | 0.04 | 19 | 0.00 | 0.166 | 0.21 | 0.3 | 0.01 | 0.9 | 0.6125 |
| A_Ohio_St_Reservoir | 937 | 0.18 | 392 | 0.07 | 0.120 | 0.34 | 0.3 | 0.09 | 5.6 | 0.6125 |
| A_Olive & Cebada takes flow ponds at IH-10 | 6635 | 1.26 | 2122 | 0.40 | 0.001 | 0.50 | 0.3 | 0.41 | 24.4 | 0.6719 |
| A_Overland Mesa to El Paso | 1143 | 0.22 | 527 | 0.10 | 0.003 | 0.42 | 0.3 | 0.13 | 8.0 | 0.6719 |

Table A-13. Summary of Lag Times for the Central Region (Continued)

| CENTRAL REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| A_Paisano and Delta Stanton to Tays | 3850 | 0.73 | 1635 | 0.31 | 0.002 | 0.43 | 0.3 | 0.28 | 16.5 | 0.6719 |
| A_Paisano Ditch | 4309 | 0.82 | 1907 | 0.36 | 0.003 | 0.41 | 0.3 | 0.28 | 17.1 | 0.6719 |
| A_Paisano San Francisco to El Paso | 4667 | 0.88 | 1730 | 0.33 | 0.004 | 0.39 | 0.3 | 0.27 | 16.1 | 0.6719 |
| A_Pera to Cebada | 4177 | 0.79 | 2920 | 0.55 | 0.003 | 0.41 | 0.3 | 0.32 | 19.2 | 0.6719 |
| A_Pershing_Dam | 4887 | 0.93 | 2370 | 0.45 | 0.006 | 0.34 | 0.3 | 0.26 | 15.7 | 0.6719 |
| A_Pollard_Ditch | 4650 | 0.88 | 2554 | 0.48 | 0.028 | 0.26 | 0.3 | 0.20 | 12.1 | 0.6125 |
| A_Pollard_Sacramento | 1605 | 0.30 | 981 | 0.19 | 0.022 | 0.27 | 0.3 | 0.11 | 6.8 | 0.6125 |
| A_Robert Alva Channel | 5507 | 1.04 | 2557 | 0.48 | 0.003 | 0.42 | 0.3 | 0.34 | 20.5 | 0.6719 |
| A_Russel_Ditch_DS | 4290 | 0.81 | 1641 | 0.31 | 0.028 | 0.25 | 0.3 | 0.17 | 9.9 | 0.6125 |
| A_Russel_Ditch_US | 6058 | 1.15 | 2516 | 0.48 | 0.035 | 0.24 | 0.3 | 0.20 | 12.0 | 0.6125 |
| A_San Antonio Hills to Lee | 4215 | 0.80 | 2414 | 0.46 | 0.001 | 0.50 | 0.3 | 0.37 | 22.2 | 0.6719 |
| A_San Antonio Mesa to El Paso | 2817 | 0.53 | 729 | 0.14 | 0.001 | 0.50 | 0.3 | 0.23 | 13.7 | 0.6719 |
| A_San_Diego_Dam | 2868 | 0.54 | 1123 | 0.21 | 0.329 | 0.26 | 0.3 | 0.14 | 8.2 | 0.6125 |
| A_Scenic_Dr_Dam | 3606 | 0.68 | 2322 | 0.44 | 0.241 | 0.28 | 0.3 | 0.20 | 11.7 | 0.6125 |
| A_Seventh and Hills Park to Ninth | 5910 | 1.12 | 2953 | 0.56 | 0.003 | 0.41 | 0.3 | 0.36 | 21.4 | 0.6719 |
| A_Seventh Chihuahueta to St Vrain East | 5327 | 1.01 | 1257 | 0.24 | 0.001 | 0.50 | 0.3 | 0.33 | 19.6 | 0.6719 |
| A_Seventh Chihuahueta to St Vrain West | 2198 | 0.42 | 1113 | 0.21 | 0.000 | 0.50 | 0.3 | 0.24 | 14.5 | 0.6719 |
| A_Tremont_Reservoir | 470 | 0.09 | 225 | 0.04 | 0.073 | 0.22 | 0.3 | 0.04 | 2.5 | 0.6125 |
| A_Upper_Durazno | 1380 | 0.26 | 512 | 0.10 | 0.043 | 0.23 | 0.3 | 0.08 | 4.6 | 0.6125 |
| A_Van_Buren_Dam | 4412 | 0.84 | 2101 | 0.40 | 0.055 | 0.41 | 0.3 | 0.29 | 17.7 | 0.6125 |
| A_Van_Buren_Ditch | 6421 | 1.22 | 3404 | 0.64 | 0.192 | 0.30 | 0.3 | 0.28 | 16.7 | 0.6125 |

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Table A-14. Summary of Lag Times for the East Side Region

| EAST SIDE REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| A_PHELPSDODGE-1 | 9500 | 1.80 | 4250 | 0.80 | 0.008 | 0.330 | 0.3 | 63.15 | 3788.8 | 0.6125 |
| A_PHELPSDODGE-3 | 5000 | 0.95 | 3400 | 0.64 | 0.004 | 0.390 | 0.3 | 57.57 | 3454.2 | 0.6125 |
| A_PHELPSDODGE-4 | 5800 | 1.10 | 1780 | 0.34 | 0.002 | 0.480 | 0.3 | 61.01 | 3660.6 | 0.6125 |
| A_PHELPSDODGE-5 | 6690 | 1.27 | 2900 | 0.55 | 0.003 | 0.410 | 0.3 | 62.97 | 3778.2 | 0.6125 |
| A_PHELPSDODGE-6 | 5800 | 1.10 | 3000 | 0.57 | 0.008 | 0.330 | 0.3 | 49.05 | 2943.3 | 0.6125 |
| A_PHELPSDODGE-7 | 5490 | 1.04 | 200 | 0.04 | 0.006 | 0.350 | 0.3 | 22.71 | 1362.7 | 0.6125 |
| A_PHELPSDODGE-8 | 12560 | 2.38 | 4050 | 0.77 | 0.005 | 0.880 | 0.3 | 180.47 | 10828.5 | 0.6125 |
| A_PHELPSDODGE-9 | 17700 | 3.35 | 7500 | 1.42 | 0.002 | 1.300 | 0.3 | 355.51 | 21330.7 | 0.6125 |
| A_PHELPSDODGE-10 | 10100 | 1.91 | 3000 | 0.57 | 0.004 | 0.950 | 0.3 | 166.78 | 10007.1 | 0.6125 |
| A_Lomaland-1 | 2590 | 0.49 | 590 | 0.11 | 0.005 | 0.360 | 0.3 | 25.80 | 1547.7 | 0.6125 |
| A_Lomaland-2 | 1600 | 0.30 | 580 | 0.11 | 0.008 | 0.330 | 0.3 | 20.36 | 1221.6 | 0.6125 |
| A_Lomaland-3 | 2300 | 0.44 | 950 | 0.18 | 0.008 | 0.330 | 0.3 | 26.32 | 1579.4 | 0.6125 |
| A_Lomaland-4 | 6220 | 1.18 | 7430 | 1.41 | 0.006 | 0.350 | 0.3 | 69.74 | 4184.6 | 0.6125 |
| A_Lomaland-4a | 6221 | 1.18 | 7431 | 1.41 | 0.006 | 0.350 | 0.3 | 69.75 | 4185.0 | 0.6125 |
| A_Lomaland-5 | 4580 | 0.87 | 1700 | 0.32 | 0.008 | 0.330 | 0.3 | 38.54 | 2312.4 | 0.6125 |
| A_Lomaland-6 | 4630 | 0.88 | 1500 | 0.28 | 0.006 | 0.350 | 0.3 | 39.50 | 2369.9 | 0.6125 |
| A_Lomaland-7 | 4100 | 0.78 | 1750 | 0.33 | 0.008 | 0.330 | 0.3 | 37.61 | 2256.4 | 0.6125 |
| A_Lomaland-8 | 7550 | 1.43 | 1700 | 0.32 | 0.020 | 0.270 | 0.3 | 36.63 | 2198.0 | 0.6125 |
| A_Lomaland-8a | 7460 | 1.41 | 3330 | 0.63 | 0.020 | 0.270 | 0.3 | 44.66 | 2679.6 | 0.6125 |
| A_Lomaland-9 | 8200 | 1.55 | 2400 | 0.45 | 0.007 | 0.340 | 0.3 | 52.44 | 3146.6 | 0.6125 |
| A_Lomaland-10 | 2690 | 0.51 | 980 | 0.19 | 0.020 | 0.270 | 0.3 | 22.79 | 1367.1 | 0.6125 |
| A_Americas-1 | 4180 | 0.79 | 1960 | 0.37 | 0.010 | 0.310 | 0.3 | 36.76 | 2205.7 | 0.6125 |
| A_Americas-2 | 5170 | 0.98 | 3000 | 0.57 | 0.005 | 0.360 | 0.3 | 51.70 | 3102.0 | 0.6125 |
| A_Americas-3 | 3600 | 0.68 | 1230 | 0.23 | 0.014 | 0.290 | 0.3 | 28.59 | 1715.6 | 0.6125 |
| A_Americas-4 | 2160 | 0.41 | 360 | 0.07 | 0.007 | 0.340 | 0.3 | 19.89 | 1193.6 | 0.6125 |

Table A-14. Summary of Lag Times for the East Side Region (Continued)

| EAST SIDE REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| A_Americas-5 | 3670 | 0.70 | 1780 | 0.34 | 0.006 | 0.800 | 0.3 | 88.64 | 5318.2 | 0.6125 |
| A_Americas-6 | 3230 | 0.61 | 1390 | 0.26 | 0.013 | 0.310 | 0.3 | 30.69 | 1841.5 | 0.6125 |
| A_Americas-7 | 2430 | 0.46 | 740 | 0.14 | 0.017 | 0.270 | 0.3 | 20.31 | 1218.9 | 0.6125 |
| A_Americas-8 | 3640 | 0.69 | 1670 | 0.32 | 0.005 | 0.880 | 0.3 | 95.42 | 5725.0 | 0.6125 |
| A_Americas-9 | 5370 | 1.02 | 2590 | 0.49 | 0.018 | 0.270 | 0.3 | 37.53 | 2251.6 | 0.6125 |
| A_Americas-10 | 2010 | 0.38 | 790 | 0.15 | 0.006 | 0.350 | 0.3 | 25.37 | 1522.2 | 0.6125 |
| A_Americas-11 | 3900 | 0.74 | 1900 | 0.36 | 0.008 | 0.330 | 0.3 | 37.97 | 2278.3 | 0.6125 |
| A_Americas-12 | 1500 | 0.28 | 450 | 0.09 | 0.004 | 0.950 | 0.3 | 53.27 | 3196.4 | 0.6125 |
| A_AmTen-1 | 7520 | 1.42 | 2800 | 0.53 | 0.004 | 0.390 | 0.3 | 61.39 | 3683.2 | 0.6125 |
| A_AmTen-2 | 1200 | 0.23 | 6300 | 1.19 | 0.001 | 0.490 | 0.3 | 56.72 | 3403.3 | 0.6125 |
| A_AmTen-3 | 5000 | 0.95 | 1550 | 0.29 | 0.005 | 0.360 | 0.3 | 41.98 | 2519.1 | 0.6125 |
| A_AmTen-4 | 4070 | 0.77 | 1930 | 0.37 | 0.005 | 0.360 | 0.3 | 42.15 | 2529.3 | 0.6125 |
| A_AmTen-5 | 1680 | 0.32 | 1000 | 0.19 | 0.023 | 0.260 | 0.3 | 19.17 | 1150.1 | 0.6125 |
| A_AmTen-6 | 12000 | 2.27 | 5800 | 1.10 | 0.002 | 1.300 | 0.3 | 292.90 | 17574.3 | 0.6125 |
| A_AmTen-7 | 9410 | 1.78 | 4120 | 0.78 | 0.003 | 1.080 | 0.3 | 204.16 | 12249.6 | 0.6125 |
| A_CarolinaDam-1 | 4420 | 0.84 | 1380 | 0.26 | 0.033 | 0.250 | 0.3 | 27.14 | 1628.1 | 0.6125 |
| A_CarolinaDam-2 | 3020 | 0.57 | 900 | 0.17 | 0.015 | 0.280 | 0.3 | 23.85 | 1430.8 | 0.6125 |
| A_MesaDrain-1 | 2750 | 0.52 | 1300 | 0.25 | 0.023 | 0.260 | 0.3 | 24.04 | 1442.5 | 0.6125 |
| A_MesaDrain-2 | 4790 | 0.91 | 2040 | 0.39 | 0.023 | 0.260 | 0.3 | 32.51 | 1950.4 | 0.6125 |
| A_Sunmount | 4500 | 0.85 | 1490 | 0.28 | 0.008 | 0.330 | 0.3 | 36.85 | 2211.0 | 0.6125 |
| A_RLH_2 | 1210 | 0.23 | 505 | 0.10 | 0.028 | 0.250 | 0.3 | 13.61 | 816.4 | 0.6125 |
| A_MesaDrain-UP | 2440 | 0.46 | 1190 | 0.23 | 0.026 | 0.250 | 0.3 | 21.72 | 1303.1 | 0.6125 |
| A_MesaDrain-3 | 3140 | 0.59 | 1390 | 0.26 | 0.023 | 0.260 | 0.3 | 25.52 | 1531.5 | 0.6125 |
| A_MesaDrain-4 | 4700 | 0.89 | 2180 | 0.41 | 0.020 | 0.270 | 0.3 | 34.24 | 2054.4 | 0.6125 |
| A_PhelpsDodge_1a | 3200 | 0.61 | 950 | 0.18 | 0.023 | 0.260 | 0.3 | 22.90 | 1374.0 | 0.6125 |

Table A-15. Summary of Lag Times for the Mission Valley Region

| MISSION VALLEY REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|---|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| A_Americas Basin | 10225 | 1.94 | 4260 | 0.81 | 0.007 | 0.780 | 0.3 | 0.89 | 53.5 | 0.6719 |
| A_Americas Ten Basin | 5043 | 0.96 | 1692 | 0.32 | 0.016 | 0.590 | 0.3 | 0.41 | 24.8 | 0.6125 |
| A_Americas Ten NonContribute | 2766 | 0.52 | 1563 | 0.30 | 0.018 | 0.590 | 0.3 | 0.34 | 20.2 | 0.6125 |
| A_Basin A | 10459 | 1.98 | 5464 | 1.03 | 0.002 | 0.480 | 0.3 | 0.60 | 35.7 | 0.6719 |
| A_Basin G | 19126 | 3.62 | 6752 | 1.28 | 0.000 | 0.500 | 0.3 | 0.79 | 47.5 | 0.6719 |
| A_Below Basin G to Cty Limit | 18490 | 3.50 | 9103 | 1.72 | 0.001 | 0.720 | 0.3 | 1.23 | 74.1 | 0.6719 |
| A_Below Carolina Dam | 11496 | 2.18 | 5810 | 1.10 | 0.014 | 0.290 | 0.3 | 0.38 | 22.6 | 0.6719 |
| A_Below Featherlake Basin | 2281 | 0.43 | 654 | 0.12 | 0.005 | 0.880 | 0.3 | 0.37 | 21.9 | 0.6719 |
| A_Below Phelps Dodge Basin | 14196 | 2.69 | 6774 | 1.28 | 0.005 | 0.370 | 0.3 | 0.54 | 32.2 | 0.6719 |
| A_Carolina Drive Basin | 4865 | 0.92 | 1950 | 0.37 | 0.025 | 0.260 | 0.3 | 0.19 | 11.3 | 0.6125 |
| A_Feather Lake Basin | 8765 | 1.66 | 3308 | 0.63 | 0.002 | 0.440 | 0.3 | 0.45 | 26.7 | 0.6719 |
| A_Franklin Drain A | 7507 | 1.42 | 3151 | 0.60 | 0.003 | 0.415 | 0.3 | 0.40 | 23.7 | 0.6719 |
| A_Franklin Drain B | 6217 | 1.18 | 2334 | 0.44 | 0.003 | 0.415 | 0.3 | 0.34 | 20.5 | 0.6719 |
| A_Franklin Drn to City Limit | 13601 | 2.58 | 6290 | 1.19 | 0.001 | 1.300 | 0.3 | 1.82 | 109.2 | 0.6719 |
| A_Franklin Spur Drain | 3831 | 0.73 | 2259 | 0.43 | 0.003 | 0.415 | 0.3 | 0.29 | 17.5 | 0.6719 |
| A_Lincoln Drain | 16605 | 3.14 | 9280 | 1.76 | 0.018 | 0.270 | 0.3 | 0.45 | 27.1 | 0.6125 |
| A_Lomaland Basin | 7144 | 1.35 | 1764 | 0.33 | 0.023 | 0.260 | 0.3 | 0.20 | 12.3 | 0.6125 |
| A_Mesa Drain A | 9197 | 1.74 | 4628 | 0.88 | 0.024 | 0.260 | 0.3 | 0.30 | 17.7 | 0.6125 |
| A_Mesa Drain B | 8686 | 1.65 | 4427 | 0.84 | 0.019 | 0.270 | 0.3 | 0.30 | 17.8 | 0.6125 |
| A_Mesa Drain C | 23070 | 4.37 | 9827 | 1.86 | 0.006 | 0.350 | 0.3 | 0.66 | 39.4 | 0.6719 |
| A_Mesa Drain to City Limit | 8574 | 1.62 | 4708 | 0.89 | 0.007 | 0.780 | 0.3 | 0.87 | 52.3 | 0.6719 |
| A_Middle Drain A | 37551 | 7.11 | 15118 | 2.86 | 0.001 | 0.500 | 0.3 | 1.23 | 74.1 | 0.6719 |
| A_Middle Drain B | 4049 | 0.77 | 2756 | 0.52 | 0.005 | 0.355 | 0.3 | 0.27 | 16.2 | 0.6719 |
| A_Middle Drain Spur A | 1527 | 0.29 | 689 | 0.13 | 0.008 | 0.325 | 0.3 | 0.12 | 7.3 | 0.6719 |
| A_Middle Drain Spur B | 2500 | 0.47 | 1374 | 0.26 | 0.006 | 0.345 | 0.3 | 0.18 | 11.0 | 0.6719 |
| A_Middle to City Limit | 8241 | 1.56 | 4125 | 0.78 | 0.002 | 0.330 | 0.3 | 0.35 | 21.0 | 0.6719 |

Table A-15. Summary of Lag Times for the Mission Valley Region (Continued)

| MISSION VALLEY REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|---|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| A_North Loop Detention Basin | 10314 | 1.95 | 5213 | 0.99 | 0.015 | 0.285 | 0.3 | 0.35 | 20.8 | 0.6719 |
| A_Phelps Dodge Basin | 9977 | 1.89 | 2988 | 0.57 | 0.010 | 0.320 | 0.3 | 0.33 | 19.6 | 0.6719 |
| A_Playa Drain A | 8716 | 1.65 | 3521 | 0.67 | 0.002 | 0.450 | 0.3 | 0.46 | 27.8 | 0.6719 |
| A_Playa Drain B | 46184 | 8.75 | 20436 | 3.87 | 0.001 | 0.500 | 0.3 | 1.44 | 86.3 | 0.6719 |

Table A-16. Summary of Lag Times for the Northeast Region

| NORTHEAST REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| A_Amber Basin | 5200 | 0.98 | 2163 | 0.41 | 0.083 | 0.210 | 0.3 | 0.16 | 9.6 | 0.6125 |
| A_Army Ditch | 6517 | 1.23 | 4495 | 0.85 | 0.009 | 0.310 | 0.3 | 0.31 | 18.9 | 0.6719 |
| A_Bossworth Ch D/S | 4318 | 0.82 | 2383 | 0.45 | 0.034 | 0.440 | 0.3 | 0.33 | 19.6 | 0.6125 |
| A_Bossworth Ch U/S | 7397 | 1.40 | 4218 | 0.80 | 0.071 | 0.380 | 0.3 | 0.39 | 23.6 | 0.6125 |
| A_Diana Ditch D/S | 20770 | 3.93 | 9008 | 1.71 | 0.035 | 0.250 | 0.3 | 0.44 | 26.6 | 0.6125 |
| A_Diana Ditch U/S Sunrise Ch | 9243 | 1.75 | 4780 | 0.91 | 0.013 | 0.280 | 0.3 | 0.32 | 19.3 | 0.6719 |
| A_E Fwy Ch | 15161 | 2.87 | 7719 | 1.46 | 0.006 | 0.830 | 0.3 | 1.28 | 76.6 | 0.6719 |
| A_Electric Ditch | 13557 | 2.57 | 6665 | 1.26 | 0.022 | 0.260 | 0.3 | 0.37 | 22.2 | 0.6125 |
| A_Fairbanks Drive | 20178 | 3.82 | 12453 | 2.36 | 0.066 | 0.390 | 0.3 | 0.75 | 45.3 | 0.6125 |
| A_Fort Bliss Diversion Ch | 3730 | 0.71 | 2035 | 0.39 | 0.048 | 0.230 | 0.3 | 0.16 | 9.3 | 0.6125 |
| A_Ft Bliss Diversion Channel D/S | 27026 | 5.12 | 2613 | 0.49 | 0.004 | 0.370 | 0.3 | 0.49 | 29.3 | 0.6719 |
| A_Ft Bliss Diversion Channel U/S | 4926 | 0.93 | 2418 | 0.46 | 0.065 | 0.220 | 0.3 | 0.17 | 10.2 | 0.6125 |
| A_Fusselman Dam | 15888 | 3.01 | 6160 | 1.17 | 0.093 | 0.360 | 0.3 | 0.52 | 31.5 | 0.6125 |
| A_Green Belt Levee D/S | 8912 | 1.69 | 4590 | 0.87 | 0.006 | 0.830 | 0.3 | 0.93 | 55.9 | 0.6719 |
| A_Green Belt Levee U/S | 38976 | 7.38 | 18966 | 3.59 | 0.026 | 0.510 | 0.3 | 1.36 | 81.8 | 0.6125 |
| A_Hondo Pass Basin | 5155 | 0.98 | 2241 | 0.42 | 0.066 | 0.215 | 0.3 | 0.17 | 9.9 | 0.6125 |
| A_Hondo Pass Ch | 1962 | 0.37 | 850 | 0.16 | 0.063 | 0.390 | 0.3 | 0.17 | 10.1 | 0.6125 |
| A_Johnson Ch | 4618 | 0.87 | 2261 | 0.43 | 0.035 | 0.240 | 0.3 | 0.18 | 10.7 | 0.6125 |
| A_Keltner Dam | 5661 | 1.07 | 4074 | 0.77 | 0.143 | 0.320 | 0.3 | 0.30 | 18.1 | 0.6125 |
| A_Mtn Park Dam | 11026 | 2.09 | 6414 | 1.21 | 0.145 | 0.315 | 0.3 | 0.42 | 25.0 | 0.6125 |
| A_NE Pond Outer | 11233 | 2.13 | 5385 | 1.02 | 0.008 | 0.320 | 0.3 | 0.40 | 24.2 | 0.6719 |
| A_NE Ponding | 17301 | 3.28 | 6884 | 1.30 | 0.007 | 0.770 | 0.3 | 1.19 | 71.4 | 0.6719 |
| A_Northgate Dam | 10857 | 2.06 | 3888 | 0.74 | 0.054 | 0.405 | 0.3 | 0.46 | 27.5 | 0.6125 |
| A_Northgate Div Ch | 13820 | 2.62 | 8409 | 1.59 | 0.082 | 0.365 | 0.3 | 0.56 | 33.6 | 0.6125 |
| A_Northgate Int Ch | 10387 | 1.97 | 7854 | 1.49 | 0.027 | 0.500 | 0.3 | 0.69 | 41.4 | 0.6125 |
| A_Northgate Out Ch | 6964 | 1.32 | 2452 | 0.46 | 0.016 | 0.595 | 0.3 | 0.51 | 30.8 | 0.6125 |

Table A-16. Summary of Lag Times for the Northeast Region (Continued)

| NORTHEAST REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| A_Northhills Dam N | 16570 | 3.14 | 9652 | 1.83 | 0.089 | 0.365 | 0.3 | 0.62 | 37.0 | 0.6125 |
| A_Northhills Dam S | 18475 | 3.50 | 9474 | 1.79 | 0.062 | 0.390 | 0.3 | 0.68 | 40.6 | 0.6125 |
| A_PSB Ch 1 D/S | 9994 | 1.89 | 6271 | 1.19 | 0.009 | 0.310 | 0.3 | 0.40 | 23.7 | 0.6719 |
| A_PSB Ch 1 U/S Fannin Elem | 26864 | 5.09 | 13672 | 2.59 | 0.056 | 0.405 | 0.3 | 0.88 | 52.7 | 0.6125 |
| A_PSB Ch 1 U/S Gateway | 6935 | 1.31 | 3511 | 0.66 | 0.054 | 0.410 | 0.3 | 0.39 | 23.6 | 0.6125 |
| A_PSB Ch 1 U/S PSB 2 Jct | 9171 | 1.74 | 5576 | 1.06 | 0.009 | 0.310 | 0.3 | 0.37 | 22.3 | 0.6719 |
| A_PSB Ch 2 D/S | 14012 | 2.65 | 7059 | 1.34 | 0.007 | 0.325 | 0.3 | 0.48 | 28.5 | 0.6719 |
| A_PSB Ch 2 U/S Gateway | 18893 | 3.58 | 9875 | 1.87 | 0.093 | 0.355 | 0.3 | 0.63 | 37.7 | 0.6125 |
| A_PSB Ch 2 U/S Rushing | 11672 | 2.21 | 4702 | 0.89 | 0.024 | 0.260 | 0.3 | 0.32 | 19.1 | 0.6125 |
| A_Railroad Drain D/S | 3909 | 0.74 | 2040 | 0.39 | 0.001 | 0.500 | 0.3 | 0.34 | 20.6 | 0.6719 |
| A_Railroad Drain U/S Statler Ditch | 6019 | 1.14 | 2486 | 0.47 | 0.005 | 0.850 | 0.3 | 0.71 | 42.3 | 0.6719 |
| A_Railroad Drain U/S Tobin Drain | 34210 | 6.48 | 15274 | 2.89 | 0.003 | 1.050 | 0.3 | 2.53 | 151.8 | 0.6719 |
| A_Range Basin | 5601 | 1.06 | 2473 | 0.47 | 0.022 | 0.260 | 0.3 | 0.21 | 12.6 | 0.6125 |
| A_Range Dam | 21002 | 3.98 | 10994 | 2.08 | 0.048 | 0.415 | 0.3 | 0.78 | 47.0 | 0.6125 |
| A_Statler Ditch | 5989 | 1.13 | 3252 | 0.62 | 0.001 | 0.500 | 0.3 | 0.45 | 26.9 | 0.6719 |
| A_Sunrise Basin | 5021 | 0.95 | 2828 | 0.54 | 0.051 | 0.230 | 0.3 | 0.19 | 11.3 | 0.6125 |
| A_Sunrise Ch | 12185 | 2.31 | 8084 | 1.53 | 0.025 | 0.260 | 0.3 | 0.38 | 22.8 | 0.6125 |
| A_Sunrise Dam | 9790 | 1.85 | 4128 | 0.78 | 0.133 | 0.320 | 0.3 | 0.36 | 21.5 | 0.6125 |
| A_Tobin Drain U/S Army Ditch | 6079 | 1.15 | 1324 | 0.25 | 0.007 | 0.330 | 0.3 | 0.23 | 13.6 | 0.6719 |
| A_Tobin Drain U/S Irvin High | 15912 | 3.01 | 7409 | 1.40 | 0.010 | 0.300 | 0.3 | 0.46 | 27.7 | 0.6719 |
| A_Tobin Drain U/S RR Drain | 6624 | 1.25 | 3660 | 0.69 | 0.005 | 0.350 | 0.3 | 0.34 | 20.1 | 0.6719 |
| A_TXDOT Pond | 14365 | 2.72 | 5556 | 1.05 | 0.041 | 0.355 | 0.3 | 0.49 | 29.2 | 0.6125 |
| A_W Fwy Ch D/S | 19427 | 3.68 | 10134 | 1.92 | 0.015 | 0.605 | 0.3 | 1.09 | 65.3 | 0.6125 |
| A_W Fwy Ch U/S | 7827 | 1.48 | 3853 | 0.73 | 0.017 | 0.270 | 0.3 | 0.28 | 16.6 | 0.6125 |
| A_War Road Ch | 7844 | 1.49 | 2560 | 0.48 | 0.014 | 0.285 | 0.3 | 0.26 | 15.5 | 0.6719 |

Table A-17. Summary of Lag Times for the Northwest Region

| NORTHWEST REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| Arroyo 1A (A1A) | 13072 | 2.48 | 8442 | 1.60 | 0.078 | 0.38 | 0.3 | 0.57 | 34.5 | 0.6125 |
| Arroyo 4 (A4_1) | 19185 | 3.63 | 9194 | 1.74 | 0.034 | 0.245 | 0.3 | 0.43 | 25.6 | 0.6125 |
| Arroyo 5 (A5_1) | 17006 | 3.22 | 7249 | 1.37 | 0.036 | 0.245 | 0.3 | 0.38 | 23.0 | 0.6125 |
| Bandolero Channel_1 (BC_1) | 12494 | 2.37 | 5166 | 0.98 | 0.029 | 0.295 | 0.3 | 0.38 | 22.8 | 0.6719 |
| Bandolero Channel_2 (BC_2) | 16448 | 3.12 | 9141 | 1.73 | 0.046 | 0.23 | 0.3 | 0.38 | 22.9 | 0.6125 |
| Belvidere Channel (BDC_1) | 17892 | 3.39 | 8978 | 1.70 | 0.036 | 0.245 | 0.3 | 0.41 | 24.9 | 0.6125 |
| Borderland Channel_1 (BLC_1) | 6064 | 1.15 | 2942 | 0.56 | 0.026 | 0.26 | 0.3 | 0.22 | 13.4 | 0.6125 |
| Borderland Channel_2 (BLC_2) | 6872 | 1.30 | 3229 | 0.61 | 0.023 | 0.268 | 0.3 | 0.25 | 15.0 | 0.6125 |
| Borderland Channel_3 (BLC_3) | 6072 | 1.15 | 3649 | 0.69 | 0.031 | 0.25 | 0.3 | 0.23 | 14.0 | 0.6125 |
| Borderland Heights Ponds (BHP) | 6454 | 1.22 | 3123 | 0.59 | 0.020 | 0.270 | 0.3 | 0.24 | 14.7 | 0.6125 |
| Buena Vista Channel_1 (BVC_1) | 1875 | 0.36 | 996 | 0.19 | 0.004 | 0.95 | 0.3 | 0.42 | 25.3 | 0.6719 |
| Buena Vista Channel_2 (BVC_2) | 17974 | 3.40 | 9057 | 1.72 | 0.052 | 0.23 | 0.3 | 0.39 | 23.4 | 0.6125 |
| Coronado Channel (CC_1) | 11499 | 2.18 | 5811 | 1.10 | 0.041 | 0.238 | 0.3 | 0.31 | 18.6 | 0.6125 |
| Doniphan Ditch_1 (DD_1) | 16518 | 3.13 | 8209 | 1.55 | 0.0007 | 0.70 | 0.3 | 1.13 | 67.5 | 0.6719 |
| Doniphan Ditch_3 (DD_3) | 5490 | 1.04 | 2924 | 0.55 | 0.020 | 0.27 | 0.3 | 0.23 | 13.7 | 0.6125 |
| Easy Channel (EC_1) | 3876 | 0.73 | 1659 | 0.31 | 0.019 | 0.27 | 0.3 | 0.17 | 10.4 | 0.6125 |
| Flow Path Number 38_1 (FPN38_1) | 12390 | 2.35 | 6418 | 1.22 | 0.023 | 0.26 | 0.3 | 0.36 | 21.4 | 0.6125 |
| Flow Path Number 38_3 (FPN38_3) | 5382 | 1.02 | 2760 | 0.52 | 0.025 | 0.26 | 0.3 | 0.22 | 12.9 | 0.6125 |
| Flow Path Number 38_4 (FPN38_4) | 15474 | 2.93 | 7595 | 1.44 | 0.049 | 0.23 | 0.3 | 0.35 | 21.2 | 0.6125 |
| Flow Path Number 38A (FPN38A) | 28155 | 5.33 | 14500 | 2.75 | 0.058 | 0.41 | 0.3 | 0.92 | 55.0 | 0.6125 |
| Flow Path Number 38B (FPN38B) | 13250 | 2.51 | 6804 | 1.29 | 0.035 | 0.47 | 0.3 | 0.67 | 40.1 | 0.6125 |
| Flow Path Number 39A_1 (FPN39A_1) | 5510 | 1.04 | 2695 | 0.51 | 0.030 | 0.25 | 0.3 | 0.21 | 12.4 | 0.6125 |
| Flow Path Number 39A_2 (FPN39A_2) | 16942 | 3.21 | 8605 | 1.63 | 0.040 | 0.46 | 0.3 | 0.76 | 45.3 | 0.6125 |
| Flow Path Number 40_1 (FPN40_1) | 5168 | 0.98 | 2336 | 0.44 | 0.027 | 0.52 | 0.3 | 0.40 | 24.3 | 0.6125 |
| Flow Path Number 40_2 (FPN40_2) | 6630 | 1.26 | 3493 | 0.66 | 0.036 | 0.47 | 0.3 | 0.44 | 26.7 | 0.6125 |
| Flow Path Number 40_3 (FPN40_3) | 33343 | 6.31 | 14135 | 2.68 | 0.040 | 0.46 | 0.3 | 1.07 | 64.5 | 0.6125 |
| Flow Path Number 41_1 (FPN41_1) | 7887 | 1.49 | 4013 | 0.76 | 0.033 | 0.48 | 0.3 | 0.50 | 29.9 | 0.6125 |
| Flow Path Number 41_2 (FPN41_2) | 23462 | 4.44 | 10691 | 2.02 | 0.033 | 0.48 | 0.3 | 0.93 | 55.7 | 0.6125 |
| Flow Path Number 41A (FPN41A) | 24856 | 4.71 | 12702 | 2.41 | 0.031 | 0.49 | 0.3 | 1.01 | 60.9 | 0.6125 |
| Flow Path Number 42 (FPN42) | 23035 | 4.36 | 11536 | 2.18 | 0.031 | 0.49 | 0.3 | 0.96 | 57.8 | 0.6125 |

Table A-17. Summary of Lag Times for the Northwest Region (Continued)

| NORTHWEST REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| Flow Path Number 42 Trib 1_1 (FPN42T1_1) | 683 | 0.13 | 440 | 0.08 | 0.016 | 0.6 | 0.3 | 0.15 | 9.2 | 0.6125 |
| Flow Path Number 42 Trib 1_2 | 13249 | 2.51 | 6712 | 1.27 | 0.034 | 0.48 | 0.3 | 0.68 | 40.8 | 0.6125 |
| Flow Path Number 42A (FPN42A) | 3965 | 0.75 | 2115 | 0.40 | 0.028 | 0.5 | 0.3 | 0.35 | 20.9 | 0.6125 |
| Flow Path Number 43 (FPN43) | 15746 | 2.98 | 8094 | 1.53 | 0.034 | 0.48 | 0.3 | 0.76 | 45.4 | 0.6125 |
| Granero Channel (GC_1) | 7933 | 1.50 | 3714 | 0.70 | 0.048 | 0.225 | 0.3 | 0.23 | 13.7 | 0.6125 |
| High Ridge_1 (HR_1) | 6423 | 1.22 | 3085 | 0.58 | 0.036 | 0.243 | 0.3 | 0.22 | 13.2 | 0.6125 |
| High Ridge_2 (HR_2) | 9166 | 1.74 | 4327 | 0.82 | 0.037 | 0.24 | 0.3 | 0.27 | 16.0 | 0.6125 |
| High Ridge_3 (HR_3) | 8656 | 1.64 | 4420 | 0.84 | 0.051 | 0.413 | 0.3 | 0.45 | 27.2 | 0.6125 |
| Highway Diversion Channel (HDC) | 12722 | 2.41 | 5405 | 1.02 | 0.025 | 0.26 | 0.3 | 0.34 | 20.5 | 0.6125 |
| Keystone Dam (KD1) | 3875 | 0.73 | 1372 | 0.26 | 0.002 | 1.25 | 0.3 | 0.76 | 45.6 | 0.6719 |
| Mace (Arroyo 1) (M1 (A1_2)) | 4286 | 0.81 | 2620 | 0.50 | 0.027 | 0.258 | 0.3 | 0.20 | 11.8 | 0.6125 |
| Mesa Dam (MeD1) | 7932 | 1.50 | 3400 | 0.64 | 0.023 | 0.263 | 0.3 | 0.26 | 15.6 | 0.6125 |
| Mesa Dam Outlet (MDO_1) | 7018 | 1.33 | 983 | 0.19 | 0.007 | 0.255 | 0.3 | 0.17 | 10.1 | 0.6125 |
| Mesa Hills Channel (MHC_2) | 11540 | 2.19 | 7267 | 1.38 | 0.040 | 0.24 | 0.3 | 0.33 | 20.0 | 0.6125 |
| Montoya Drain_1 (MD_1) | 15180 | 2.88 | 8578 | 1.62 | 0.0002 | 1.15 | 0.3 | 1.83 | 109.6 | 0.6719 |
| Montoya Drain_2 (MD_2) | 13486 | 2.55 | 7045 | 1.33 | 0.005 | 0.36 | 0.3 | 0.52 | 31.2 | 0.6719 |
| Montoya Drain_3 (MD_3) | 22111 | 4.19 | 13545 | 2.57 | 0.0004 | 0.86 | 0.3 | 1.75 | 105.2 | 0.6719 |
| Mulberry Dam (MD1) | 15180 | 2.88 | 3042 | 0.58 | 0.000 | 0.258 | 0.3 | 0.30 | 18.0 | 0.6125 |
| Mulberry Dam Outlet (MBDO_1) | 5632 | 1.07 | 3097 | 0.59 | 0.022 | 0.265 | 0.3 | 0.23 | 13.8 | 0.6125 |
| Nemexas Drain (NeD1) | 23356 | 4.42 | 8280 | 1.57 | 0.001 | 0.61 | 0.3 | 1.09 | 65.4 | 0.6719 |
| Ojo de Agua_1 (ODA_1) | 16046 | 3.04 | 7935 | 1.50 | 0.035 | 0.245 | 0.3 | 0.39 | 23.2 | 0.6125 |
| Ojo de Agua_2 (ODA_2) | 10148 | 1.92 | 5696 | 1.08 | 0.074 | 0.38 | 0.3 | 0.47 | 28.4 | 0.6125 |
| Oxidation Dam (OD) | 7520 | 1.42 | 2527 | 0.48 | 0.038 | 0.241 | 0.3 | 0.21 | 12.9 | 0.6125 |
| Oxidation Outlet (OO_1) | 4497 | 0.85 | 2588 | 0.49 | 0.022 | 0.65 | 0.3 | 0.50 | 30.0 | 0.6125 |
| Resler Channel_1 (RC_1) | 21276 | 4.03 | 11815 | 2.24 | 0.033 | 0.48 | 0.3 | 0.93 | 55.7 | 0.6125 |
| Resler Channel_2 (RC_2) | 22453 | 4.25 | 11048 | 2.09 | 0.075 | 0.38 | 0.3 | 0.73 | 43.9 | 0.6125 |
| Ridge View (RV_1) | 20294 | 3.84 | 11952 | 2.26 | 0.057 | 0.41 | 0.3 | 0.78 | 47.1 | 0.6125 |
| Silver Springs Channel_1 (SSC_1) | 11379 | 2.16 | 7982 | 1.51 | 0.076 | 0.38 | 0.3 | 0.54 | 32.5 | 0.6125 |
| Silver Springs Channel_2 (SSC_2) | 6840 | 1.30 | 4390 | 0.83 | 0.230 | 0.28 | 0.3 | 0.29 | 17.2 | 0.6125 |
| Spring Crest Channel (SCC_1) | 7790 | 1.48 | 4130 | 0.78 | 0.060 | 0.22 | 0.3 | 0.23 | 13.8 | 0.6125 |

Table A-17. Summary of Lag Times for the Northwest Region (Continued)

| NORTHWEST REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------|--------|-----------------|--------|-----------------|----------------|-----|------------------|------------------|----------------|
| Watershed Name and HEC-HMS ID | L _L | | L _{CA} | | S _{ST} | C _T | N | T _{lag} | T _{lag} | C _P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| Thorn Dam (ThoD1) | 7036 | 1.33 | 3131 | 0.59 | 0.025 | 0.258 | 0.3 | 0.24 | 14.4 | 0.6125 |
| Thorn Dam Outlet (TDO_1) | 3242 | 0.61 | 946 | 0.18 | 0.028 | 0.255 | 0.3 | 0.13 | 7.9 | 0.6125 |
| Thunderbird Valley (TBV_1) | 16810 | 3.18 | 10187 | 1.93 | 0.046 | 0.235 | 0.3 | 0.41 | 24.3 | 0.6125 |
| Unknown 1(UN01) | 7171 | 1.36 | 3829 | 0.73 | 0.028 | 0.5 | 0.3 | 0.50 | 29.9 | 0.6125 |
| Unknown 2_1 (UN02_1) | 3451 | 0.65 | 1775 | 0.34 | 0.022 | 0.54 | 0.3 | 0.34 | 20.6 | 0.6125 |
| Unknown 2_2 (UN02_2) | 2805 | 0.53 | 1410 | 0.27 | 0.033 | 0.48 | 0.3 | 0.27 | 16.0 | 0.6125 |
| Unknown 24 (UN024_1) | 4088 | 0.77 | 2068 | 0.39 | 0.027 | 0.51 | 0.3 | 0.36 | 21.4 | 0.6125 |
| Unknown 3 (UN03) | 6714 | 1.27 | 3123 | 0.59 | 0.027 | 0.5 | 0.3 | 0.46 | 27.5 | 0.6125 |
| Unnamed Stream 23_1 (UN23_1) | 15603 | 2.96 | 8228 | 1.56 | 0.027 | 0.51 | 0.3 | 0.81 | 48.4 | 0.6125 |
| Unnamed Stream 23_2 (UN23_2) | 2647 | 0.50 | 1462 | 0.28 | 0.031 | 0.49 | 0.3 | 0.27 | 16.3 | 0.6125 |
| Unnamed Stream 23_3 (UN23_3) | 5780 | 1.09 | 3289 | 0.62 | 0.024 | 0.53 | 0.3 | 0.47 | 28.3 | 0.6125 |
| Unnamed Stream 23A (UN23A) | 1956 | 0.37 | 1019 | 0.19 | 0.028 | 0.5 | 0.3 | 0.23 | 13.6 | 0.6125 |
| Unnamed Stream 24A Trib 1 (UN24AT1) | 2528 | 0.48 | 1309 | 0.25 | 0.035 | 0.47 | 0.3 | 0.25 | 14.9 | 0.6125 |
| Unnamed Stream 24A_1 (UN24A1) | 3346 | 0.63 | 1783 | 0.34 | 0.035 | 0.47 | 0.3 | 0.30 | 17.8 | 0.6125 |
| Unnamed Stream 24A_2 (UN24A2) | 4896 | 0.93 | 2532 | 0.48 | 0.031 | 0.49 | 0.3 | 0.38 | 23.1 | 0.6125 |
| Unnamed Stream 24B (UN24B) | 6535 | 1.24 | 3396 | 0.64 | 0.029 | 0.5 | 0.3 | 0.47 | 28.0 | 0.6125 |
| Unnamed Stream 24C (UN24C) | 3040 | 0.58 | 1489 | 0.28 | 0.041 | 0.45 | 0.3 | 0.26 | 15.6 | 0.6125 |
| Unnamed Stream 24D (UN24D) | 1354 | 0.26 | 733 | 0.14 | 0.030 | 0.49 | 0.3 | 0.18 | 10.8 | 0.6125 |
| Via Serena (VS_1) | 11544 | 2.19 | 6741 | 1.28 | 0.089 | 0.365 | 0.3 | 0.50 | 29.8 | 0.6125 |
| West of Rio Grande (WRG) | 28510 | 5.40 | 11973 | 2.27 | 0.009 | 0.72 | 0.3 | 1.53 | 91.6 | 0.6719 |
| West Montoya (WM) | 16386 | 3.10 | 8118 | 1.54 | 0.001 | 0.62 | 0.3 | 0.99 | 59.4 | 0.6719 |
| White Spur Drain_1 (WSD_1) | 4186 | 0.79 | 2324 | 0.44 | 0.004 | 0.38 | 0.3 | 0.28 | 16.6 | 0.6719 |
| White Spur Drain_2 (WSD_2) | 6462 | 1.22 | 3698 | 0.70 | 0.025 | 0.258 | 0.3 | 0.25 | 14.8 | 0.6125 |

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Table A-18. Summary of Lag Times for the West Central Region

| WEST CENTRAL REGION - USACE SNYDER LAG TIME CALCULATION | | | | | | | | | | |
|--|----------------------|---------------|-----------------------|---------------|-----------------------|----------------------|------------|------------------------|------------------------|----------------------|
| Watershed Name and HEC-HMS ID | L_L | | L_{CA} | | S_{ST} | C_T | N | T_{lag} | T_{lag} | C_P |
| | (ft) | (mile) | (ft) | (mile) | (ft/ft) | (-) | (-) | (hr) | (min) | (-) |
| Border Canal (Bcanal) | 11389 | 2.16 | 5845 | 1.11 | 0.001 | 0.610 | 0.3 | 0.79 | 47.5 | 0.6719 |
| Canterbury Channel (CBC_1) | 17367 | 3.29 | 9981 | 1.89 | 0.060 | 0.41 | 0.3 | 0.71 | 42.6 | 0.6125 |
| Flow Path Number 20_1 (FPN20_1) | 5537 | 1.05 | 3110 | 0.59 | 0.030 | 0.49 | 0.3 | 0.42 | 25.4 | 0.6125 |
| Flow Path Number 20_2 (FPN20_2) | 15662 | 2.97 | 8225 | 1.56 | 0.075 | 0.21 | 0.3 | 0.32 | 19.5 | 0.6125 |
| Flow Path Number 21_1 (FPN21_1) | 7059 | 1.34 | 3556 | 0.67 | 0.039 | 0.24 | 0.3 | 0.23 | 14.0 | 0.6125 |
| Flow Path Number 21_2 (FPN21_2) | 12086 | 2.29 | 6033 | 1.14 | 0.035 | 0.26 | 0.3 | 0.35 | 20.8 | 0.6125 |
| Flow Path Number 23 (FPN23_1) | 22242 | 4.21 | 9040 | 1.71 | 0.040 | 0.24 | 0.3 | 0.43 | 26.0 | 0.6125 |
| Industrial 1 (Ind1) | 10017 | 1.90 | 5119 | 0.97 | 0.047 | 0.44 | 0.3 | 0.53 | 31.7 | 0.6125 |
| Paragon Channel (PC_1) | 19477 | 3.69 | 10650 | 2.02 | 0.066 | 0.22 | 0.3 | 0.40 | 24.1 | 0.6125 |

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Table A-19a. Muskingum-Cunge Routing Inputs for the Central Region

| CENTRAL REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|--------------------------|--------------------------|-------------|---------------|---------------------|-----------|-------------------|--------------------|-------------|--------------------------------------|--|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| R_McKelligon Channel | S_McKelligon Dam | S_McKelligon_Reservoir_B | 1129.0 | 0.0453 | 0.0400 | Irregular | N/A | N/A | 21.8 | 1122 1256 1276 1500 1534 | 4315.4 4294.2 4293.6 4305.2 4313 |
| R_El Paso Rock Quarries | S_McKelligon_Reservoir_C | S_McKelligon_Reservoir_D | 618.0 | 0.0138 | 0.0400 | Trapezoid | 50 | 2.0 | 10.0 | N/A | N/A |
| R_McKelligon_D_Out | S_McKelligon_Reservoir_D | S_Van_Buren_Dam | 2455.3 | 0.0300 | 0.0160 | Trapezoid | 35 | 0.1 | 0.5 | N/A | N/A |
| R_Van_Buren_DS | J_Van_Buren_Ditch_US | S_Van_Buren_Dam | 2077.0 | 0.0470 | 0.0350 | Trapezoid | 15 | 1.0 | 5.1 | N/A | N/A |
| R_Pollard_Sacramento | J_Pollard_Sacramento | J_Pershing_Dam | 1087.8 | 0.0220 | 0.0160 | Trapezoid | 35 | 0.1 | 0.5 | N/A | N/A |
| R_Pollard_Ditch | A_Pollard Ditch | J_Pershing_Dam | 467.8 | 0.0176 | 0.0200 | Trapezoid | 8 | 1.0 | 5.0 | N/A | N/A |
| R_Gov_Hills_Conduit | J_Pershing_Dam | D_Boone_St_Basin | 9325.2 | 0.0112 | 0.013 | Trapezoid | 14 | 1.3 | 4.4 | 0 3.6 19.2 22.8 | 3788.415 3783.759 3783.617 3787.716 |
| R_Russel_Ditch | J_Russel_Ditch | D_Boone_St_Basin | 5975.0 | 0.0200 | 0.0160 | Trapezoid | 45 | 0.1 | 0.5 | N/A | N/A |
| R_Fort_Blvd_to_Copia_DitchUS | S_Fort_Blvd_Reservoir | J_Copia_Ditch_US | 6108.0 | 0.0600 | 0.0160 | Trapezoid | 40 | 0.1 | 0.5 | N/A | N/A |
| R_Copia_Ditch_DS | J_Copia_Ditch_US | J_Copia_Ditch_DS | 1998.1 | 0.0325 | 0.0130 | Trapezoid | 10 | 1.0 | 5.0 | N/A | N/A |
| R_Copia_St | J_Copia_Ditch_DS | J_Cebada_US | 885.0 | 0.0500 | 0.0160 | Trapezoid | 50 | 0.1 | 0.5 | N/A | N/A |
| R_Cebada_to_Cebada_Reservoir | J_Cebada_US | S_Cebada_Reservoir | 5340.0 | 0.0300 | 0.0160 | Trapezoid | 35 | 0.1 | 0.5 | N/A | N/A |
| R_Cebada_Reservoir_2 | J_Cebada_North | S_Cebada_Reservoir | 9148.0 | 0.0400 | 0.0160 | Trapezoid | 35 | 0.1 | 0.5 | N/A | N/A |
| R_Altura_to_Kentucky_Upper | S_Altura_Ave_Dam | S_Kentucky_Dam_Upper | 890.8 | 0.0590 | 0.0160 | Trapezoid | 35 | 0.1 | 0.5 | N/A | N/A |

Table A-19a. Muskingum-Cunge Routing Inputs for the Central Region (Continued)

| CENTRAL REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|----------------------------|------------------------|-------------|---------------|---------------------|-----------|-------------------|--------------------|-------------|-------------|-----|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| R_Cebada_Reservoir_3 | S_Kentucky_Dam_Lower | S_Cebada_Reservoir | 6633.4 | 0.0340 | 0.0160 | Trapezoid | 30 | 0.1 | 0.5 | N/A | N/A |
| R_Cebada_Reservoir_4 | S_Scenic_Dr_Dam | S_Cebada_Reservoir | 4800.0 | 0.0560 | 0.0160 | Trapezoid | 35 | 0.1 | 0.5 | N/A | N/A |
| R_Tremont_to_Magnolia | S_Tremont_Reservoir | S_Magnolia_Reservoir | 1585.5 | 0.0680 | 0.0160 | Trapezoid | 35 | 0.1 | 0.5 | N/A | N/A |
| R_Magnolia_to_Eucalyptus | S_Magnolia_Reservoir | J_Eucalyptus_to_Cebada | 2090.0 | 0.0230 | 0.0160 | Trapezoid | 55 | 0.1 | 0.5 | N/A | N/A |
| R_Dam_9 and_8_to_Dallas_Res | J_Dam_9_and_8 | S_Dallas_Reservoir | 2279.7 | 0.0400 | 0.0160 | Trapezoid | 50 | 0.1 | 0.5 | N/A | N/A |
| R_CottonDallas_to_Dallas_Res | J_Cotton_Dallas_US | S_Dallas_Reservoir | 4188.5 | 0.0330 | 0.0160 | Trapezoid | 35 | 0.1 | 0.5 | N/A | N/A |
| R_Paisano_Ditch | J_Nixon_Cypress_to_Central | J_Paisano_Ditch | 2038.3 | 0.0050 | 0.0350 | Trapezoid | 4 | 5.0 | 8.0 | N/A | N/A |

Table A-19b. Lag Routing Inputs for the Central Region

| CENTRAL REGION - LAG ROUTING (CONDUITS) | | | | | | |
|--|-----------------------------|------------------------------|---|--------------------|------------------------|------------------|
| Reach Name | From Element | To Element | Conduit Name | Length (ft) | Velocity (ft/s) | Lag (min) |
| R_Mountain_Avenue_Conduit | S_Van_Buren_Dam | S_Pershing Dam | Mountain Avenue Outlet Conduit | 8034.0 | 20.00 | 6.7 |
| R_FortBliss_Sump | J_FortBliss_Sump_Inflow | S_Pershing Dam | Fort Bliss Outfall Conduit | 9473.2 | 16.57 | 9.5 |
| R_Boone_to_Concordia | D_Boone_St_Basin | J_Concordia Cemetery | Gov. Hill Outlet Conduit (90" CBC) | 2530.0 | 15.00 | 2.8 |
| R_Concordia_to_Hardesty | J_Concordia Cemetery | J_Hardesty_to_Shelter | Gov. Hill Outlet Conduit (90" CBC) | 4296.0 | 15.00 | 4.8 |
| R_Hardesty_to_Gov_Hills_Out | J_Hardesty_to_Shelter | Gov_Hills_Outfall | Gov. Hill Outlet Conduit (90" CBC) | 2278.0 | 15.00 | 2.5 |
| R_24hr-Emergency Drain | J_24hr-Emergency Drain | D_Voone_St_Basin | 24hr-Emergency Drain (48in Conduit) | 4434.0 | 15.00 | 4.9 |
| R_Alameda_Avenue | J_Alameda Avenue | J_Blanco_Avenue | Ch 108 3X7 CBC Storm Drain | 1760.0 | 15.00 | 2.0 |
| R_Blanco_to_Comanche | J_Blanco_Avenue | J_Comanche_Avenue | Ch 108 3X7 CBC Storm Drain | 1399.0 | 15.00 | 1.6 |
| R_Comanche_to_Delta_Dr | J_Comanche_Avenue | J_Delta_Drive | Ch 108 3X7 CBC Storm Drain | 1135.0 | 15.00 | 1.3 |
| R_Delta_Dr_to_Channel108_Out | J_Delta_Drive | J_Channel 108 | Ch 108 3X7 CBC Storm Drain | 1366.0 | 15.00 | 1.5 |
| R_Channel108_to_Robert_Alva | J_Channel 108 | J_Robert_Alva_Channel | Ch 108 3X7 CBC Storm Drain | 1490.0 | 15.00 | 1.7 |
| R_Glenwood_to_Robert_Alva | J_Glenwood_Street_48in_RCP | J_Robert_Alva_Channel | Glenwood Street 48-inch rcp | 1445.0 | 8.93 | 2.7 |
| R_Paisano_to_Hills_Delta | J_Paisano and Delta to Tays | J_Hills Delta to Ninth | Hills Delta to Ninth | 1247.2 | 2.96 | 7.0 |
| R_hills_Delta_to_Seventh_Out | J_Hills Delta to Ninth | J_Seventh and Hills to Ninth | Hills Delta to Ninth | 1527.3 | 2.96 | 8.6 |
| R_Paisano_to_Ninth | J_El Paso Paisano US | J_El Paso Paisano to Ninth | El Paso Paisano to Ninth 54-inch RCP | 2330.0 | 6.92 | 5.6 |
| R_Sevnth_Vrain_West_to_Ninth | J_Seventh_Vrain_West | J_El Paso Paisano to Ninth | Seventh Chihauhuita to St. Vrain (west) 42-inch RCP | 573.9 | 4.09 | 2.3 |
| R_Sevnth_Vrain_East_to_Ninth | J_Seventh_Vrain_East | J_El Paso Paisano to Ninth | Seventh Chihauhuita to St. Vrain (east) 42-inch RCP | 5401.9 | 5.49 | 16.4 |
| R_Ninth_to_Outfall | J_El Paso Paisano to Ninth | J_El Paso Paisano Outfall | El Paso Paisano to Ninth 54-inch RCP | 1104.0 | 5.66 | 3.3 |
| R_Eucalyptus to Cebada | J_Eucalyptus_to_Cebada | S_Cebada_Reservoir | Eucalyptus_to_Cebada | 2734.0 | 15.00 | 3.0 |
| R_Cebada_Reservoir_Outfall | S_Cebada_Reservoir | J_Pera | Cebada Drainage Outfall | 3330.0 | 10.43 | 5.3 |

Table A-19b. Lag Routing Inputs for the Central Region (Continued)

| CENTRAL REGION - LAG ROUTING (CONDUITS) | | | | | | |
|--|----------------------------|----------------------------|--------------------------------------|--------------------|------------------------|------------------|
| Reach Name | From Element | To Element | Conduit Name | Length (ft) | Velocity (ft/s) | Lag (min) |
| R_Campbell_to_Dallas_Res | S_Campbell | S_Dallas_Reservoir | unknown | 3937.00 | 15.00 | 4.4 |
| R_Dallas_to_Cebada_Connector | D_IH_10_Dallas | J_Olive_to_Cebada | Olive and Cebada 2-5x5 CBC | 6693.20 | 5.17 | 21.6 |
| R_Pera_to_Cebada_Outfall | J_Pera | J_Cebada_Drainage_Outfall | Cebada Drainage Outfall | 1909.4 | 6.67 | 4.8 |
| R_Dallas_Res_to_San_Antonio | D_IH_10_Dallas | A_Dallas_San_Antonio | Dallas, San Antonio, and Lee | 3070.7 | 8.08 | 6.3 |
| R_San_Antonio_Hills | J_San_Antonio_Hills_to_Lee | A_Dallas_San_Antonio | San Antonio Hills to Lee 48-Inch RCP | 1916.0 | 3.65 | 8.7 |
| R_Dallas_System_Outfall | A_Dallas_San_Antonio | J_Dallas_System_Outfall | Dallas, San Antonio, and Lee | 1770.9 | 8.08 | 3.7 |
| R_Copia_St | L_Copia_Ditch_DS | J_Cebada_US | Copia Ditch | 1287.0 | 15.00 | 1.4 |
| R_Cebada_to_Cebada_Reservoir | J_Cebada_US | J_Cebada_Reservoir_Outfall | Cebada Drainage Outfall | 10092.0 | 15.00 | 11.2 |
| R_Houston_Magnolia | S_Magnolia_Reservoir | D_Houston_Elementary | unknown | 2197.0 | 15.00 | 2.4 |

Table A-20a. Kinematic Wave Routing Inputs for the East Side Region

| EAST SIDE REGION - KINEMATIC WAVE ROUTING | | | | | | | | |
|---|--------------|----------------|-------------|---------------|---------------------|-----------|-------------------|--------------------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) |
| Sunmount Channel | A_Sunmount | A_EID_1 | 825 | 0.005 | 0.3 | Trapezoid | 10 | 5 |
| Joe Battle Channel | A_Americas_5 | A_Americas_4 | 200 | 0.005 | 0.013 | Rectangle | 20 | |
| ARROYO-EAST | 124C | 124JE | 3000 | 0.022 | 0.013 | Trapezoid | 60 | 1 |
| ARROYO-EAST2 | 124JE | JB | 3000 | 0.017 | 0.013 | Trapezoid | 50 | 1 |
| ARROYO-WEST | 124A | 124JW | 2600 | 0.019 | 0.03 | Trapezoid | 50 | 1 |
| ARROYO-WEST2 | 124JW | JB | 3000 | 0.023 | 0.013 | Trapezoid | 60 | 1 |
| MV#14 | 9J | MISSION VALLEY | 404 | 0.00248 | 0.013 | Trapezoid | 60 | 1 |
| MV#20 | JB | MISSION VALLEY | 200 | 0.02 | 0.013 | Trapezoid | 100 | 1 |

Table A-20b. Kinematic Wave Routing Inputs (Conduits) for the East Side Region

| EAST SIDE REGION - KINEMATIC WAVE ROUTING (CONDUITS) | | | | | | | |
|--|------------------|----------------|--------------|-------------|---------------|--------------|---------------|
| Reach Name | From Element | To Element | Conduit Name | Length (ft) | Slope (ft/ft) | Mannings (n) | Diameter (ft) |
| VCNT-1 | CVP-1 | CVB-A | VCNT-1 | 1422 | 0.0165 | 0.013 | 4.5 |
| VCNT-2 | CVP-2 | CVB-A | VCNT-2 | 500 | 0.1025 | 0.013 | 6 |
| VCNT-3 | CVP-3 | CVB-B | VCNT-3 | 546 | 0.0751 | 0.013 | 4.5 |
| MV#11 | LOMALAND @ IH-10 | MISSION VALLEY | MV#11 | 260 | 0.005 | 0.013 | 3 |
| 9BR | 9B_P | 9J | 9BR | 2300 | 0.01 | 0.013 | 1.5 |
| 9CR | 9C_P | 9J | 9CR | 4500 | 0.01 | 0.013 | 1.5 |
| MV#17 | 90 | MISSION VALLEY | MV#17 | 260 | 0.00769 | 0.013 | 4 |
| MV#17a | 96J | MISSION VALLEY | MV#17a | 694 | 0.018 | 0.013 | 4.5 |
| MV#18 | 100 | MISSION VALLEY | MV#18 | 355 | 0.01127 | 0.013 | 3 |
| RCP375 | 96A | 96J | RCP375 | 1475 | 0.03 | 0.013 | 4.5 |

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Table A-21a. Muskingum-Cunge Routing Inputs for the Mission Valley Region

| MISSION VALLEY REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | |
|---|-------------------------------|-------------------------------|-------------|---------------|---------------------|-----------|-------------------|--------------------|-------------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) |
| R_Franklin Drain A | J_Middle Int w Franklin Drn | J_Franklin and Franklin Spur | 4921.4 | 0.1900 | 0.045 | Trapezoid | 12 | 2 | 15.0 |
| R_Franklin Drain Spur A | D_Playa and Playa Intercepto | R_Franklin Drain Spur B | 2598.3 | 0.0050 | 0.085 | Trapezoid | 14 | 2 | 10.0 |
| R_Franklin Drain Spur B | R_Franklin Drain Spur A | J_Franklin and Franklin Spur | 1475.6 | 0.0050 | 0.085 | Trapezoid | 12 | 2 | 14.0 |
| R_Franklin Drn to City Lmt A | J_Franklin and Franklin Spur | R_Franklin Drn to City Lmt B | 907.6 | 0.1900 | 0.045 | Trapezoid | 8 | 2 | 10.0 |
| R_Franklin Drn to City Lmt B | R_Franklin Drn to City Lmt A | J_Franklin Drain City Limit | 8727.0 | 0.1900 | 0.045 | Trapezoid | 15 | 1 | 15.0 |
| R_Lincoln Drain A | Source_CE Input | R_Lincoln Drain B | 5704.7 | 0.0050 | 0.030 | Trapezoid | 7 | 1 | 4.5 |
| R_Lincoln Drain B | R_Lincoln Drain A | J_Lincoln Drain Outlet | 2413.0 | 0.0050 | 0.035 | Trapezoid | 8 | 2 | 1 |
| R_Mesa Drain above Amer BsnA | J_Mesa Drain w Lomaland | R_Mesa Drain above Amer Bas B | 17030.8 | 0.0050 | 0.035 | Trapezoid | 15 | 2 | 9.0 |
| R_Mesa Drain above Amer BsnB | R_Mesa Drain above Amer Bas A | J_Mesa Drain w Americas Bsn | 1125.0 | 0.0050 | 0.035 | Trapezoid | 70 | 2 | 6.0 |
| R_Mesa Drain above Carolina | J_Mesa Drain w Phelps Dodge | J_Mesa Drain w Carolina Bsn | 946.3 | 0.0050 | 0.030 | Trapezoid | 10 | 1 | 9.0 |
| R_Mesa Drain below Carolina | J_Mesa Drain w Carolina Bsn | J_Mesa Drain w Lafayette Drw | 7140.6 | 0.0050 | 0.035 | Trapezoid | 10 | 2 | 9.0 |
| R_Mesa Drain above Lomaland | J_Mesa Drain w Lafayette Drw | J_Mesa Drain w Lomaland | 1981.8 | 0.0050 | 0.030 | Trapezoid | 15 | 2 | 9.0 |
| R_Mesa Drain to City Limit | D_Mesa to Mesa Interceptor | J_Mesa Drain w Americas Ten | 6002.6 | 0.0050 | 0.035 | Trapezoid | 15 | 2 | 9.0 |
| R_Mesa Interceptor above FL | D_Mesa to Mesa Interceptor | S_Featherlake Basin | 1004.1 | 0.0050 | 0.035 | Trapezoid | 70 | 1 | 15.0 |

Table A-21a. Muskingum-Cunge Routing Inputs for the Mission Valley Region (Continued)

| MISSION VALLEY REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | |
|---|------------------------------|------------------------------|-------------|---------------|---------------------|-----------|-------------------|--------------------|-------------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) |
| R_Mesa Interceptor blw FL A | S_Featherlake Basin | R_Mesa Interceptor blw FL B | 652.8 | 0.0050 | 0.035 | Trapezoid | 18 | 1 | 15.0 |
| R_Mesa Interceptor blw FL B | R_Mesa Interceptor blw FL A | J_Mesa Int w Middle Drain | 907.0 | 0.0050 | 0.035 | Trapezoid | 10 | 2 | 12.0 |
| R_Middle Drain to City Limit | D_Middle and Middle Int | J_Middle Drain City Limit | 5070.0 | 0.0010 | 0.080 | Trapezoid | 10 | 0 | 15.0 |
| R_Middle Drain to Intercept | J_Mesa Int w Middle Drain | J_Middle Drain w Middle Int | 1844.1 | 0.0010 | 0.013 | Trapezoid | 18 | 2 | 12.0 |
| R_Middle Interceptor A | D_Middle and Middle Int | J_Middle Int w Franklin Canl | 1402.0 | 0.0050 | 0.030 | Trapezoid | 21 | 1 | 11.0 |
| R_Middle Interceptor B | J_Middle Int w Franklin Canl | J_Middle Int w Franklin Drn | 2767.9 | 0.0050 | 0.050 | Trapezoid | 20 | 1 | 12.0 |
| R_Playa Drain Lower_A | J_Playa Drain Outlet Basin A | R_Playa Drain Conduit | 7359.3 | 0.0500 | 0.030 | Trapezoid | 10 | 1 | 15.0 |
| R_Playa Drain Lower_B | R_Playa Drain Conduit | R_Playa Drain Lower_C | 26719.3 | 0.0500 | 0.030 | Trapezoid | 10 | 1 | 15.0 |
| R_Playa Drain Lower_C | R_Playa Drain Lower_B | J_Playa Drain with Intercept | 4394.3 | 0.0567 | 0.030 | Trapezoid | 24 | 1 | 15.0 |
| R_Playa Drain Upper A | J_Playa Drain with Conduit | J_Playa Drn with North Loop | 1910.0 | 0.0050 | 0.030 | Trapezoid | 10 | 1 | 12.0 |
| R_Playa Drain Upper B | J_Playa Drn with North Loop | J_Playa Drain w Basin A | 6875.9 | 0.0050 | 0.020 | Trapezoid | 10 | 1 | 12.0 |

Table A-21b. Lag Routing Inputs for the Mission Valley Region

| MISSION VALLEY REGION - LAG ROUTING | | | | | | |
|-------------------------------------|------------------------|----------------------------|--------------|-------------|-----------------|-----------|
| Reach Name | From Element | To Element | Conduit Name | Length (ft) | Velocity (ft/s) | Lag (min) |
| R_Lincoln to Playa Conduit | J_Lincoln Drain Outlet | J_Playa Drain with Conduit | Ch35 - Cor3 | 2204.0 | 15.0 | 2.45 |
| R_Playa Drain Conduit | R_Playa Drain Lower_A | R_Playa Drain Lower_B | Ch89 - Cor1 | 4762.0 | 15.0 | 5.29 |

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Table A-22a. Muskingum-Cunge Routing Inputs for the Northeast Region

| NORTHEAST REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|--------------------|--------------------|-------------|---------------|---------------------|-------------|-------------------|--------------------|-------------|--|--|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| R_Army Ditch | D_Range Dam | J_Army Ditch | 4789.1 | 0.0015 | 0.030 | Eight Point | N/A | N/A | N/A | 0 5 17 23 41 47 50 55 | 3884.90 3884.90 3884.90 3880.90 3881.10 3885.60 3885.60 3885.60 |
| R_Bossworth U/S | A_Bossworth U/S | J_Bossworth Ch D/S | 4588.7 | 0.0360 | 0.035 | Trapezoid | 25 | 2 | 5.0 | N/A | N/A |
| R_Diana Ditch | J_Diana Ditch U/S | J_Diana Ditch D/S | 5903.4 | 0.0014 | 0.016 | Eight Point | N/A | N/A | 4.5 | 1200 1201 1202 1209 1218 1226 1227 1228 | 3883.80 3883.20 3883.20 3878.60 3878.60 3883.40 3883.40 3883.40 |
| R_Electric Ditch | J_Fairbanks Drive | J_Electric Ditch | 5609.5 | 0.0070 | 0.030 | Trapezoid | 20 | 7 | 2.0 | N/A | N/A |
| R_Fusselman Out | S_Fusselman Dam | S_Northgate Dam | 9263.3 | 0.0500 | 0.035 | Eight Point | N/A | N/A | N/A | 47.73 78.51 123.13 136.85 186.76 207.16 253.09 282.94 | 4272.89 4270.39 4268.32 4267.15 4270.38 4271.84 4273.42 4274.29 |
| R_Green Belt Levee | J_Green Belt Levee | D_NE Ponding | 8925.2 | 0.0071 | 0.040 | Trapezoid | 1000 | 4 | 5.0 | N/A | N/A |
| R_Hondo Pass Diversion | D_Hondo Pass | J_Diana Ditch U/S | 7886.4 | 0.0230 | 0.016 | Trapezoid | 65 | 0.1 | 0.5 | N/A | N/A |

Table A-22a. Muskingum-Cunge Routing Inputs for the Northeast Region (Continued)

| NORTHEAST REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|-----------------------------|-----------------------------|-------------|---------------|---------------------|-----------|-------------------|--------------------|-------------|-------------|-----|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| R_Keltner Dam Out | S_Keltner Dam | J_Ft Bliss Sump | 8939.9 | 0.0400 | 0.016 | Trapezoid | 36 | 0 | 0.5 | N/A | N/A |
| R_NE Pond Overflow | S_NE Pond Outer | J_RR Drain U/S of Tobin | 13842.1 | 0.0066 | 0.016 | Trapezoid | 36 | 0 | 0.5 | N/A | N/A |
| R_Northgate Dam Out | S_Northgate Dam | J_Northgate Dam Out | 5437.9 | 0.0077 | 0.035 | Trapezoid | 15 | 1 | 10.0 | N/A | N/A |
| R_PSB Ch 1 a | J_PSB Ch 1 Jct 1 | J_PSB Ch1 Jct2 | 7158.5 | 0.0050 | 0.016 | Trapezoid | 30 | 1 | 15.0 | N/A | N/A |
| R_PSB Ch 1 b | J_PSB Ch1 Jct2 | J_PSB Ch1 Jct3 | 6226.9 | 0.0050 | 0.016 | Trapezoid | 30 | 1 | 15.0 | N/A | N/A |
| R_PSB Ch 1 c | J_PSB Ch1 Jct3 | J_PSB Ch 1 D/S | 2816.8 | 0.0050 | 0.016 | Trapezoid | 30 | 1 | 15.0 | N/A | N/A |
| R_PSB Ch 2 a | J_PSB Ch 2 at Gateway | J_PSB Ch 2 at Rushing | 7202.4 | 0.0033 | 0.030 | Trapezoid | 30 | 1 | 5.0 | N/A | N/A |
| R_PSB Ch 2 b | J_PSB Ch 2 at Rushing | D_PSB Ch 2 D/S | 8659.4 | 0.0033 | 0.030 | Trapezoid | 30 | 1 | 5.0 | N/A | N/A |
| R_Range Dam Overflow | D_Range Dam | S_Range Basin | 3553.6 | 0.0110 | 0.016 | Trapezoid | 36 | 0 | 0.5 | N/A | N/A |
| R_RR Dr D/S | J_RR Ditch at Statler Ditch | J_RR Ditch Downstream | 3745.9 | 0.0014 | 0.016 | Trapezoid | 7 | 2 | 3.4 | N/A | N/A |
| R_RR Dr U/S Statler Ch | J_Tobin Drain and RR | J_RR Ditch at Statler Ditch | 3844.5 | 0.0042 | 0.030 | Trapezoid | 6 | 3 | 4.0 | N/A | N/A |
| R_Sunrise Channel | J_Sunrise Ch U/S | J_Sunrise Ch D/S | 3515.7 | 0.0123 | 0.016 | Trapezoid | 10 | 1 | 4.0 | N/A | N/A |

Table A-22a. Muskingum-Cunge Routing Inputs for the Northeast Region (Continued)

| NORTHEAST REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|-----------------------------|-----------------------------|-------------|---------------|---------------------|-------------|-------------------|--------------------|-------------|-------------|---------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| R_Tobin Drain U/S Army Ditch | J_Tobin Drain U/S Irwin H | J_Tobin Drain at Army Ditch | 2187.7 | 0.0018 | 0.030 | Eight Point | N/A | N/A | N/A | 1189.8 | 3885.10 |
| | | | | | | | | | | 1189.9 | 3885.10 |
| | | | | | | | | | | 1190.00 | 3885.10 |
| | | | | | | | | | | 1213.00 | 3875.00 |
| | | | | | | | | | | 1239.00 | 3875.70 |
| | | | | | | | | | | 1260.00 | 3885.70 |
| | | | | | | | | | | 1260.1 | 3885.70 |
| R_Tobin Drain U/S RR Ditch | J_Tobin Drain at Army Ditch | J_Tobin Drain D/S | 5473.1 | 0.0018 | 0.016 | Eight Point | N/A | N/A | N/A | 1260.2 | 3885.70 |
| | | | | | | | | | | 1049.80 | 3881.50 |
| | | | | | | | | | | 1049.90 | 3881.50 |
| | | | | | | | | | | 1050.00 | 3881.50 |
| | | | | | | | | | | 1054.00 | 3877.40 |
| | | | | | | | | | | 1075.00 | 3877.50 |
| | | | | | | | | | | 1080.00 | 3881.70 |
| R_W Fwy Ch_U/S | J_War Road Channel | J_W Fwy Ch U/S | 8006.8 | 0.0045 | 0.035 | Trapezoid | 32 | 1 | 10.0 | 1080.10 | 3881.70 |
| | | | | | | | | | | 1080.20 | 3881.70 |
| R_W Fwy Ch_D/S | J_W Fwy Ch U/S | J_W Fwy Ch D/S | 6794.5 | 0.0045 | 0.035 | Trapezoid | 43 | 2 | 6.0 | N/A | N/A |

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Table A-22b. Lag Routing Inputs for Northeast Region

| NORTHEAST REGION - LAG ROUTING (CONDUITS) | | | | | | |
|--|---------------------------|---------------------------|-----------------------|--------------------|------------------------|------------------|
| Reach Name | From Element | To Element | Conduit Name | Length (ft) | Velocity (ft/s) | Lag (min) |
| R_Ft Bliss Div Ch D/S | J_Ft Bliss Div Ch Dyer St | J_Ft Bliss Sump | Core of Engineer-CH63 | 6399.2 | 13.6 | 7.9 |
| R_Ft Bliss Div Ch U/S | J_Ft Bliss Div Ch U/S | J_Ft Bliss Div Ch Dyer St | Core of Engineer-CH63 | 8247.2 | 13.6 | 10.1 |
| R_Hondo Channel | D_Hondo Pass | S_Hondo Pass Basin | Hondo Pass Channel | 7006.9 | 16.7 | 7.0 |

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Table A-23. Routing Inputs for the Northwest Region

| NORTHWEST REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|--------------|------------|-------------|---------------|---------------------|-------------|-------------------|--------------------|-------------|-------------|---------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| A1 | M1 (A1_2) | M1 DS | 5637 | 0.0059 | 0.1 | Eight Point | N/A | N/A | N/A | 0.0 | 3753.0 |
| | | | | | | | | | | 743.0 | 3750.0 |
| | | | | | | | | | | 893.0 | 3749.0 |
| | | | | | | | | | | 932.0 | 3750.0 |
| | | | | | | | | | | 2313.0 | 3753.0 |
| | | | | | | | | | | 2313.1 | 3753.1 |
| | | | | | | | | | | 2313.2 | 3753.2 |
| | | | | | | | | | | 2313.3 | 3753.3 |
| BC_C1 | GC1,BC2 | BC_1,C1 | 4512 | 0.027 | 0.016 | Eight Point | N/A | N/A | N/A | 4861.2 | 4004.92 |
| | | | | | | | | | | 4977.2 | 4004.31 |
| | | | | | | | | | | 4985.0 | 4000.15 |
| | | | | | | | | | | 4991.2 | 3994.15 |
| | | | | | | | | | | 5009.1 | 3994.15 |
| | | | | | | | | | | 5011.3 | 4000.15 |
| | | | | | | | | | | 5017.6 | 4003.96 |
| | | | | | | | | | | 5587.3 | 4008.32 |
| BLC_C1 | BLC2,MDO1 | BLC2,BLC1 | 5661 | 0.007 | 0.013 | Circle | N/A | N/A | 11.0 | N/A | N/A |
| BLC_C2 | BLC3,TDO1 | BLC_2,C2 | 2864 | 0.0021 | 0.027 | Eight Point | N/A | N/A | N/A | 4893.1 | 3830.55 |
| | | | | | | | | | | 4976.2 | 3822.12 |
| | | | | | | | | | | 4995.8 | 3817.96 |
| | | | | | | | | | | 5003.5 | 3816.19 |
| | | | | | | | | | | 5003.8 | 3814.84 |
| | | | | | | | | | | 5010.5 | 3817.96 |
| | | | | | | | | | | 5059.1 | 3831.75 |
| | | | | | | | | | | 5074.5 | 3831.61 |

Table A-23. Routing Inputs for the Northwest Region (Continued)

| NORTHWEST REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|--------------|------------|-------------|---------------|---------------------|-------------|-------------------|--------------------|-------------|-------------|---------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| BLC_C3 | MD1,MBDO_1 | BLC_3,C3 | 2730 | 0.007 | 0.027 | Eight Point | N/A | N/A | N/A | 4892.4 | 3869.87 |
| | | | | | | | | | | 4916.7 | 3865.62 |
| | | | | | | | | | | 4996.5 | 3831.37 |
| | | | | | | | | | | 5004.9 | 3827.25 |
| | | | | | | | | | | 5005.0 | 3827.25 |
| | | | | | | | | | | 5014.4 | 3831.22 |
| | | | | | | | | | | 5098.5 | 3861.24 |
| | | | | | | | | | | 5098.6 | 3861.25 |
| BVC_C1 | BVC2,TBV1 | BVC_1,C1 | 2180 | 0.017 | 0.016 | Eight Point | N/A | N/A | N/A | 4920.0 | 3919.78 |
| | | | | | | | | | | 4944.9 | 3911.37 |
| | | | | | | | | | | 4972.5 | 3909.78 |
| | | | | | | | | | | 4976.1 | 3899.43 |
| | | | | | | | | | | 5013.3 | 3900.16 |
| | | | | | | | | | | 5019.8 | 3910.29 |
| | | | | | | | | | | 5035.4 | 3912.92 |
| | | | | | | | | | | 5094.4 | 3915.87 |
| BVC_C2 | CC | BVC_2,C2 | 2538 | 0.007 | 0.016 | Eight Point | N/A | N/A | N/A | 4891.0 | 3924.68 |
| | | | | | | | | | | 4916.0 | 3922.67 |
| | | | | | | | | | | 4981.9 | 3921.16 |
| | | | | | | | | | | 4985.3 | 3912.28 |
| | | | | | | | | | | 5014.8 | 3912.28 |
| | | | | | | | | | | 5020.2 | 3921.16 |
| | | | | | | | | | | 5072.2 | 3923.12 |
| | | | | | | | | | | 5075.2 | 3924.44 |

Table A-23. Routing Inputs for the Northwest Region (Continued)

| NORTHWEST REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|--------------|------------|-------------|---------------|---------------------|-------------|-------------------|--------------------|-------------|-------------|---------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| CC_C | SCC1,SSC1 | CC | 7398 | 0.037 | 0.017 | Eight Point | N/A | N/A | N/A | 4612.37 | 4056.00 |
| | | | | | | | | | | 4867.80 | 4055.56 |
| | | | | | | | | | | 4990.90 | 4051.95 |
| | | | | | | | | | | 4994.30 | 4043.84 |
| | | | | | | | | | | 5011.40 | 4043.80 |
| | | | | | | | | | | 5015.40 | 4051.08 |
| | | | | | | | | | | 5031.90 | 4054.31 |
| | | | | | | | | | | 5203.14 | 4056.00 |
| HR_C1 | RV1,HR2 | HR1,LDE1 | 4851 | 0.034 | 0.016 | Eight Point | N/A | N/A | N/A | 4956.3 | 4051.30 |
| | | | | | | | | | | 4968.4 | 4048.45 |
| | | | | | | | | | | 4970.0 | 4046.80 |
| | | | | | | | | | | 4982.3 | 4034.17 |
| | | | | | | | | | | 5010.8 | 4034.08 |
| | | | | | | | | | | 5036.2 | 4044.89 |
| | | | | | | | | | | 5048.3 | 4050.22 |
| | | | | | | | | | | 5302.4 | 4049.42 |
| HR_C2 | A1A,HR3 | HR_2,C2 | 5855 | 0.036 | 0.016 | Eight Point | N/A | N/A | N/A | 0.0 | 4227.0 |
| | | | | | | | | | | 215.0 | 4221.0 |
| | | | | | | | | | | 309.0 | 4212.0 |
| | | | | | | | | | | 316.0 | 4209.0 |
| | | | | | | | | | | 336.0 | 4209.0 |
| | | | | | | | | | | 346.0 | 4215.0 |
| | | | | | | | | | | 368.0 | 4218.0 |
| | | | | | | | | | | 567.0 | 4293.0 |
| KD_C | KD1 Dam | KD_Out | 9751 | 0.004 | 0.013 | Circle | N/A | N/A | 8.0 | N/A | N/A |

Table A-23. Routing Inputs for the Northwest Region (Continued)

| NORTHWEST REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|--------------|------------|-------------|---------------|---------------------|-------------|-------------------|--------------------|-------------|-------------|--------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| MBDO_C1 | MD1 Dam | MD1,MBDO_1 | 4812 | 0.024 | 0.016 | Eight Point | N/A | N/A | N/A | 0.0 | 3924.0 |
| | | | | | | | | | | 225.0 | 3921.0 |
| | | | | | | | | | | 280.0 | 3904.0 |
| | | | | | | | | | | 284.0 | 3901.0 |
| | | | | | | | | | | 289.0 | 3901.0 |
| | | | | | | | | | | 293.0 | 3904.0 |
| | | | | | | | | | | 299.0 | 3906.0 |
| | | | | | | | | | | 315.0 | 3906.0 |
| MD_C | MD2,WSD1 | MD_Out | 15180 | 0.00013 | 0.03 | Eight Point | N/A | N/A | N/A | 0.0 | 3739.0 |
| | | | | | | | | | | 76.0 | 3738.0 |
| | | | | | | | | | | 1478.0 | 3735.0 |
| | | | | | | | | | | 1485.0 | 3732.0 |
| | | | | | | | | | | 1507.0 | 3731.0 |
| | | | | | | | | | | 1519.0 | 3732.0 |
| | | | | | | | | | | 1532.0 | 3738.0 |
| | | | | | | | | | | 1565.0 | 3739.0 |
| MDO_C | Mesa Dam | MDO_1,C | 1636 | 0.02400 | 0.013 | Circle | N/A | N/A | 5.0 | N/A | N/A |
| MD2 | M1 DS | MD_2,C2 | 6746 | 0.00104 | 0.03 | Eight Point | N/A | N/A | N/A | 0.0 | 3747.0 |
| | | | | | | | | | | 2033.0 | 3744.0 |
| | | | | | | | | | | 2039.0 | 3741.0 |
| | | | | | | | | | | 2046.0 | 3738.0 |
| | | | | | | | | | | 2075.0 | 3738.0 |
| | | | | | | | | | | 2083.0 | 3741.0 |
| | | | | | | | | | | 2093.0 | 3744.0 |
| | | | | | | | | | | 3307.0 | 3747.0 |
| OD_C | OD Dam | Ox_Out | 3989 | 0.02100 | 0.013 | Circle | N/A | N/A | 3.0 | N/A | N/A |

Table A-23. Routing Inputs for the Northwest Region (Continued)

| NORTHWEST REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|--------------|--------------|-------------|---------------|---------------------|-------------|-------------------|--------------------|-------------|-------------|--------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| ODA_C1 | VS1,ODA2 | ER1,ODA1 | 13033 | 0.032 | 0.016 | Eight Point | N/A | N/A | N/A | 0.0 | 4131.0 |
| | | | | | | | | | | 1.0 | 4131.0 |
| | | | | | | | | | | 190.0 | 4122.0 |
| | | | | | | | | | | 219.0 | 4107.0 |
| | | | | | | | | | | 232.0 | 4107.0 |
| | | | | | | | | | | 268.0 | 4122.0 |
| | | | | | | | | | | 586.0 | 4131.0 |
| | | | | | | | | | | 586.1 | 4131.1 |
| SSC_C1 | SSC_2 | SSC_C1,SSC_1 | 3468 | 0.044 | 0.03 | Eight Point | N/A | N/A | N/A | 0.0 | 4275.0 |
| | | | | | | | | | | 30.0 | 4260.0 |
| | | | | | | | | | | 35.0 | 4257.0 |
| | | | | | | | | | | 50.0 | 4257.0 |
| | | | | | | | | | | 55.0 | 4260.0 |
| | | | | | | | | | | 229.0 | 4263.0 |
| | | | | | | | | | | 244.0 | 4269.0 |
| | | | | | | | | | | 246.0 | 4271.0 |
| TDO_C | Thorn Dam | TDO_1,C | 1468 | 0.033 | 0.033 | Eight Point | N/A | N/A | N/A | 0.0 | 3846.0 |
| | | | | | | | | | | 104.0 | 3837.0 |
| | | | | | | | | | | 405.0 | 3836.0 |
| | | | | | | | | | | 780.0 | 3837.0 |
| | | | | | | | | | | 854.0 | 3840.0 |
| | | | | | | | | | | 884.0 | 3846.0 |
| | | | | | | | | | | 885.0 | 3846.0 |
| | | | | | | | | | | 886.0 | 3846.0 |

Table A-23. Routing Inputs for the Northwest Region (Continued)

| NORTHWEST REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|--|--------------|--------------|-------------|---------------|---------------------|-------------|-------------------|--------------------|-------------|-------------|--------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| WSD_1_1 | DD3,WSD2 | WSD_1,WSD1_1 | 4182 | 0.003 | 0.035 | Eight Point | N/A | N/A | N/A | 0.0 | 3747.0 |
| | | | | | | | | | | 15.0 | 3747.0 |
| | | | | | | | | | | 16.0 | 3747.0 |
| | | | | | | | | | | 26.0 | 3744.0 |
| | | | | | | | | | | 33.0 | 3744.0 |
| | | | | | | | | | | 40.0 | 3747.0 |
| | | | | | | | | | | 66.0 | 3747.0 |
| | | | | | | | | | | 66.1 | 3747.1 |

Table A-24. Routing Inputs for the West Central Region

| WEST CENTRAL REGION - MUSKINGUM CUNGE ROUTING | | | | | | | | | | | |
|---|--------------|------------|-------------|---------------|---------------------|-------------|-------------------|--------------------|-------------|-------------|--------|
| Reach Name | From Element | To Element | Length (ft) | Slope (ft/ft) | Channel Manning's n | Shape | Trapezoid | | | Eight Point | |
| | | | | | | | Bottom Width (ft) | Side Slope (xH:1V) | Height (ft) | X | Y |
| FPN21_C1 | CBC1,FPN21 | FPN21_OUT | 1834 | 0.016 | 0.035 | Eight Point | N/A | N/A | N/A | 0.0 | 3795.0 |
| | | | | | | | | | | 26.0 | 3786.0 |
| | | | | | | | | | | 80.0 | 3747.0 |
| | | | | | | | | | | 202.0 | 3747.0 |
| | | | | | | | | | | 275.0 | 3774.0 |
| | | | | | | | | | | 275.1 | 3774.1 |
| | | | | | | | | | | 275.2 | 3774.2 |
| | | | | | | | | | | 275.3 | 3774.3 |

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Table A-25. Adjusted Curve Numbers for the Central Region

| CENTRAL REGION - ADJUSTED CURVE NUMBERS | | |
|--|-------------------|----------------------------|
| Watershed Name and HEC-HMS ID | Initial CN | Storage Adjusted CN |
| A_Louisiana_Dr_Dam_Upper | 87 | 87 |
| A_Magnolia_Reservoir | 92 | 67 |
| A_McKelligon_Reservoir_A | 89 | 38 |

Table A-26. Adjusted Curve Numbers for the East Side Region

| EAST SIDE REGION - ADJUSTED CURVE NUMBERS | | |
|--|-------------------|----------------------------|
| Watershed Name and HEC-HMS ID | Initial CN | Storage Adjusted CN |
| There were no adjustments made to watershed curve numbers. See Section A.8.3 for discussion. | | |

Table A-27. Adjusted Curve Numbers for the Mission Valley Region

| MISSION VALLEY REGION - ADJUSTED CURVE NUMBERS | | |
|---|-------------------|----------------------------|
| Watershed Name and HEC-HMS ID | Initial CN | Storage Adjusted CN |
| A_Below Featherlake Basin | 90 | 69 |
| A_Below Phelps Dodge Basin | 80 | 49 |
| A_Carolina Drive Basin | 78 | 38 |
| A_Feather Lake Basin | 78 | 44 |
| A_Franklin Drain B | 82 | 81 |
| A_Franklin Drn to City Limit | 76 | 76 |
| A_Lincoln Drain | 78 | 78 |
| A_Lomaland Basin | 64 | 62 |
| A_Mesa Drain A | 70 | 38 |
| A_Mesa Drain B | 73 | 63 |
| A_Mesa Drain C | 77 | 58 |
| A_Middle Drain A | 80 | 69 |
| A_North Loop Detention Basin | 78 | 44 |
| A_Playa Drain B | 83 | 70 |

Table A-28. Adjusted Curve Numbers for the Northeast Region

| NORTHEAST REGION - ADJUSTED CURVE NUMBERS | | |
|--|-------------------|----------------------------|
| Watershed Name and HEC-HMS ID | Initial CN | Storage Adjusted CN |
| A_Army Ditch | 82 | 79 |
| A_Diana Ditch U/S Sunrise Ch | 83 | 81 |
| A_Ft Bliss Diversion Channel D/S | 83 | 83 |
| A_Green Belt Levee D/S | 76 | 73 |
| A_NE Pond Outer | 81 | 81 |
| A_PSB Ch 1 D/S | 83 | 64 |
| A_PSB Ch 1 U/S Fannin Elem | 81 | 78 |
| A_PSB Ch 2 D/S | 76 | 75 |
| A_Railroad Drain U/S Tobin Drain | 78 | 78 |
| A_Tobin Drain U/S Irvin High | 80 | 74 |
| A_W Fwy Ch U/S | 76 | 71 |
| A_War Road Ch | 76 | 60 |

Table A-29. Adjusted Curve Numbers for the Northwest Region

| NORTHWEST REGION - ADJUSTED CURVE NUMBERS | | |
|--|-------------------|----------------------------|
| Watershed Name and HEC-HMS ID | Initial CN | Storage Adjusted CN |
| Arroyo 4 | 89 | 78 |
| Bandolero Channel_2 | 87 | 77 |
| Belvidere Channel | 88 | 82 |
| Borderland Heights Ponds | 70 | 33 |
| Doniphan Ditch_1 | 81 | 80 |
| Flow Path Number 38_4 | 85 | 33 |
| High Ridge_1 | 87 | 84 |
| Mace (Arroyo 1) | 74 | 33 |
| Montoya Drain_2 | 74 | 65 |
| Montoya Drain_3 | 77 | 73 |
| Mulberry Dam Outlet | 85 | 42 |
| Ojo De Agua_1 | 88 | 84 |
| Thunderbird Valley | 86 | 83 |
| West of Rio Grande | 66 | 65 |

Table A-30. Adjusted Curve Numbers for the West Central Region

| WEST CENTRAL REGION - ADJUSTED CURVE NUMBERS | | |
|---|-------------------|----------------------------|
| Watershed Name and HEC-HMS ID | Initial CN | Storage Adjusted CN |
| Flow Path Number 21_2 | 87 | 81 |

Table A-31. Estimation of Rainfall Depth by Annual Exceedance Probability

| Return Frequency | Total Rainfall Depth (inches) by Duration | | | | | | |
|--------------------------------------|---|------|------|------|------|-------|-------|
| | 1 hr | 2 hr | 3 hr | 4 hr | 6 hr | 12 hr | 24 hr |
| Central and Northeast El Paso | | | | | | | |
| 1 | 0.41 | 0.52 | 0.57 | 0.61 | 0.66 | 0.72 | 0.8 |
| 2 | 0.7 | 0.88 | 0.95 | 0.99 | 1.07 | 1.18 | 1.35 |
| 5 | 0.97 | 1.22 | 1.3 | 1.36 | 1.46 | 1.61 | 1.83 |
| 10 | 1.15 | 1.45 | 1.55 | 1.62 | 1.73 | 1.91 | 2.16 |
| 25 | 1.41 | 1.79 | 1.89 | 1.99 | 2.11 | 2.33 | 2.6 |
| 50 | 1.61 | 20.6 | 2.18 | 2.3 | 2.43 | 2.68 | 2.96 |
| 100 | 1.84 | 2.36 | 2.49 | 2.64 | 2.78 | 3.06 | 3.34 |
| 250 | 2.18 | 2.82 | 2.96 | 3.16 | 3.3 | 3.63 | 3.89 |
| 500 | 2.47 | 3.21 | 3.37 | 3.62 | 3.74 | 4.12 | 4.35 |
| West El Paso | | | | | | | |
| 1 | 0.43 | 0.54 | 0.59 | 0.63 | 0.68 | 0.74 | 0.83 |
| 2 | 0.73 | 0.91 | 0.98 | 1.03 | 1.11 | 1.22 | 1.4 |
| 5 | 1.04 | 1.31 | 1.4 | 1.47 | 1.58 | 1.74 | 1.98 |
| 10 | 1.28 | 1.62 | 1.72 | 1.81 | 1.93 | 2.13 | 2.41 |
| 25 | 1.64 | 2.08 | 2.2 | 2.32 | 2.46 | 2.72 | 3.03 |
| 50 | 1.95 | 2.49 | 2.63 | 2.77 | 2.93 | 3.23 | 3.57 |
| 100 | 2.31 | 2.96 | 3.12 | 3.31 | 3.47 | 3.83 | 4.18 |
| 250 | 2.86 | 3.7 | 3.89 | 4.15 | 4.33 | 4.76 | 5.11 |
| 500 | 3.36 | 4.36 | 4.58 | 4.92 | 5.09 | 5.6 | 5.92 |
| East El Paso | | | | | | | |
| 1 | 0.35 | 0.45 | 0.49 | 0.52 | 0.56 | 0.61 | 0.69 |
| 2 | 0.64 | 0.8 | 0.87 | 0.91 | 0.98 | 1.08 | 1.23 |
| 5 | 0.97 | 1.22 | 1.3 | 1.36 | 1.46 | 1.61 | 1.83 |
| 10 | 1.22 | 1.54 | 1.64 | 1.72 | 1.84 | 2.02 | 2.29 |
| 25 | 1.61 | 2.05 | 2.17 | 2.28 | 2.42 | 2.67 | 2.98 |
| 50 | 1.96 | 2.5 | 2.64 | 2.79 | 2.95 | 3.25 | 3.59 |
| 100 | 2.38 | 3.05 | 3.21 | 3.41 | 3.58 | 3.94 | 4.3 |
| 250 | 3.04 | 3.92 | 4.12 | 4.4 | 4.59 | 5.05 | 5.42 |
| 500 | 3.65 | 4.73 | 4.97 | 5.34 | 5.52 | 6.08 | 6.42 |

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Table A-32. Central Region Complete HEC-HMS Results for 10 - 100-Year Storms

| CENTRAL REGION - HEC-HMS RESULTS | | | | | | | |
|----------------------------------|------------------------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers(s) | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-40, A-41 | A_Alameda Avenue | 0.299 | | | | 11 | |
| A-36, A-37 | A_Altura_Ave_Dam | 0.122 | 69 | 102 | 128 | 157 | 242 |
| A-40, A-41 | A_Blanco Avenue | 0.087 | | | | 58 | |
| A-34, A-35 | A_Boone_St_Basin | 0.398 | 176 | 264 | 337 | 419 | 658 |
| A-40, A-41 | A_Cebada_Drainage_Outfall | 0.273 | | | | 341 | |
| A-38, A-39 | A_Cebada_Reservoir | 0.699 | 435 | 626 | 777 | 948 | 1431 |
| A-34, A-35 | A_Cemex_Spillway | 0.923 | 575 | 793 | 963 | 1156 | 1694 |
| A-40, A-41 | A_Channel_108_Discharge | 0.031 | | | | 76 | |
| A-40, A-41 | A_Comanche Avenue | 0.136 | | | | 233 | |
| A-34, A-35 | A_Concordia_Cemetery | 0.305 | 171 | 251 | 315 | 388 | 597 |
| A-36, A-37 | A_Copia_Ditch_DS | 0.160 | 174 | 230 | 272 | 320 | 451 |
| A-36, A-37 | A_Copia_Ditch_US | 0.411 | 355 | 474 | 566 | 670 | 958 |
| A-38, A-39 | A_Cotton_Dallas_DS | 0.375 | 428 | 567 | 670 | 670 | 670 |
| A-38, A-39 | A_Cotton_Dallas_US | 1.047 | 828 | 1121 | 1342 | 1342 | 1342 |
| A-38, A-39 | A_Dam_No_10 | 0.073 | 88 | 123 | 150 | 150 | 150 |
| A-38, A-39 | A_Dam_No_8 | 0.052 | 49 | 71 | 88 | 88 | 88 |
| A-38, A-39 | A_Dam_No_9 | 0.033 | 39 | 54 | 65 | 65 | 65 |
| A-40, A-41 | A_Delta_Drive | 0.076 | | | | 146 | |
| A-38, A-39 | A_Eucalyptus_to_Cebada | 0.226 | 244 | 319 | 374 | 437 | 609 |
| A-36, A-37 | A_Fort_Blvd_Reservoir | 0.219 | 123 | 181 | 227 | 280 | 431 |
| A-40, A-41 | A_Glenwood_Street_48in_RCP | 0.062 | | | | 79 | |
| A-34, A-35 | A_Hardesty_to_Shelter | 0.018 | 16 | 23 | 27 | 33 | 48 |
| A-38, A-39 | A_Houston_Elementary | 0.498 | 279 | 377 | 453 | 538 | 774 |
| A-36, A-37 | A_Kentucky_Dam_Lower | 0.124 | 62 | 91 | 114 | 140 | 214 |
| A-36, A-37 | A_Kentucky_Dam_Upper | 0.057 | 56 | 79 | 98 | 118 | 176 |
| A-36, A-37 | A_Louisiana_Dr_Dam_Lower | 0.049 | 60 | 82 | 99 | 118 | 171 |
| A-36, A-37 | A_Louisiana_Dr_Dam_Upper | 0.137 | 105 | 151 | 188 | 231 | 351 |
| A-34, A-35 | A_Lower_Durazno | 1.037 | 125 | 245 | 353 | 485 | 892 |
| A-38, A-39 | A_Magnolia_Reservoir | 0.095 | 10 | 25 | 40 | 57 | 118 |
| A-34, A-35 | A_McKelligon_Dam | 2.168 | 839 | 1200 | 1485 | 1809 | 2724 |
| A-34, A-35 | A_McKelligon_Reservoir_A | 0.038 | 38 | 54 | 66 | 80 | 119 |
| A-34, A-35 | A_McKelligon_Reservoir_B | 0.104 | 93 | 132 | 163 | 197 | 294 |
| A-34, A-35 | A_McKelligon_Reservoir_C | 0.009 | 8 | 11 | 14 | 18 | 27 |
| A-38, A-39 | A_McKelligon_Reservoir_D | 0.006 | 9 | 12 | 14 | 16 | 22 |
| A-36, A-37 | A_Memorial_Park | 0.151 | 130 | 179 | 216 | 257 | 373 |
| A-36, A-37 | A_Memphis_Dam_Lower | 0.015 | 13 | 19 | 24 | 30 | 45 |
| A-36, A-37 | A_Memphis_Dam_Upper | 0.249 | 135 | 200 | 252 | 312 | 481 |
| A-40, A-41 | A_Modesto Ditch | 0.117 | | | | 218 | |
| A-34, A-35 | A_Mountain_Ave_Outlet_Condui | 0.876 | 695 | 934 | 1116 | 1321 | 1890 |
| A-40, A-41 | A_Nixon_Cypress_to_Central | 0.048 | | | | 110 | |
| A-38, A-39 | A_Ohio_St_Reservoir | 0.009 | 10 | 14 | 17 | 20 | 29 |
| A-38, A-39 | A_Ohio_St_Reservoir_DS | 0.002 | 0 | 0 | 0 | 0 | 0 |
| A-40, A-41 | A_Paisano Ditch | 0.223 | | | | 347 | |
| A-34, A-35 | A_Pershing Dam | 0.193 | 82 | 127 | 164 | 207 | 331 |
| A-34, A-35 | A_Pollard Ditch | 0.113 | 115 | 152 | 180 | 211 | 298 |
| A-34, A-35 | A_Pollard_Sacramento | 0.021 | 28 | 37 | 44 | 52 | 73 |
| A-40, A-41 | A_Robert_Alva_Channel | 0.442 | | | | 486 | |
| A-36, A-37 | A_Russel_Ditch_DS | 0.123 | 131 | 175 | 208 | 246 | 351 |
| A-34, A-35 | A_Russel_Ditch_US | 0.434 | 424 | 564 | 671 | 791 | 1123 |
| A-34, A-35 | A_Saipan | 0.152 | 141 | 205 | 258 | 316 | 484 |

**Table A-32. Central Region Complete HEC-HMS Results for 10 - 100-Year Storms
(Continued)**

| CENTRAL REGION - HEC-HMS RESULTS | | | | | | | |
|-----------------------------------|------------------------------|----------------------------|------------------|------------------|------------------|-------------------|-------------------|
| Schematic Figure Numbers(s) | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-38, A-39 | A_San_Diego_Dam | 0.122 | 92 | 134 | 168 | 207 | 316 |
| A-36, A-37 | A_Scenic_Dr_Dam | 0.126 | 75 | 111 | 139 | 172 | 264 |
| A-38, A-39 | A_Tremont_Reservoir | 0.005 | 7 | 9 | 11 | 13 | 19 |
| A-34, A-35 | A_Upper_Durazno | 0.018 | 11 | 17 | 22 | 28 | 46 |
| A-34, A-35 | A_Van_Buren_Dam | 0.279 | 207 | 278 | 333 | 395 | 565 |
| A-34, A-35 | A_Van_Buren_Ditch | 0.120 | 73 | 103 | 126 | 153 | 227 |
| A-38, A-39 | D_3708 | 1.580 | 530 | 530 | 530 | 530 | 530 |
| A-34, A-35 | D_Boone_St_Basin | 5.682 | 375 | 375 | 375 | 375 | 375 |
| A-36, A-37 | D_Capacity of 60" Conduit | 0.956 | 271 | 338 | 434 | 568 | 890 |
| A-34, A-35 | D_Government6_Hills | 4.850 | 222 | 270 | 307 | 348 | 462 |
| A-36, A-37 | D_Houston_Elementary | 0.498 | 250 | 250 | 250 | 250 | 250 |
| A-38, A-39 | D_IH_10_Dallas | 1.580 | 216 | 216 | 216 | 216 | 216 |
| A-38, A-39 | D_Over_Cebada_Magnolia_Ridge | 0.000 | 0 | 0 | 0 | 0 | 0 |
| A-38, A-39 | D_Overflow_Beneath_I-10 | 0.000 | 0 | 0 | 0 | 0 | 0 |
| A-38, A-39 | D_Overflow_Raynor_St | 0.000 | 0 | 0 | 0 | 0 | 0 |
| A-38, A-39 | J_24hr-Emergency_Drain | 0.000 | 100 | 100 | 100 | 100 | 100 |
| A-40, A-41 | J_Alameda Avenue | 0.299 | | | | 11 | |
| A-40, A-41 | J_Blanco_Avenue | 0.386 | | | | 59 | |
| A-40, A-41 | J_Cebada_Drainage_Outfall | 0.544 | | | | 780 | |
| A-36, A-37 | J_Cebada_Inflow | 2.641 | 1186 | 1801 | 2480 | 3031 | 4682 |
| A-36, A-37 | J_Cebada_North | 0.450 | 75 | 236 | 355 | 465 | 736 |
| A-36, A-37 | J_Cebada_Reservoir_Outfall | 1.064 | 725 | 981 | 1171 | 1386 | 2134 |
| A-38, A-39 | J_Cebada_Total | 0.878 | 239 | 451 | 589 | 732 | 1101 |
| A-36, A-37 | J_Cebada_US | 1.064 | 738 | 988 | 1178 | 1393 | 2173 |
| A-40, A-41 | J_Channel 108 | 0.630 | | | | 435 | |
| A-40, A-41 | J_Comanche Avenue | 0.522 | | | | 249 | |
| A-34, A-35 | J_Concordia Cemetery | 5.834 | 504 | 580 | 633 | 691 | 859 |
| A-36, A-37 | J_Copia_Ditch_DS | 0.790 | 510 | 684 | 817 | 966 | 1635 |
| A-36, A-37 | J_Copia_Ditch_US | 0.630 | 355 | 474 | 566 | 768 | 1294 |
| A-38, A-39 | J_Cotton_Dallas_US | 0.073 | 0 | 0 | 0 | 0 | 0 |
| A-38, A-39 | J_Dallas_Reservoir | 1.580 | 1248 | 1673 | 1988 | 1988 | 1988 |
| A-38, A-39 | J_Dallas_West | 1.580 | 216 | 216 | 216 | 216 | 216 |
| A-38, A-39 | J_Dam_9_and_8 | 0.085 | 71 | 88 | 97 | 97 | 97 |
| A-40, A-41 | J_Delta_Drive | 0.599 | | | | 376 | |
| A-38, A-39 | J_Diversion | 0.000 | 314 | 314 | 314 | 314 | 314 |
| A-36, A-37 | J_Eucalyptus_to_Cebada | 0.956 | 371 | 438 | 534 | 668 | 990 |
| A-34, A-35 | J_Fort Bliss Channel Inflow | 0.000 | 200 | 200 | 200 | 200 | 200 |
| A-40, A-41 | J_Glenwood_Street_48in_RCP | 0.062 | | | | 79 | |
| A-34, A-35 | J_Gov Hills Central Inflow | 5.284 | 615 | 799 | 951 | 1098 | 1557 |
| A-34, A-35 | J_Gov Hills North Inflow | 4.850 | 218 | 264 | 300 | 336 | 445 |
| A-34, A-35 | J_Gov Hills South Inflow | 5.682 | 790 | 1063 | 1288 | 1517 | 2214 |
| A-34, A-35 | J_Gov_Hills_Outfall | 5.852 | 496 | 574 | 629 | 687 | 852 |
| A-34, A-35 | J_Hardesty_to_Shelter | 5.852 | 515 | 592 | 645 | 705 | 878 |
| A-36, A-37 | J_Houston_to_Cebada | 0.699 | 435 | 673 | 880 | 1116 | 1775 |
| A-36, A-37 | J_I-10 Overtopping Flow | 0.956 | 271 | 338 | 434 | 568 | 890 |
| A-34, A-35 | J_Inflow from Pershing Dam | 4.850 | 322 | 370 | 407 | 448 | 562 |
| A-36, A-37 | J_Inflow to San Diego Dam | 0.122 | 92 | 134 | 168 | 207 | 316 |
| A-38, A-39 | J_Inflow_Dam_No_10 | 0.073 | 88 | 123 | 150 | 150 | 150 |

**Table A-32. Central Region Complete HEC-HMS Results for 10 - 100-Year Storms
(Continued)**

| CENTRAL REGION - HEC-HMS RESULTS | | | | | | | |
|-----------------------------------|------------------------------|----------------------------|------------------|------------------|------------------|-------------------|-------------------|
| Schematic Figure Numbers(s) | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-38, A-39 | J_Inflow_Dam_No_8 | 0.052 | 49 | 71 | 88 | 88 | 88 |
| A-38, A-39 | J_Inflow_Dam_No_9 | 0.033 | 39 | 54 | 65 | 65 | 65 |
| A-36, A-37 | J_Inflow_Ft_Bldv_Res | 0.219 | 123 | 181 | 227 | 280 | 431 |
| A-36, A-37 | J_Inflow_Kentucky_Dam_Lower | 0.303 | 62 | 91 | 114 | 140 | 285 |
| A-36, A-37 | J_Inflow_Kentucky_Dam_Upper | 0.179 | 61 | 117 | 165 | 211 | 348 |
| A-38, A-39 | J_Inflow_Louisiana_Dam_Lower | 0.186 | 164 | 232 | 287 | 348 | 522 |
| A-36, A-37 | J_Inflow_Memphis_Dam | 0.264 | 146 | 215 | 271 | 334 | 515 |
| A-36, A-37 | J_Inflow_Ohio_St_Res | 0.130 | 69 | 91 | 105 | 118 | 148 |
| A-36, A-37 | J_Inflow_Tremont_Reservoir | 0.138 | 47 | 54 | 58 | 99 | 152 |
| A-34, A-35 | J_Inflow_Van_Buren_Dam | 3.647 | 833 | 1146 | 1386 | 1658 | 2421 |
| A-34, A-35 | J_Lower_Durazno_Out | 1.360 | 0 | 0 | 0 | 0 | 42 |
| A-34, A-35 | J_Mckelligon Res A Inflow | 2.206 | 38 | 54 | 66 | 113 | 209 |
| A-34, A-35 | J_Mckelligon Res B Inflow | 2.310 | 93 | 132 | 163 | 197 | 294 |
| A-34, A-35 | J_Mckelligon Res C Inflow | 2.318 | 79 | 134 | 165 | 199 | 297 |
| A-34, A-35 | J_Mckelligon Res D Inflow | 2.324 | 9 | 13 | 31 | 102 | 217 |
| A-40, A-41 | J_Modesto Ditch | 0.117 | | | | 218 | |
| A-40, A-41 | J_Nixon_Cypress_to_Central | 0.048 | | | | 110 | |
| A-40, A-41 | J_Outflow from Robert Alva | 0.062 | | | | 75 | |
| A-38, A-39 | J_Overflow_3708 | 0.000 | 47 | 120 | 160 | 160 | 160 |
| A-40, A-41 | J_Paisano_Ditch | 0.271 | | | | 453 | |
| A-40, A-41 | J_Pera | 0.271 | | | | 453 | |
| A-34, A-35 | J_Pershing_Dam | 4.850 | 322 | 370 | 407 | 448 | 562 |
| A-34, A-35 | J_Pollard Ditch Inflow | 0.113 | 113 | 150 | 178 | 209 | 295 |
| A-34, A-35 | J_Pollard_Sacramento | 0.021 | 28 | 37 | 44 | 52 | 73 |
| A-40, A-41 | J_Robert_Alva_Channel | 1.134 | | | | 971 | |
| A-34, A-35 | J_Russel Ditch | 0.434 | 424 | 564 | 671 | 791 | 1123 |
| A-34, A-35 | J_Van Buren Ditch Inflow | 1.044 | 626 | 870 | 1058 | 1272 | 1868 |
| A-34, A-35 | J_Van_Buren_Ditch_US | 0.923 | 573 | 790 | 958 | 1148 | 1679 |
| A-34, A-35 | R_24hr-Emergency Drain | 0.000 | 100 | 100 | 100 | 100 | 100 |
| A-40, A-41 | R_Alameda_Avenue | 0.299 | | | | 11 | |
| A-36, A-37 | R_Altura_to_Kentucky_Upper | 0.122 | 46 | 89 | 115 | 150 | 234 |
| A-40, A-41 | R_Blanco_to_Comanche | 0.386 | | | | 59 | |
| A-34, A-35 | R_Boone_to_Concordia | 5.682 | 375 | 375 | 375 | 375 | 375 |
| A-36, A-37 | R_Cebada_Reservoir_2 | 0.450 | 72 | 232 | 344 | 457 | 734 |
| A-36, A-37 | R_Cebada_Reservoir_3 | 0.303 | 65 | 92 | 111 | 137 | 283 |
| A-36, A-37 | R_Cebada_Reservoir_4 | 0.126 | 29 | 35 | 39 | 43 | 52 |
| A-36, A-37 | R_Cebada_to_Cebada_Reservoir | 1.064 | 725 | 981 | 1171 | 1386 | 2134 |
| A-40, A-41 | R_Channel108_to_Robert_Alva | 0.630 | | | | 420 | |
| A-40, A-41 | R_Comanche_to_Delta_Dr | 0.522 | | | | 247 | |
| A-34, A-35 | R_Concordia_to_Hardesty | 5.834 | 499 | 569 | 618 | 673 | 829 |
| A-36, A-37 | R_Copia_Ditch_DS | 0.630 | 354 | 474 | 564 | 751 | 1257 |
| A-38, A-39 | R_CottonDallas_to_Dallas_Res | 0.073 | 0 | 0 | 0 | 0 | 0 |
| A-38, A-39 | R_Dallas_to_Cebada_Connector | 0.000 | 314 | 314 | 314 | 314 | 314 |
| A-38, A-39 | R_Dam_9_and_8_to_Dallas_Res | 0.085 | 68 | 87 | 97 | 97 | 97 |
| A-40, A-41 | R_Delta_Dr_to_Channel108_Out | 0.599 | | | | 363 | |
| A-34, A-35 | R_El Paso Rock Quarries | 2.318 | 0 | 13 | 31 | 102 | 217 |
| A-36, A-37 | R_Eucalyptus to Cebada | 0.000 | 100 | 100 | 100 | 100 | 100 |
| A-36, A-37 | R_Fort_Bldv_to_Copia_DitchUS | 0.219 | 43 | 110 | 169 | 241 | 403 |

**Table A-32. Central Region Complete HEC-HMS Results for 10 - 100-Year Storms
(Continued)**

| CENTRAL REGION - HEC-HMS RESULTS | | | | | | | |
|-----------------------------------|-----------------------------|----------------------------|------------------|------------------|------------------|-------------------|-------------------|
| Schematic Figure Numbers(s) | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-34, A-35 | R_FortBliss Inflow | 0.000 | 200 | 200 | 200 | 200 | 200 |
| A-40, A-41 | R_Glenwood_to_Robert_Alva | 0.062 | | | | 75 | |
| A-34, A-35 | R_Gov_Hills_Conduit | 4.850 | 218 | 264 | 300 | 336 | 445 |
| A-34, A-35 | R_Hardesty_to_Gov_Hills_Out | 5.852 | 496 | 574 | 629 | 687 | 852 |
| A-36, A-37 | R_Houston_Magnolia | 0.498 | 250 | 250 | 250 | 250 | 250 |
| A-36, A-37 | R_Magnolia_to_Eucalyptus | 0.731 | 288 | 301 | 309 | 327 | 406 |
| A-34, A-35 | R_Mckelligon_Channel | 2.206 | 0 | 3 | 30 | 112 | 207 |
| A-34, A-35 | R_Mckelligon_D_Out | 2.324 | 7 | 12 | 31 | 95 | 217 |
| A-34, A-35 | R_Mountain_Avenue_Conduit | 3.647 | 820 | 1053 | 1133 | 1205 | 1359 |
| A-40, A-41 | R_Paisano_Ditch | 0.048 | | | | 106 | |
| A-40, A-41 | R_Pera_to_Cebada_Outfall | 0.271 | | | | 439 | |
| A-34, A-35 | R_Pollard_Ditch | 0.113 | 113 | 150 | 178 | 209 | 295 |
| A-34, A-35 | R_Pollard_Sacramento | 0.021 | 25 | 33 | 39 | 47 | 67 |
| A-34, A-35 | R_Russel_Ditch | 0.434 | 410 | 545 | 659 | 767 | 1112 |
| A-36, A-37 | R_Tremont_to_Magnolia | 0.138 | 40 | 46 | 49 | 54 | 133 |
| A-38, A-39 | R_Van_Buren_DS | 0.923 | 557 | 772 | 939 | 1128 | 1655 |
| A-36, A-37 | S_Altura_Ave_Dam | 0.122 | 49 | 90 | 121 | 154 | 236 |
| A-36, A-37 | S_Cebada_Reservoir | 2.641 | 530 | 571 | 600 | 637 | 742 |
| A-34, A-35 | S_Cemex_Spilway | 0.923 | 573 | 790 | 958 | 1148 | 1679 |
| A-38, A-39 | S_Dallas_Reservoir | 1.580 | 577 | 650 | 690 | 690 | 690 |
| A-38, A-39 | S_Dam_No_10 | 0.073 | 0 | 0 | 0 | 0 | 0 |
| A-38, A-39 | S_Dam_No_8 | 0.052 | 36 | 43 | 49 | 49 | 49 |
| A-38, A-39 | S_Dam_NO_9 | 0.033 | 36 | 45 | 49 | 49 | 49 |
| A-36, A-37 | S_Fort_Blvd_Reservoir | 0.219 | 43 | 111 | 169 | 242 | 410 |
| A-36, A-37 | S_Kentucky_Dam_Lower | 0.303 | 68 | 95 | 112 | 138 | 285 |
| A-36, A-37 | S_Kentucky_Dam_Upper | 0.179 | 2 | 10 | 31 | 57 | 134 |
| A-36, A-37 | S_Louisiana_Dam_Lower | 0.186 | 25 | 79 | 124 | 163 | 246 |
| A-34, A-35 | S_Lower_Durazno | 1.360 | 0 | 0 | 0 | 0 | 42 |
| A-36, A-37 | S_Magnolia_Reservoir | 0.731 | 291 | 301 | 309 | 330 | 411 |
| A-34, A-35 | S_Mckelligon_Dam | 2.168 | 0 | 4 | 30 | 111 | 205 |
| A-34, A-35 | S_Mckelligon_Reservoir_A | 2.206 | 0 | 3 | 30 | 112 | 207 |
| A-34, A-35 | S_Mckelligon_Reservoir_B | 2.310 | 73 | 126 | 154 | 186 | 277 |
| A-34, A-35 | S_Mckelligon_Reservoir_C | 2.318 | 0 | 13 | 31 | 103 | 217 |
| A-34, A-35 | S_Mckelligon_Reservoir_D | 2.324 | 7 | 12 | 31 | 95 | 218 |
| A-36, A-37 | S_Memorial_Park | 0.941 | 631 | 847 | 1010 | 1196 | 1893 |
| A-36, A-37 | S_Memphis_Dam_Lower | 0.264 | 72 | 157 | 232 | 308 | 494 |
| A-36, A-37 | S_Ohio_St_Reservoir | 0.130 | 46 | 53 | 57 | 97 | 148 |
| A-34, A-35 | S_Pershing_Dam | 4.716 | 225 | 240 | 252 | 263 | 298 |
| A-36, A-37 | S_San_Diego_Dam | 0.122 | 64 | 85 | 97 | 110 | 138 |
| A-36, A-37 | S_Scenic_Dr_Dam | 0.126 | 29 | 35 | 39 | 43 | 52 |
| A-36, A-37 | S_Tremont_Reservoir | 0.138 | 40 | 46 | 49 | 54 | 142 |
| A-34, A-35 | S_Upper_Durazno | 0.323 | 0 | 0 | 50 | 222 | 1531 |
| A-34, A-35 | S_Van_Buren_Dam | 3.647 | 834 | 1058 | 1135 | 1206 | 1359 |
| A-34, A-35 | Source_NE_Input | Not Specified | 200 | 200 | 200 | 200 | 200 |

Table A-33. East Side Region Complete HEC-HMS Results for 10 - 100-Year Storms

| EAST SIDE REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|------------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-42, A-45 | A-PD-1 | 0.7542 | 341 | 492 | 618 | 763 | 1178 |
| A-42, A-45 | A-PD-1A | 0.1608 | 161 | 220 | 269 | 324 | 478 |
| A-42, A-45 | A_Sunmount | 0.2858 | 153 | 226 | 289 | 361 | 569 |
| A-42, A-45 | EID-1 | 0.3002 | 238 | 292 | 334 | 382 | 514 |
| A-42, A-45 | CVP-1 | 0.1859 | 130 | 164 | 190 | 220 | 302 |
| A-42, A-45 | CVP-2 | 0.5040 | 352 | 443 | 514 | 595 | 817 |
| A-42, A-45 | EID-2 | 0.1395 | 89 | 109 | 125 | 143 | 193 |
| A-42, A-45 | CVP-3 | 0.0630 | 45 | 57 | 66 | 77 | 105 |
| A-42, A-45 | RLH-1 | 0.1246 | 59 | 74 | 87 | 101 | 139 |
| A-42, A-45 | RLH_2 | 0.0319 | 17 | 27 | 36 | 47 | 77 |
| A-42, A-45 | ESTWD1 | 0.6150 | 499 | 618 | 710 | 815 | 1106 |
| A-42, A-45 | ESTWD2 | 0.6680 | 1195 | 1471 | 1688 | 1929 | 2604 |
| A-42, A-45 | SLTRHL | 0.4390 | 253 | 320 | 372 | 431 | 594 |
| A-42, A-45 | A-CAR DAM-1 | 0.4161 | 29 | 74 | 124 | 190 | 409 |
| A-42, A-45 | A_CAR DAM-2 | 0.1015 | 105 | 142 | 172 | 206 | 300 |
| A-42, A-45 | A_MesaDrain_UP | 0.0735 | 69 | 96 | 118 | 142 | 212 |
| A-42, A-45 | A-LL-8 | 1.0568 | 151 | 301 | 447 | 626 | 1191 |
| A-42, A-45 | A-LL-8a | 0.7243 | 210 | 342 | 459 | 596 | 1005 |
| A-42, A-45 | A-LL-10 | 0.3416 | 341 | 467 | 571 | 687 | 1014 |
| A-42, A-45 | A-MESA-2 | 0.5021 | 143 | 244 | 335 | 443 | 768 |
| A-42, A-45 | A_MESA_3 | 0.2018 | 200 | 271 | 329 | 394 | 576 |
| A-42, A-45 | A_MESA_4 | 0.1603 | 49 | 82 | 111 | 145 | 248 |
| A-42, A-45 | CVB-A | 0.9757 | 32 | 32 | 32 | 32 | 32 |
| A-42, A-45 | CVB-B | 0.0630 | 22 | 26 | 26 | 26 | 26 |
| A-42, A-45 | ED | 0.6150 | 214 | 306 | 381 | 466 | 692 |
| A-42, A-45 | LAF-B | 0.4161 | 18 | 26 | 26 | 26 | 26 |
| A-42, A-45 | JESUIT BASIN | 1.7811 | 22 | 22 | 22 | 22 | 22 |
| A-42, A-45 | PENDALE BASIN | 0.5021 | 32 | 32 | 32 | 32 | 32 |
| A-42, A-45 | CLB_A_JN | 1.2759 | 270 | 324 | 366 | 414 | 546 |
| A-42, A-45 | CLB_B_JN | 0.1876 | 80 | 100 | 113 | 127 | 165 |
| A-42, A-45 | Node19 | 1.2830 | 1211 | 1488 | 1706 | 1949 | 2654 |
| A-42, A-45 | CARDAM@IH-10 | 0.5176 | 106 | 149 | 188 | 232 | 326 |
| A-42, A-45 | LOMALAND @IH-10 | 2.1227 | 355 | 489 | 593 | 709 | 1036 |
| A-42, A-45 | MESA -JN | 0.7039 | 214 | 299 | 361 | 426 | 608 |
| A-42, A-45 | MV#1 | 0.7542 | 341 | 492 | 618 | 763 | 1178 |
| A-42, A-45 | MV#2 | 0.1608 | 161 | 220 | 269 | 324 | 478 |
| A-42, A-45 | Sunmount Channel | 0.2858 | 151 | 224 | 286 | 357 | 566 |
| A-42, A-45 | VCNT-1 | 0.1859 | 130 | 164 | 190 | 220 | 302 |
| A-42, A-45 | VCNT-2 | 0.5040 | 352 | 443 | 514 | 595 | 817 |
| A-42, A-45 | MV#3 | 1.2759 | 270 | 324 | 366 | 414 | 546 |
| A-42, A-45 | MV#4 | 0.1395 | 89 | 109 | 125 | 143 | 193 |
| A-42, A-45 | VCNT-3 | 0.0630 | 45 | 57 | 66 | 77 | 105 |
| A-42, A-45 | MV#5 | 0.1876 | 80 | 100 | 113 | 127 | 165 |
| A-42, A-45 | MV#6 | 0.0319 | 17 | 27 | 36 | 47 | 77 |

Table A-33. East Side Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| EAST SIDE REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|--------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-42, A-45 | MV#7 | 1.2830 | 1211 | 1488 | 1706 | 1949 | 2654 |
| A-42, A-45 | MV#8 | 0.4390 | 253 | 320 | 372 | 431 | 594 |
| A-42, A-45 | MV#9 | 0.5176 | 106 | 149 | 188 | 232 | 326 |
| A-42, A-45 | MV#10 | 0.0735 | 69 | 96 | 118 | 142 | 212 |
| A-42, A-45 | MV#11 | 2.1227 | 354 | 488 | 591 | 706 | 1032 |
| A-42, A-45 | MV#12 | 0.7039 | 214 | 299 | 361 | 426 | 608 |
| A-42, A-45 | MV#13 | 0.1603 | 49 | 82 | 111 | 145 | 248 |
| A-43, A-45 | 9C | 0.444 | 665 | 816 | 934 | 1066 | 1436 |
| A-43, A-45 | 9A | 0.934 | 1076 | 1321 | 1509 | 1725 | 2323 |
| A-43, A-45 | 9B | 0.262 | 433 | 531 | 608 | 694 | 934 |
| A-43, A-45 | 29 | 0.0270 | 51 | 63 | 72 | 83 | 112 |
| A-43, A-45 | 22 | 0.0440 | 84 | 103 | 119 | 135 | 182 |
| A-43, A-45 | 34 | 0.0480 | 90 | 111 | 128 | 146 | 197 |
| A-43, A-45 | 46 | 0.1180 | 226 | 278 | 319 | 364 | 490 |
| A-43, A-45 | 52 | 0.0450 | 86 | 105 | 121 | 138 | 186 |
| A-43, A-45 | 58 | 0.009 | 17 | 21 | 24 | 28 | 37 |
| A-43, A-45 | 66 | 0.03 | 58 | 71 | 81 | 92 | 125 |
| A-43, A-45 | 77 | 0.087 | 166 | 204 | 235 | 268 | 361 |
| A-43, A-45 | 83 | 0.044 | 80 | 99 | 115 | 131 | 179 |
| A-43, A-45 | 90 | 0.009 | 16 | 20 | 23 | 27 | 36 |
| A-43, A-45 | 96A | 0.05 | 95 | 117 | 134 | 154 | 207 |
| A-43, A-45 | 96B | 0.006 | 11 | 13 | 16 | 18 | 24 |
| A-43, A-45 | 100 | 0.0490 | 88 | 110 | 127 | 145 | 198 |
| A-43, A-45 | 106 | 0.0220 | 42 | 52 | 59 | 68 | 91 |
| A-43, A-45 | 110 | 0.0150 | 29 | 35 | 40 | 46 | 62 |
| A-43, A-45 | 124F | 0.0160 | 31 | 38 | 43 | 49 | 66 |
| A-43, A-45 | 124B | 0.2380 | 377 | 463 | 530 | 606 | 816 |
| A-43, A-45 | 124E | 0.0690 | 8 | 11 | 13 | 15 | 21 |
| A-43, A-45 | 124A | 0.1990 | 367 | 454 | 523 | 599 | 811 |
| A-43, A-45 | 124C | 1.1480 | 621 | 842 | 1005 | 1181 | 1665 |
| A-43, A-45 | 124D | 0.0870 | 76 | 96 | 111 | 128 | 176 |
| A-43, A-45 | 9C_P | 0.444 | 6 | 9 | 112 | 226 | 745 |
| A-43, A-45 | 9B_P | 0.262 | 2 | 3 | 4 | 5 | 7 |
| A-43, A-45 | 9J | 1.64 | 1076 | 1321 | 1509 | 1726 | 2545 |
| A-43, A-45 | WS-22 | 0.282 | 537 | 660 | 758 | 866 | 1168 |
| A-43, A-45 | WS-77 | 0.17 | 321 | 395 | 454 | 519 | 701 |
| A-43, A-45 | 96J | 0.056 | 106 | 130 | 149 | 171 | 230 |
| A-43, A-45 | WS-110 | 0.037 | 71 | 87 | 100 | 114 | 153 |
| A-43, A-45 | 124JW | 0.5060 | 741 | 912 | 1048 | 1203 | 1630 |
| A-43, A-45 | 124JE | 1.2350 | 677 | 914 | 1089 | 1279 | 1801 |
| A-43, A-45 | JB | 1.757 | 966 | 1257 | 1495 | 1754 | 2467 |
| A-43, A-45 | 9CR | 0.444 | 6 | 9 | 112 | 226 | 741 |
| A-43, A-45 | 9BR | 0.262 | 2 | 3 | 4 | 5 | 7 |
| A-43, A-45 | MV#14 | 1.64 | 1075 | 1320 | 1509 | 1725 | 2538 |

Table A-33. East Side Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| EAST SIDE REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|--------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-43, A-45 | MV#15 | 0.282 | 537 | 660 | 758 | 866 | 1168 |
| A-43, A-45 | MV#16 | 0.17 | 321 | 395 | 454 | 519 | 701 |
| A-43, A-45 | MV#17 | 0.009 | 16 | 20 | 23 | 27 | 36 |
| A-43, A-45 | RCP375 | 0.05 | 95 | 117 | 134 | 153 | 206 |
| A-43, A-45 | MV#17a | 0.056 | 105 | 129 | 148 | 169 | 229 |
| A-43, A-45 | MV#18 | 0.049 | 88 | 109 | 126 | 145 | 197 |
| A-43, A-45 | MV#19 | 0.037 | 71 | 87 | 100 | 114 | 153 |
| A-43, A-45 | ARROYO-WEST | 0.199 | 366 | 450 | 517 | 592 | 805 |
| A-43, A-45 | ARROYO-WEST2 | 0.506 | 739 | 908 | 1046 | 1197 | 1618 |
| A-43, A-45 | ARROYO-EAST | 1.148 | 621 | 842 | 1004 | 1180 | 1663 |
| A-43, A-45 | ARROYO-EAST2 | 1.235 | 676 | 913 | 1089 | 1278 | 1801 |
| A-43, A-45 | MV#20 | 1.757 | 966 | 1257 | 1493 | 1753 | 2466 |
| A-43, A-45 | A-PD-2 | 0.148594 | 202 | 259 | 304 | 354 | 493 |
| A-43, A-45 | A-PD-3 | 0.185453 | 82 | 121 | 153 | 190 | 296 |
| A-43, A-45 | A-PD-4 | 0.367969 | 85 | 142 | 192 | 251 | 430 |
| A-43, A-45 | A-PD-5 | 0.545313 | 265 | 378 | 471 | 578 | 882 |
| A-43, A-45 | A-PD-6 | 0.44422 | 201 | 299 | 382 | 477 | 752 |
| A-43, A-45 | A-PD-7 | 0.941047 | 661 | 977 | 1248 | 1557 | 2454 |
| A-43, A-45 | A-PD-8 | 4.475078 | 773 | 1163 | 1501 | 1890 | 3025 |
| A-43, A-45 | A-PD-9 | 6.086 | 623 | 928 | 1201 | 1509 | 2416 |
| A-43, A-45 | A-PD-10 | 1.915484 | 355 | 533 | 687 | 865 | 1384 |
| A-43, A-45 | A-LL-1 | 0.380719 | 270 | 393 | 497 | 617 | 962 |
| A-43, A-45 | A-LL-2 | 0.206188 | 73 | 127 | 176 | 234 | 412 |
| A-43, A-45 | A-LL-3 | 0.347156 | 121 | 206 | 283 | 373 | 644 |
| A-43, A-45 | A-LL-4 | 2.332031 | 971 | 1403 | 1765 | 2179 | 3361 |
| A-43, A-45 | A-LL-5 | 1.092469 | 659 | 949 | 1193 | 1471 | 2267 |
| A-43, A-45 | A-LL-6 | 1.632359 | 948 | 1366 | 1717 | 2119 | 3268 |
| A-43, A-45 | A-LL-7 | 0.455859 | 262 | 384 | 485 | 602 | 938 |
| A-43, A-45 | A-LL-9 | 1.600547 | 447 | 727 | 974 | 1264 | 2131 |
| A-43, A-45 | A-AM-1 | 3.529938 | 1892 | 2806 | 3585 | 4480 | 7069 |
| A-44, A-45 | A-AM-2 | 1.820891 | 801 | 1190 | 1519 | 1898 | 2998 |
| A-44, A-45 | A-AM-3 | 0.69725 | 463 | 676 | 855 | 1060 | 1652 |
| A-44, A-45 | A-AM-4 | 0.161688 | 119 | 177 | 225 | 281 | 441 |
| A-44, A-45 | A-AM-5 | 0.480344 | 218 | 312 | 389 | 478 | 729 |
| A-44, A-45 | A-AM-6 | 0.143594 | 4 | 14 | 26 | 44 | 108 |
| A-44, A-45 | A-AM-7 | 0.105219 | 8 | 22 | 37 | 56 | 122 |
| A-44, A-45 | A-AM-8 | 0.260047 | 65 | 100 | 130 | 165 | 267 |
| A-44, A-45 | A-AM-9 | 0.2859533 | 40 | 79 | 118 | 165 | 314 |
| A-44, A-45 | A-AM-10 | 0.107359 | 55 | 86 | 113 | 144 | 235 |
| A-44, A-45 | A-AM-11 | 1.724141 | 221 | 459 | 694 | 988 | 1916 |
| A-44, A-45 | A-AM-12 | 0.158297 | 69 | 103 | 131 | 164 | 258 |
| A-44, A-45 | A-AMTEN-1 | 1.504406 | 685 | 990 | 1244 | 1536 | 2369 |
| A-44, A-45 | A-AMTEN-2 | 1.535656 | 808 | 1122 | 1380 | 1673 | 2498 |
| A-44, A-45 | A-AMTEN-3 | 1.262859 | 673 | 983 | 1244 | 1545 | 2410 |

Table A-33. East Side Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| EAST SIDE REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|--------------|----------------------------|------------------|------------------|------------------|-------------------|-------------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-44, A-45 | A-AMTEN-4 | 0.772672 | 477 | 679 | 846 | 1038 | 1582 |
| A-44, A-45 | A-AMTEN-5 | 0.921422 | 759 | 1090 | 1372 | 1690 | 2603 |
| A-44, A-45 | A-AMTEN-6 | 3.006453 | 393 | 580 | 743 | 929 | 1470 |
| A-44, A-45 | A-AMTEN-7 | 3.861875 | 662 | 980 | 1255 | 1570 | 2485 |

Table A-34. Mission Valley Region Complete HEC-HMS Results for 10 - 100-Year Storms

| MISSION VALLEY REGION - HEC-HMS RESULTS | | | | | | | |
|---|------------------------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-46, A-47 | A_Americas Basin | 0.498 | 38 | 71 | 101 | 138 | 253 |
| A-46, A-47 | A_Americas Ten Basin | 0.261 | 2 | 7 | 14 | 25 | 73 |
| A-46, A-47 | A_Americas Ten NonContribute | 0.085 | 0 | 0 | 1 | 3 | 12 |
| A-46, A-47 | A_Basin A | 1.421 | 205 | 355 | 486 | 644 | 1119 |
| A-46, A-47 | A_Basin G | 0.356 | 114 | 161 | 199 | 241 | 363 |
| A-46, A-47 | A_Below Basin G to Cty Limi | 1.878 | 266 | 414 | 539 | 682 | 1104 |
| A-46, A-47 | A_Below Carolina Dam | 1.024 | 229 | 387 | 522 | 684 | 1167 |
| A-46, A-47 | A_Below Featherlake Basin | 0.153 | 15 | 31 | 47 | 66 | 127 |
| A-46, A-47 | A_Below Phelps Dodge Basin | 1.386 | 0 | 3 | 17 | 44 | 166 |
| A-46, A-47 | A_Carolina Drive Basin | 0.291 | 0 | 0 | 0 | 0 | 6 |
| A-46, A-47 | A_Feather Lake Basin | 0.704 | 0 | 0 | 1 | 4 | 43 |
| A-46, A-47 | A_Franklin Drain A | 0.668 | 318 | 455 | 565 | 691 | 1046 |
| A-46, A-47 | A_Franklin Drain B | 0.908 | 333 | 519 | 671 | 847 | 1355 |
| A-46, A-47 | A_Franklin Drn to City Limit | 2.884 | 181 | 298 | 402 | 523 | 888 |
| A-46, A-47 | A_Franklin Spur Drain | 0.114 | 44 | 70 | 91 | 115 | 185 |
| A-46, A-47 | A_Lincoln Drain | 2.330 | 481 | 790 | 1052 | 1364 | 2287 |
| A-46, A-47 | A_Lomaland Basin | 0.663 | 22 | 66 | 122 | 204 | 499 |
| A-46, A-47 | A_Mesa Drain A | 0.663 | 0 | 0 | 0 | 0 | 10 |
| A-46, A-47 | A_Mesa Drain B | 0.740 | 26 | 70 | 123 | 196 | 443 |
| A-46, A-47 | A_Mesa Drain C | 3.185 | 27 | 103 | 193 | 320 | 830 |
| A-46, A-47 | A_Mesa Drain to City Limit | 0.803 | 67 | 124 | 175 | 238 | 430 |
| A-46, A-47 | A_Middle Drain A | 4.306 | 200 | 394 | 580 | 807 | 1531 |
| A-46, A-47 | A_Middle Drain B | 0.123 | 91 | 126 | 154 | 185 | 273 |
| A-46, A-47 | A_Middle Drain Spur A | 0.055 | 59 | 85 | 106 | 129 | 195 |
| A-46, A-47 | A_Middle Drain Spur B | 0.074 | 69 | 96 | 118 | 143 | 211 |
| A-46, A-47 | A_Middle to City Limit | 1.013 | 346 | 544 | 707 | 896 | 1445 |
| A-46, A-47 | A_North Loop Detention Basin | 1.129 | 0 | 0 | 1 | 7 | 73 |
| A-46, A-47 | A_Phelps Dodge Basin | 1.081 | 162 | 318 | 458 | 627 | 1144 |
| A-46, A-47 | A_Playa Drain A | 0.571 | 144 | 230 | 302 | 388 | 638 |
| A-46, A-47 | A_Playa Drain B | 5.842 | 263 | 507 | 735 | 1014 | 1902 |
| A-46, A-47 | Basin_A_Sink | 0.000 | 130 | 390 | 390 | 390 | 390 |
| A-46, A-47 | D_Basin A 42inch Culvert | NS | 581 | 954 | 1275 | 1644 | 2785 |
| A-46, A-47 | D_Mesa to Mesa Interceptor | NS | 1301 | 1783 | 2214 | 2728 | 4548 |
| A-46, A-47 | D_Middle and Middle Int | NS | 416 | 663 | 903 | 1243 | 4359 |
| A-46, A-47 | D_Playa and Playa Intercepto | NS | 342 | 882 | 1576 | 2552 | 5040 |
| A-46, A-47 | J_Franklin and Franklin Spur | NS | 853 | 1576 | 2510 | 3733 | 8637 |
| A-46, A-47 | J_Franklin Drain City Limit | NS | 995 | 1867 | 2878 | 4150 | 9344 |
| A-46, A-47 | J_Lincoln Drain Outlet | NS | 481 | 790 | 1052 | 1364 | 2316 |
| A-46, A-47 | J_Mesa Drain w Americas Bsn | NS | 1301 | 1783 | 2214 | 2728 | 4548 |
| A-46, A-47 | J_Mesa Drain w Americas Ten | NS | 112 | 192 | 582 | 1155 | 2448 |
| A-46, A-47 | J_Mesa Drain w Carolina Bsn | NS | 1160 | 1425 | 1632 | 1868 | 2559 |
| A-46, A-47 | J_Mesa Drain w Lafayette Drw | NS | 1282 | 1660 | 1965 | 2318 | 3422 |
| A-46, A-47 | J_Mesa Drain w Lomaland | NS | 1337 | 1787 | 2159 | 2596 | 3955 |
| A-46, A-47 | J_Mesa Drain w Phelps Dodge | NS | 1256 | 1535 | 1753 | 1999 | 2728 |

Table A-34. Mission Valley Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| MISSION VALLEY REGION - HEC-HMS RESULTS | | | | | | | |
|---|------------------------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-46, A-47 | J_Mesa Int w Middle Drain | NS | 416 | 664 | 905 | 1252 | 4439 |
| A-46, A-47 | J_Middle Drain City Limit | 1.013 | 346 | 544 | 707 | 896 | 1445 |
| A-46, A-47 | J_Middle Drain w Middle Int | NS | 416 | 663 | 903 | 1243 | 4359 |
| A-46, A-47 | J_Middle Int w Franklin Canl | NS | 417 | 666 | 906 | 1240 | 4324 |
| A-46, A-47 | J_Middle Int w Franklin Drn | NS | 505 | 732 | 994 | 1311 | 4381 |
| A-46, A-47 | J_Playa Drain Outlet Basin A | NS | 104 | 411 | 905 | 1672 | 3649 |
| A-46, A-47 | J_Playa Drain w Basin A | NS | 641 | 1036 | 1367 | 1747 | 2902 |
| A-46, A-47 | J_Playa Drain with Conduit | NS | 621 | 1018 | 1352 | 1744 | 2924 |
| A-46, A-47 | J_Playa Drain with Intercept | NS | 342 | 882 | 1576 | 2552 | 5040 |
| A-46, A-47 | J_Playa Drn with North Loop | NS | 652 | 1043 | 1377 | 1773 | 2953 |
| A-46, A-47 | R_Franklin Drain A | NS | 500 | 725 | 993 | 1309 | 4359 |
| A-46, A-47 | R_Franklin Drain Spur A | NS | 342 | 857 | 1511 | 2390 | 4838 |
| A-46, A-47 | R_Franklin Drain Spur B | NS | 341 | 843 | 1489 | 2341 | 4738 |
| A-46, A-47 | R_Franklin Drn to City Lmt A | NS | 853 | 1575 | 2503 | 3720 | 8632 |
| A-46, A-47 | R_Franklin Drn to City Lmt B | NS | 844 | 1570 | 2504 | 3711 | 8583 |
| A-46, A-47 | R_Lincoln Drain A | NS | 0 | 0 | 0 | 0 | 30 |
| A-46, A-47 | R_Lincoln Drain B | NS | 0 | 0 | 0 | 0 | 30 |
| A-46, A-47 | R_Lincoln to Playa Conduit | NS | 477 | 788 | 1051 | 1359 | 2296 |
| A-46, A-47 | R_Mesa Drain above Amer BsnA | NS | 1211 | 1599 | 1944 | 2359 | 3585 |
| A-46, A-47 | R_Mesa Drain above Amer BsnB | NS | 1183 | 1585 | 1915 | 2287 | 3577 |
| A-46, A-47 | R_Mesa Drain above Carolina | NS | 1160 | 1425 | 1632 | 1868 | 2559 |
| A-46, A-47 | R_Mesa Drain above Lomaland | NS | 1231 | 1625 | 1939 | 2298 | 3398 |
| A-46, A-47 | R_Mesa Drain below Carolina | NS | 1059 | 1298 | 1489 | 1713 | 2391 |
| A-46, A-47 | R_Mesa Drain to City Limit | 0.000 | 0 | 0 | 0 | 0 | 0 |
| A-46, A-47 | R_Mesa Interceptor above FL | NS | 1287 | 1744 | 2188 | 2725 | 4498 |
| A-46, A-47 | R_Mesa Interceptor blw FL A | NS | 331 | 413 | 478 | 905 | 2981 |
| A-46, A-47 | R_Mesa Interceptor blw FL B | NS | 331 | 413 | 478 | 904 | 2941 |
| A-46, A-47 | R_Middle Drain to City Limit | 0.000 | 0 | 0 | 0 | 0 | 0 |
| A-46, A-47 | R_Middle Drain to Intercept | NS | 416 | 663 | 903 | 1243 | 4359 |
| A-46, A-47 | R_Middle Interceptor A | NS | 416 | 663 | 903 | 1237 | 4319 |
| A-46, A-47 | R_Middle Interceptor B | NS | 417 | 665 | 905 | 1234 | 4248 |
| A-46, A-47 | R_Playa Drain Conduit | NS | 104 | 408 | 884 | 1628 | 3546 |
| A-46, A-47 | R_Playa Drain Lower_A | NS | 104 | 408 | 884 | 1628 | 3546 |
| A-46, A-47 | R_Playa Drain Lower_B | NS | 104 | 406 | 876 | 1591 | 3538 |
| A-46, A-47 | R_Playa Drain Lower_C | NS | 103 | 406 | 850 | 1581 | 3449 |
| A-46, A-47 | R_Playa Drain Upper_A | NS | 612 | 997 | 1329 | 1720 | 2897 |
| A-46, A-47 | R_Playa Drain Upper_B | NS | 641 | 1036 | 1367 | 1747 | 2902 |
| A-46, A-47 | S_Americas Basin | NS | 104 | 115 | 124 | 135 | 159 |
| A-46, A-47 | S_Americas Ten Basin | NS | 61 | 85 | 438 | 920 | 2074 |
| A-46, A-47 | S_Basin A | NS | 77 | 353 | 828 | 1578 | 3532 |
| A-46, A-47 | S_Basin G | 0.356 | 0 | 0 | 0 | 0 | 0 |
| A-46, A-47 | S_Carolina Drive Basin | NS | 65 | 97 | 115 | 132 | 171 |
| A-46, A-47 | S_Featherlake Basin | NS | 331 | 414 | 478 | 907 | 3004 |
| A-46, A-47 | S_Lomaland Basin | NS | 89 | 97 | 104 | 110 | 128 |

Table A-34. Mission Valley Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| MISSION VALLEY REGION - HEC-HMS RESULTS | | | | | | | |
|---|------------------------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-46, A-47 | S_North Loop Detention Basin | NS | 47 | 54 | 55 | 55 | 55 |
| A-46, A-47 | S_Phelps Dodge Basin | NS | 112 | 122 | 130 | 138 | 158 |
| A-46, A-47 | Source_CE Input | NS | 0 | 0 | 0 | 0 | 30 |
| A-46, A-47 | Source_MV# 1,2 | NS | 404 | 577 | 720 | 885 | 1352 |
| A-46, A-47 | Source_MV#11 | NS | 345 | 479 | 581 | 696 | 1016 |
| A-46, A-47 | Source_MV#12,13 | NS | 264 | 376 | 462 | 558 | 833 |
| A-46, A-47 | Source_MV#14,15,16,17a | NS | 1623 | 1998 | 2285 | 2615 | 3534 |
| A-46, A-47 | Source_MV#17a,18,19,20 | NS | 1114 | 1434 | 1698 | 1992 | 2812 |
| A-46, A-47 | Source_MV# 3,4,5 | NS | 410 | 500 | 569 | 646 | 854 |
| A-46, A-47 | Source_MV#6,7 | NS | 1178 | 1454 | 1670 | 1913 | 2620 |
| A-46, A-47 | Source_MV#8,9,10 | NS | 304 | 391 | 466 | 552 | 786 |

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Table A-35. Northeast Region Complete HEC-HMS Results for 10 - 100-Year Storms

| NORTHEAST REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|------------------------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-48, A-49 | A_Amber Basin | 0.248 | 203 | 287 | 353 | 404 | 717 |
| A-48, A-49 | A_Army Ditch | 0.423 | 134 | 217 | 285 | 359 | 625 |
| A-48, A-49 | A_Bossworth D/S | 0.120 | 68 | 95 | 117 | 139 | 217 |
| A-48, A-49 | A_Bossworth U/S | 0.417 | 191 | 274 | 339 | 408 | 639 |
| A-48, A-49 | A_Diana Ditch DS Sunrise Ch | 1.859 | 598 | 902 | 1150 | 1420 | 2295 |
| A-48, A-49 | A_Diana Ditch US Sunrise Ch | 0.960 | 361 | 559 | 722 | 891 | 1508 |
| A-48, A-49 | A_E Fwy Channel | 1.674 | 114 | 205 | 288 | 386 | 694 |
| A-48, A-49 | A_Electric Ditch | 0.626 | 215 | 327 | 419 | 519 | 853 |
| A-48, A-49 | A_Fairbanks Drive | 1.114 | 224 | 345 | 445 | 558 | 901 |
| A-48, A-49 | A_Fort Bliss Div Ch | 0.166 | 146 | 204 | 249 | 282 | 496 |
| A-48, A-49 | A_Fort Bliss Div Ch D/S | 24.625 | 7322 | 10969 | 13930 | 17154 | 27502 |
| A-48, A-49 | A_Fort Bliss Div Ch U/S | 0.154 | 120 | 170 | 210 | 242 | 424 |
| A-48, A-49 | A_Fusselman Dam | 3.371 | 958 | 1445 | 1843 | 2283 | 3667 |
| A-48, A-49 | A_Green Belt Levee D/S | 0.968 | 86 | 154 | 215 | 288 | 516 |
| A-48, A-49 | A_Green Belt Levee U/S | 14.301 | 1349 | 2183 | 2902 | 3735 | 6249 |
| A-48, A-49 | A_Hondo Pass Basin | 0.079 | 66 | 93 | 114 | 130 | 226 |
| A-48, A-49 | A_Hondo Pass Ch | 0.047 | 31 | 46 | 58 | 67 | 121 |
| A-48, A-49 | A_Johnson Channel | 0.075 | 74 | 100 | 120 | 135 | 225 |
| A-48, A-49 | A_Keltner Dam | 0.486 | 276 | 391 | 481 | 572 | 908 |
| A-48, A-49 | A_Mtn Park Dam | 0.806 | 350 | 501 | 621 | 749 | 1169 |
| A-48, A-49 | A_NE. Pond Outer | 3.201 | 1044 | 1612 | 2080 | 2584 | 4287 |
| A-48, A-49 | A_NE Ponding | 3.133 | 286 | 489 | 668 | 878 | 1523 |
| A-48, A-49 | A_Northgate Dam | 1.472 | 275 | 462 | 621 | 805 | 1393 |
| A-48, A-49 | A_Northgate Div Ch | 1.293 | 422 | 615 | 770 | 940 | 1468 |
| A-48, A-49 | A_Northgate Int Ch | 0.599 | 26 | 57 | 87 | 127 | 255 |
| A-48, A-49 | A_Northgate Outlet Channel | 0.472 | 56 | 103 | 145 | 195 | 354 |
| A-48, A-49 | A_Northhills Dam N | 2.446 | 674 | 999 | 1262 | 1555 | 2450 |
| A-48, A-49 | A_Northhills Dam S | 3.087 | 853 | 1249 | 1568 | 1923 | 2995 |
| A-48, A-49 | A_PSB Ch 1 D/S | 0.460 | 20 | 50 | 83 | 127 | 275 |
| A-48, A-49 | A_PSB Ch 1 U/S Fannin | 1.798 | 136 | 249 | 352 | 478 | 867 |
| A-48, A-49 | A_PSB Ch 1 U/S Gateway | 0.239 | 62 | 100 | 131 | 166 | 282 |
| A-48, A-49 | A_PSB Ch 1 U/S PSB2 | 0.701 | 240 | 372 | 481 | 597 | 998 |
| A-48, A-49 | A_PSB Ch 2 D/S | 0.992 | 169 | 293 | 401 | 525 | 929 |
| A-48, A-49 | A_PSB Ch 2 U/S Gateway | 1.371 | 267 | 424 | 555 | 705 | 1167 |
| A-48, A-49 | A_PSB Ch 2 U/S Rushing | 0.803 | 162 | 283 | 389 | 509 | 919 |
| A-48, A-49 | A_Railroad Drain D/S | 0.053 | 1 | 4 | 7 | 12 | 29 |
| A-48, A-49 | A_Railroad Drain U/S Statler | 0.152 | 17 | 30 | 42 | 56 | 100 |
| A-48, A-49 | A_Railroad Drain U/S Tobin | 9.876 | 635 | 1016 | 1350 | 1734 | 2886 |
| A-48, A-49 | A_Range Basin | 0.391 | 136 | 224 | 297 | 373 | 680 |
| A-48, A-49 | A_Range Dam | 2.210 | 428 | 658 | 849 | 1066 | 1720 |
| A-48, A-49 | A_Statler Ditch | 0.448 | 100 | 165 | 221 | 283 | 487 |
| A-48, A-49 | A_Sunrise Basin | 0.135 | 101 | 143 | 176 | 204 | 348 |
| A-48, A-49 | A_Sunrise Channel | 0.318 | 135 | 197 | 247 | 299 | 476 |
| A-48, A-49 | A_Sunrise Dam | 0.499 | 239 | 343 | 425 | 510 | 804 |

Table A-35. Northeast Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| NORTHEAST REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|------------------------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-48, A-49 | A_Tobin Drain at U/S Army | 0.501 | 317 | 460 | 574 | 677 | 1147 |
| A-48, A-49 | A_Tobin Drain U/S Irvin H | 2.190 | 343 | 611 | 846 | 1120 | 2012 |
| A-48, A-49 | A_Tobin Drain U/S RR Drain | 0.503 | 115 | 198 | 269 | 348 | 622 |
| A-48, A-49 | A_TXDOT Pond | 0.614 | 145 | 229 | 300 | 379 | 632 |
| A-48, A-49 | A_W. Fwy Ch D/S | 1.336 | 94 | 169 | 237 | 318 | 572 |
| A-48, A-49 | A_W. Fwy Ch U/S | 1.031 | 65 | 158 | 254 | 378 | 803 |
| A-48, A-49 | A_War Road Channel | 0.524 | 140 | 242 | 329 | 423 | 776 |
| A-48, A-49 | D_Ft Bliss Outflow | 92.239 | 9104 | 14002 | 18049 | 22557 | 36838 |
| A-48, A-49 | D_Ft Bliss Sump | 92.239 | 0 | 0 | 0 | 437 | 10013 |
| A-48, A-49 | D_Hondo Pass | 0.047 | 31 | 46 | 58 | 67 | 121 |
| A-48, A-49 | D_NE Ponding | 32.347 | 0 | 0 | 0 | 0 | 0 |
| A-48, A-49 | D_Range Dam | 11.157 | 0 | 0 | 0 | 0 | 0 |
| A-48, A-49 | J_Army Ditch | 11.972 | 134 | 217 | 285 | 359 | 625 |
| A-48, A-49 | J_Bossworth Ch D/S | 0.538 | 248 | 356 | 440 | 531 | 824 |
| A-48, A-49 | J_Diana Ditch and FB Div | 5.272 | 1255 | 1920 | 2448 | 3009 | 4873 |
| A-48, A-49 | J_Diana Ditch D/S | 3.647 | 1039 | 1609 | 2066 | 2563 | 4173 |
| A-48, A-49 | J_Diana Ditch U/S | 1.788 | 496 | 756 | 969 | 1193 | 1978 |
| A-48, A-49 | J_Electric Ditch | 1.740 | 334 | 515 | 664 | 836 | 1345 |
| A-48, A-49 | J_Ft Bliss Div Ch Dyer St | 1.624 | 222 | 312 | 382 | 447 | 723 |
| A-48, A-49 | J_Ft Bliss Div Ch U/S | 1.459 | 120 | 170 | 220 | 357 | 448 |
| A-48, A-49 | J_Ft Bliss Sump | 92.239 | 9304 | 14202 | 18249 | 22757 | 37038 |
| A-48, A-49 | J_Ft Bliss Sump Upper | 66.515 | 1794 | 2915 | 3902 | 5065 | 8573 |
| A-48, A-49 | J_Green Belt Levee | 25.014 | 1849 | 2990 | 3970 | 5109 | 8544 |
| A-48, A-49 | J_Green Belt Levee D/S | 32.347 | 2292 | 3772 | 5065 | 6576 | 11191 |
| A-48, A-49 | J_Northgate Dam Out | 7.207 | 56 | 103 | 145 | 195 | 354 |
| A-48, A-49 | J_PSB Ch 1 D/S | 6.365 | 766 | 1295 | 1760 | 2317 | 4023 |
| A-48, A-49 | J_PSB Ch1 Jct1 | 0.239 | 62 | 100 | 131 | 166 | 282 |
| A-48, A-49 | J_PSB Ch1 Jct2 | 2.037 | 187 | 327 | 453 | 602 | 1064 |
| A-48, A-49 | J_PSB Ch1 Jct3 | 5.905 | 749 | 1257 | 1700 | 2227 | 3830 |
| A-48, A-49 | J_PSB Ch 2 at Gateway | 1.371 | 267 | 424 | 555 | 705 | 1167 |
| A-48, A-49 | J_PSB Ch 2 at Rushing | 2.175 | 350 | 567 | 752 | 966 | 1622 |
| A-48, A-49 | J_PSB Ch 2 D/S | 3.167 | 460 | 763 | 1026 | 1337 | 2292 |
| A-48, A-49 | J_RR and Tobin Drain | 60.590 | 756 | 1270 | 1718 | 2252 | 3869 |
| A-48, A-49 | J_RR Ditch at Statler Ditch | 61.190 | 846 | 1427 | 1936 | 2542 | 4372 |
| A-48, A-49 | J_RR Ditch Downstream | 61.243 | 840 | 1414 | 1917 | 2516 | 4331 |
| A-48, A-49 | J_RR Drain U/S of Tobin | 45.424 | 635 | 1016 | 1350 | 1734 | 2886 |
| A-48, A-49 | J_RR Dr U/S Statler Ch | 60.742 | 770 | 1295 | 1752 | 2296 | 3945 |
| A-48, A-49 | J_Sunrise Ch D/S | 0.828 | 139 | 203 | 254 | 308 | 487 |
| A-48, A-49 | J_Sunrise Ch U/S | 0.510 | 9 | 11 | 12 | 14 | 19 |
| A-48, A-49 | J_Tobin Drain at Army Ditch | 14.663 | 572 | 970 | 1315 | 1720 | 2960 |
| A-48, A-49 | J_Tobin Drain D/S | 15.166 | 652 | 1117 | 1522 | 2003 | 3452 |
| A-48, A-49 | J_Tobin Drain U/S Army Ditch | 2.691 | 470 | 801 | 1088 | 1422 | 2474 |
| A-48, A-49 | J_War Road Channel | 6.058 | 140 | 243 | 337 | 445 | 844 |
| A-48, A-49 | J_W Fwy Ch @ War Road | 6.672 | 268 | 408 | 526 | 671 | 1091 |

Table A-35. Northeast Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| NORTHEAST REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|------------------------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-48, A-49 | J_W Fwy Ch U/S | 7.703 | 299 | 495 | 672 | 902 | 1624 |
| A-48, A-49 | J_W Fwy D/S | 9.039 | 388 | 658 | 894 | 1175 | 2026 |
| A-48, A-49 | R_Army Ditch | 0.000 | 0 | 0 | 0 | 14 | 159 |
| A-48, A-49 | R_Bossworth U/S | 0.417 | 191 | 274 | 339 | 408 | 638 |
| A-48, A-49 | R_Diana Ditch | 1.788 | 457 | 715 | 920 | 1145 | 1878 |
| A-48, A-49 | R_Electric Ditch | 1.114 | 223 | 344 | 443 | 556 | 897 |
| A-48, A-49 | R_Ft Bliss Div Ch D/S | 1.624 | 222 | 312 | 382 | 447 | 723 |
| A-48, A-49 | R_Ft Bliss Div Ch U/S | 1.459 | 120 | 170 | 220 | 357 | 448 |
| A-48, A-49 | R_Fusselman Out | 3.371 | 52 | 59 | 63 | 66 | 74 |
| A-48, A-49 | R_Green Belt Levee | 25.014 | 1843 | 2983 | 3961 | 5099 | 8529 |
| A-48, A-49 | R_Hondo Pass Channel | 0.047 | 31 | 46 | 58 | 67 | 121 |
| A-48, A-49 | R_Hondo Pass Diversion | 0.000 | 0 | 0 | 0 | 0 | 0 |
| A-48, A-49 | R_Keltner Dam Out | 0.486 | 86 | 91 | 94 | 97 | 372 |
| A-48, A-49 | R_NE Pond Overflow | 35.548 | 0 | 0 | 0 | 0 | 0 |
| A-48, A-49 | R_Northgate Dam Out | 6.735 | 4 | 31 | 45 | 81 | 161 |
| A-48, A-49 | R_PSB Ch1 a | 0.239 | 62 | 99 | 131 | 166 | 280 |
| A-48, A-49 | R_PSB Ch 1 b | 2.037 | 186 | 327 | 452 | 602 | 1063 |
| A-48, A-49 | R_PSB Ch 1 c | 5.905 | 749 | 1256 | 1699 | 2226 | 3829 |
| A-48, A-49 | R_PSB Ch 2 a | 1.371 | 263 | 417 | 546 | 695 | 1144 |
| A-48, A-49 | R_PSB Ch 2 b | 2.175 | 350 | 567 | 752 | 966 | 1622 |
| A-48, A-49 | R_Range Dam Overflow | 11.157 | 0 | 0 | 0 | 0 | 0 |
| A-48, A-49 | R_RR Dr D/S | 61.190 | 838 | 1410 | 1911 | 2507 | 4310 |
| A-48, A-49 | R_RR Dr U/S Statler Ch | 60.590 | 754 | 1265 | 1711 | 2242 | 3852 |
| A-48, A-49 | R_Sunrise Channel | 0.510 | 9 | 11 | 12 | 14 | 19 |
| A-48, A-49 | R_Tobin Drain U/S Army Ditch | 2.190 | 333 | 590 | 818 | 1085 | 1933 |
| A-48, A-49 | R_Tobin Drain U/S RR Drain | 14.663 | 565 | 962 | 1305 | 1708 | 2941 |
| A-48, A-49 | R_W Fwy Ch D/S | 7.703 | 296 | 490 | 668 | 891 | 1585 |
| A-48, A-49 | R_W Fwy Ch U/S | 6.672 | 258 | 397 | 515 | 657 | 1066 |
| A-48, A-49 | S_Amber Basin | 0.248 | 5 | 6 | 7 | 8 | 9 |
| A-48, A-49 | S_Ft Bliss Outer Sump | 92.239 | 0 | 0 | 0 | 0 | 0 |
| A-48, A-49 | S_Ft Bliss Sump | 0.000 | 9104 | 14002 | 18049 | 22557 | 36838 |
| A-48, A-49 | S_Fusselman Dam | 3.371 | 52 | 59 | 63 | 66 | 74 |
| A-48, A-49 | S_Hondo Pass Basin | 0.127 | 1 | 2 | 2 | 3 | 4 |
| A-48, A-49 | S_Keltner Dam | 0.486 | 86 | 91 | 94 | 97 | 372 |
| A-48, A-49 | S_Mtn Park Dam | 0.806 | 5 | 25 | 49 | 168 | 177 |
| A-48, A-49 | S_NE Ponding | 3.133 | 2519 | 4189 | 5657 | 7376 | 12639 |
| A-48, A-49 | S_NE Pond Outer | 35.548 | 0 | 0 | 0 | 0 | 0 |
| A-48, A-49 | S_Northgate Dam | 6.735 | 5 | 32 | 45 | 81 | 161 |
| A-48, A-49 | S_Northhills Dam N | 2.446 | 19 | 53 | 61 | 69 | 88 |
| A-48, A-49 | S_Northhills Dam S | 5.533 | 70 | 72 | 73 | 74 | 76 |
| A-48, A-49 | S_Pershing Dam | 0.000 | 200 | 200 | 200 | 200 | 200 |
| A-48, A-49 | S_Range Basin | 11.549 | 0 | 0 | 1 | 1 | 3 |
| A-48, A-49 | S_Range Dam | 11.157 | 0 | 0 | 0 | 15 | 159 |
| A-48, A-49 | S_Sunrise Basin | 0.135 | 3 | 3 | 4 | 4 | 6 |

Table A-35. Northeast Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| NORTHEAST REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|--------------------|----------------------------|------------------|------------------|------------------|-------------------|-------------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-48, A-49 | S_Sunrise Dam | 0.499 | 32 | 130 | 168 | 173 | 185 |
| A-48, A-49 | Sink - Gov Hill Ch | 92.239 | 0 | 0 | 0 | 0 | 0 |
| A-48, A-49 | TXDOT Pond | 0.614 | 130 | 205 | 268 | 340 | 558 |

Table A-36. Northwest Region Complete HEC-HMS Results for 10 - 100-Year Storms

| NORTHWEST REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|----------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-50 | A1 | 0.16 | 0 | 0 | 0 | 0 | 5 |
| A-53, A-54 | A1A | 1.04 | 503 | 763 | 1005 | 1291 | 2145 |
| A-53, A-54 | A1A,HR3 | 1.33 | 672 | 1017 | 1340 | 1719 | 2853 |
| A-53, A-54 | A4_1 | 0.97 | 370 | 613 | 850 | 1141 | 2052 |
| A-53, A-54 | A5_1 | 0.79 | 639 | 935 | 1205 | 1519 | 2438 |
| A-53, A-54 | BC_1 | 0.38 | 318 | 472 | 613 | 777 | 1262 |
| A-53, A-54 | BC_1,C1 | 1.58 | 1004 | 1552 | 2070 | 2687 | 4561 |
| A-53, A-54 | BC_2 | 0.86 | 342 | 575 | 805 | 1087 | 1978 |
| A-53, A-54 | BC_C1 | 1.20 | 686 | 1081 | 1458 | 1910 | 3299 |
| A-53, A-54 | BDC_1 | 0.99 | 530 | 828 | 1111 | 1449 | 2475 |
| A-53, A-54 | BeforeKD1 | 13.66 | 2559 | 3837 | 5036 | 6544 | 10855 |
| A-53, A-54 | Before MesaDam | 2.57 | 1534 | 2380 | 3181 | 4136 | 7036 |
| A-52 | BHP | 0.45 | 0 | 0 | 0 | 0 | 18 |
| A-52 | BHP_Outlet | 0.45 | 0 | 0 | 0 | 0 | 18 |
| A-53, A-54 | BLC_1 | 0.21 | 335 | 458 | 566 | 689 | 1039 |
| A-53, A-54 | BLC_2 | 0.23 | 184 | 287 | 384 | 500 | 847 |
| A-53, A-54 | BLC_2,C2 | 7.78 | 332 | 465 | 663 | 956 | 1765 |
| A-53, A-54 | BLC_3 | 0.30 | 99 | 186 | 277 | 391 | 771 |
| A-53, A-54 | BLC_3,C3 | 4.52 | 192 | 203 | 305 | 482 | 953 |
| A-53, A-54 | BLC_C1 | 10.70 | 463 | 543 | 694 | 1012 | 1868 |
| A-53, A-54 | BLC_C2 | 7.56 | 325 | 342 | 358 | 521 | 918 |
| A-53, A-54 | BLC_C3 | 4.22 | 187 | 194 | 199 | 205 | 239 |
| A-53, A-54 | BLC2,BLC1 | 10.91 | 605 | 923 | 1235 | 1701 | 2906 |
| A-53, A-54 | BLC2,MDO1 | 10.70 | 464 | 544 | 770 | 1162 | 2086 |
| A-53, A-54 | BLC3,TDO1 | 7.56 | 325 | 342 | 359 | 595 | 1146 |
| A-55 | BVC_1 | 0.02 | 13 | 19 | 25 | 31 | 50 |
| A-55 | BVC_1,C1 | 3.46 | 2145 | 3276 | 4308 | 5555 | 9146 |
| A-55 | BVC_2 | 0.71 | 561 | 821 | 1058 | 1334 | 2141 |
| A-55 | BVC_2,C2 | 2.56 | 1713 | 2588 | 3374 | 4328 | 7035 |
| A-55 | BVC_C1 | 3.45 | 2132 | 3257 | 4284 | 5524 | 9096 |
| A-55 | BVC_C2 | 1.85 | 1152 | 1767 | 2316 | 2994 | 4893 |
| A-55 | BVC1,MHC2 | 4.53 | 3190 | 4785 | 6236 | 7966 | 12963 |
| A-55 | BVC2,TBV1 | 3.45 | 2224 | 3376 | 4424 | 5687 | 9327 |
| A-55 | CC | 1.85 | 1242 | 1883 | 2451 | 3153 | 5126 |
| A-55 | CC_1 | 0.16 | 194 | 269 | 336 | 412 | 631 |
| A-55 | CC_C | 1.70 | 1048 | 1614 | 2115 | 2741 | 4495 |
| A-50 | DD_1 | 1.53 | 341 | 542 | 735 | 968 | 1684 |
| A-50 | DD_3 | 0.16 | 169 | 249 | 323 | 408 | 659 |
| A-50 | DD_Out | 1.53 | 341 | 542 | 735 | 968 | 1684 |
| A-50 | DD3,WSD2 | 0.36 | 454 | 650 | 826 | 1029 | 1616 |
| A-52 | EC_1 | 0.13 | 10 | 30 | 54 | 87 | 209 |
| A-52 | EC1US | 8.00 | 1334 | 2005 | 2628 | 3360 | 5552 |
| A-53, A-54 | ER1,ODA1 | 2.51 | 1329 | 2016 | 2657 | 3412 | 5662 |
| A-52 | FPN38_1 | 0.50 | 347 | 528 | 697 | 896 | 1490 |

Table A-36. Northwest Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| NORTHWEST REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|-------------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-52 | FPN38_1US | 4.65 | 348 | 528 | 697 | 896 | 1918 |
| A-52 | FPN38_3 | 0.27 | 316 | 461 | 592 | 743 | 1185 |
| A-52 | FPN38_4 | 1.49 | 0 | 0 | 0 | 0 | 51 |
| A-52 | FPN38_4US | 1.49 | 0 | 0 | 0 | 0 | 51 |
| A-52 | FPN38A | 1.72 | 544 | 823 | 1084 | 1392 | 2317 |
| A-52 | FPN38A,B,_3 | 4.15 | 864 | 1291 | 1687 | 2152 | 3582 |
| A-52 | FPN38B | 0.67 | 315 | 466 | 605 | 768 | 1250 |
| A-52 | FPN39A_1 | 0.06 | 95 | 132 | 164 | 201 | 306 |
| A-52 | FPN39A1US | 2.50 | 994 | 1495 | 1961 | 2509 | 4143 |
| A-52 | FPN39A2 | 0.69 | 281 | 420 | 548 | 698 | 1145 |
| A-52 | FPN39A2a | 0.69 | 281 | 420 | 548 | 698 | 1145 |
| A-52 | FPN39A2aUS | 2.44 | 988 | 1487 | 1951 | 2498 | 4126 |
| A-52 | FPN39A2US | 2.44 | 988 | 1487 | 1951 | 2498 | 4126 |
| A-52 | FPN40_1 | 0.14 | 162 | 220 | 271 | 329 | 494 |
| A-52 | FPN40_2 | 0.21 | 128 | 193 | 253 | 324 | 534 |
| A-52 | FPN40_2 US | 2.65 | 1061 | 1595 | 2092 | 2675 | 4413 |
| A-52 | FPN40_2US,FPN40_3 | 5.27 | 1718 | 2591 | 3403 | 4362 | 7230 |
| A-51 | FPN40_3 | 2.63 | 743 | 1122 | 1475 | 1891 | 3140 |
| A-52 | FPN41_1 | 0.13 | 76 | 113 | 148 | 188 | 309 |
| A-52 | FPN41_1 US | 3.83 | 1158 | 1745 | 2291 | 2934 | 4884 |
| A-52 | FPN41_2 | 1.83 | 572 | 865 | 1140 | 1464 | 2437 |
| A-52 | FPN41A | 1.87 | 564 | 851 | 1119 | 1434 | 2379 |
| A-52 | FPN41A, FP41_2 | 3.70 | 1125 | 1696 | 2227 | 2854 | 4727 |
| A-51 | FPN42 | 1.20 | 369 | 556 | 730 | 937 | 1561 |
| A-51 | FPN42A | 0.11 | 76 | 116 | 153 | 197 | 327 |
| A-51 | FPN42T1_1 | 0.11 | 107 | 162 | 213 | 273 | 449 |
| A-51 | FPN42T1_1OUT | 0.79 | 329 | 501 | 661 | 851 | 1421 |
| A-51 | FPN42T1_2 | 0.44 | 179 | 272 | 359 | 462 | 769 |
| A-51 | FPN43 | 1.12 | 427 | 646 | 850 | 1090 | 1808 |
| A-53, A-54 | GC_1 | 0.34 | 389 | 567 | 728 | 915 | 1459 |
| A-53, A-54 | GC1,BC2 | 1.20 | 731 | 1142 | 1534 | 2002 | 3437 |
| A-53, A-54 | HDC_1 | 0.99 | 946 | 1366 | 1746 | 2184 | 3460 |
| A-53, A-54 | HR_1 | 0.54 | 516 | 782 | 1030 | 1319 | 2178 |
| A-53, A-54 | HR_2 | 0.39 | 395 | 584 | 758 | 960 | 1551 |
| A-53, A-54 | HR_2,C2 | 1.72 | 844 | 1286 | 1699 | 2187 | 3651 |
| A-53, A-54 | HR_3 | 0.29 | 168 | 254 | 334 | 429 | 708 |
| A-53, A-54 | HR_C1 | 3.01 | 1254 | 1895 | 2491 | 3194 | 5294 |
| A-53, A-55 | HR_C2 | 1.33 | 643 | 980 | 1295 | 1667 | 2781 |
| A-53, A-54 | HR1,LDE1 | 3.56 | 1506 | 2308 | 3060 | 3950 | 6626 |
| A-53, A-54 | KD_C | 13.81 | 251 | 387 | 473 | 534 | 1163 |
| A-53, A-54 | KD_Out | 13.81 | 251 | 387 | 473 | 534 | 1163 |
| A-53, A-54 | KD1 | 0.14 | 37 | 61 | 85 | 114 | 205 |
| A-53, A-54 | KD1 Dam | 13.81 | 251 | 387 | 473 | 534 | 1173 |
| A-50 | M1(A1_2) | 0.16 | 0 | 0 | 0 | 0 | 7 |

Table A-36. Northwest Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| NORTHWEST REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|---------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-50 | M1 DS | 3.49 | 301 | 530 | 761 | 1049 | 1977 |
| A-53, A-54 | MBDO_1 | 0.25 | 0 | 0 | 2 | 11 | 92 |
| A-53, A-54 | MBDO_C1 | 3.97 | 187 | 194 | 199 | 204 | 216 |
| A-50 | MD_1 | 1.36 | 247 | 376 | 497 | 640 | 1073 |
| A-50 | MD_2 | 1.43 | 150 | 337 | 544 | 817 | 1772 |
| A-50 | MD_2,C2 | 4.92 | 304 | 551 | 791 | 1090 | 1957 |
| A-50 | MD_3 | 3.33 | 301 | 530 | 761 | 1049 | 1977 |
| A-50 | MD_C | 6.66 | 161 | 298 | 442 | 618 | 1280 |
| A-50 | MD_Out | 8.01 | 339 | 536 | 720 | 959 | 1810 |
| A-53, A-54 | MD1 | 0.41 | 411 | 600 | 772 | 972 | 1556 |
| A-53, A-54 | MD1,MBDO_1 | 4.22 | 187 | 194 | 199 | 205 | 239 |
| A-53, A-54 | MD1 Dam | 3.97 | 187 | 194 | 199 | 204 | 216 |
| A-50 | MD2 | 3.49 | 288 | 514 | 738 | 1018 | 1774 |
| A-50 | MD2,WSD1 | 6.66 | 683 | 1137 | 1595 | 2155 | 4055 |
| A-53, A-54 | MDO_1 | 0.04 | 33 | 50 | 66 | 85 | 142 |
| A-53, A-54 | MDO_1,C | 2.92 | 132 | 190 | 194 | 207 | 321 |
| A-53, A-54 | MDO_C | 2.88 | 131 | 188 | 192 | 196 | 207 |
| A-53, A-54 | MeD1 | 0.31 | 270 | 416 | 553 | 714 | 1197 |
| A-53, A-54 | Mesa Dam | 2.88 | 132 | 188 | 192 | 196 | 207 |
| A-55 | MHC_2 | 1.07 | 1045 | 1508 | 1927 | 2411 | 3818 |
| A-50 | NeD1 | 1.29 | 187 | 328 | 468 | 643 | 1205 |
| A-55 | OD | 0.24 | 284 | 414 | 532 | 667 | 1063 |
| A-55 | OD_C | 4.78 | 147 | 157 | 165 | 173 | 192 |
| A-53, A-54 | ODA_1 | 1.29 | 837 | 1273 | 1680 | 2161 | 3598 |
| A-53, A-54 | ODA_2 | 0.52 | 308 | 465 | 612 | 785 | 1299 |
| A-53, A-54 | ODA_C1 | 1.22 | 642 | 982 | 1300 | 1676 | 2803 |
| A-55 | OD Dam | 4.78 | 147 | 157 | 165 | 173 | 192 |
| A-55 | OO_1 | 0.19 | 90 | 140 | 188 | 244 | 415 |
| A-55 | Ox_Out | 4.96 | 225 | 282 | 335 | 398 | 583 |
| A-52 | Pond 4 | 4.15 | 1 | 12 | 27 | 46 | 1854 |
| A-52 | RC_1 | 1.47 | 491 | 735 | 960 | 1226 | 2017 |
| A-52 | RC_2 | 1.75 | 707 | 1067 | 1403 | 1799 | 2981 |
| A-52 | RC_2a | 1.75 | 707 | 1067 | 1403 | 1799 | 2981 |
| A-52 | RC_2c | 1.75 | 707 | 1067 | 1403 | 1799 | 2981 |
| A-52 | RC1US,FPN38_1 | 7.88 | 1332 | 2000 | 2621 | 3351 | 5534 |
| A-52 | RC2aUS | 1.75 | 707 | 1067 | 1403 | 1799 | 2981 |
| A-52 | RC2cUS | 3.23 | 1198 | 1802 | 2364 | 3025 | 4998 |
| A-52 | RC2US | 1.75 | 707 | 1067 | 1403 | 1799 | 2981 |
| A-53, A-54 | RV_1 | 1.30 | 517 | 772 | 1008 | 1285 | 2108 |
| A-53, A-54 | RV1,HR2 | 3.02 | 1282 | 1929 | 2531 | 3240 | 5356 |
| A-55 | SCC_1 | 0.32 | 325 | 487 | 636 | 809 | 1321 |
| A-55 | SCC1,SSC1 | 1.70 | 1167 | 1769 | 2297 | 2957 | 4830 |
| A-55 | SSC_1 | 0.64 | 348 | 521 | 681 | 868 | 1424 |
| A-55 | SSC_2 | 0.74 | 619 | 941 | 1241 | 1594 | 2642 |

Table A-36. Northwest Region Complete HEC-HMS Results for 10 - 100-Year Storms (Continued)

| NORTHWEST REGION - HEC-HMS RESULTS | | | | | | | |
|------------------------------------|----------------|-------------------------|---------------|---------------|---------------|----------------|----------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-55 | SSC_C1 | 0.74 | 574 | 880 | 1133 | 1470 | 2386 |
| A-55 | SSC_C1,SSC_1 | 1.38 | 842 | 1283 | 1661 | 2148 | 3509 |
| A-55 | TBV_1 | 0.89 | 511 | 788 | 1049 | 1359 | 2293 |
| A-53, A-54 | TDO_1 | 0.07 | 6 | 16 | 29 | 47 | 112 |
| A-53, A-54 | TDO_1,C | 3.04 | 134 | 142 | 149 | 155 | 193 |
| A-53, A-54 | TDO_C | 2.97 | 134 | 141 | 148 | 154 | 170 |
| A-53, A-54 | ThoD1 | 0.46 | 433 | 657 | 865 | 1109 | 1833 |
| A-53, A-54 | Thorn Dam | 2.97 | 134 | 141 | 148 | 154 | 170 |
| A-51 | UN01 | 0.24 | 131 | 198 | 261 | 335 | 556 |
| A-51 | UN01,FPN42T1_2 | 0.68 | 310 | 471 | 620 | 797 | 1325 |
| A-51 | UN02_1 | 0.05 | 36 | 55 | 73 | 94 | 156 |
| A-51 | UN01_1OUT | 0.24 | 153 | 233 | 307 | 395 | 658 |
| A-51 | UN02_2 | 0.03 | 30 | 46 | 61 | 78 | 129 |
| A-51 | UN024_1 | 0.07 | 52 | 79 | 104 | 133 | 222 |
| A-51 | UN03 | 0.16 | 93 | 141 | 186 | 238 | 394 |
| A-51 | UN03,02,_2 | 0.19 | 117 | 177 | 234 | 302 | 503 |
| A-52 | UN23_1 | 0.81 | 150 | 258 | 365 | 498 | 924 |
| A-52 | UN23_1US | 10.23 | 3148 | 4770 | 6287 | 8082 | 13481 |
| A-52 | UN23_2 | 0.05 | 44 | 66 | 86 | 110 | 180 |
| A-52 | UN23_2US | 9.43 | 2999 | 4513 | 5922 | 7584 | 12558 |
| A-52 | UN23_3 | 0.13 | 88 | 130 | 169 | 213 | 345 |
| A-52 | UN23_3,FPN40_1 | 9.38 | 2993 | 4503 | 5910 | 7570 | 12536 |
| A-51 | UN23A | 0.03 | 28 | 42 | 56 | 71 | 118 |
| A-51 | UN24A1 | 0.10 | 78 | 119 | 157 | 202 | 334 |
| A-51 | UN24A1OUT | 0.19 | 149 | 227 | 299 | 385 | 638 |
| A-51 | UN24A2 | 0.07 | 44 | 67 | 88 | 113 | 189 |
| A-51 | UN24A2,T1 | 0.10 | 71 | 108 | 143 | 183 | 304 |
| A-51 | UN24AT1 | 0.03 | 27 | 41 | 54 | 70 | 115 |
| A-51 | UN24B | 0.19 | 114 | 172 | 226 | 290 | 480 |
| A-51 | UN24C | 0.06 | 55 | 83 | 109 | 138 | 226 |
| A-51 | UN24D | 0.02 | 23 | 33 | 43 | 54 | 88 |
| A-53, A-54 | VS_1 | 0.70 | 382 | 578 | 761 | 977 | 1619 |
| A-53, A-54 | VS1,ODA2 | 1.22 | 690 | 1044 | 1374 | 1762 | 2918 |
| A-50 | WM | 1.46 | 325 | 530 | 730 | 973 | 1730 |
| A-50 | WRG | 14.56 | 656 | 1423 | 2262 | 3366 | 7182 |
| A-50 | WSD_1 | 0.08 | 51 | 84 | 116 | 155 | 278 |
| A-50 | WSD_1_1 | 0.36 | 394 | 555 | 691 | 832 | 1282 |
| A-50 | WSD_1,WSD1_1 | 0.45 | 420 | 597 | 749 | 907 | 1559 |
| A-50 | WSD_2 | 0.21 | 286 | 401 | 503 | 620 | 958 |

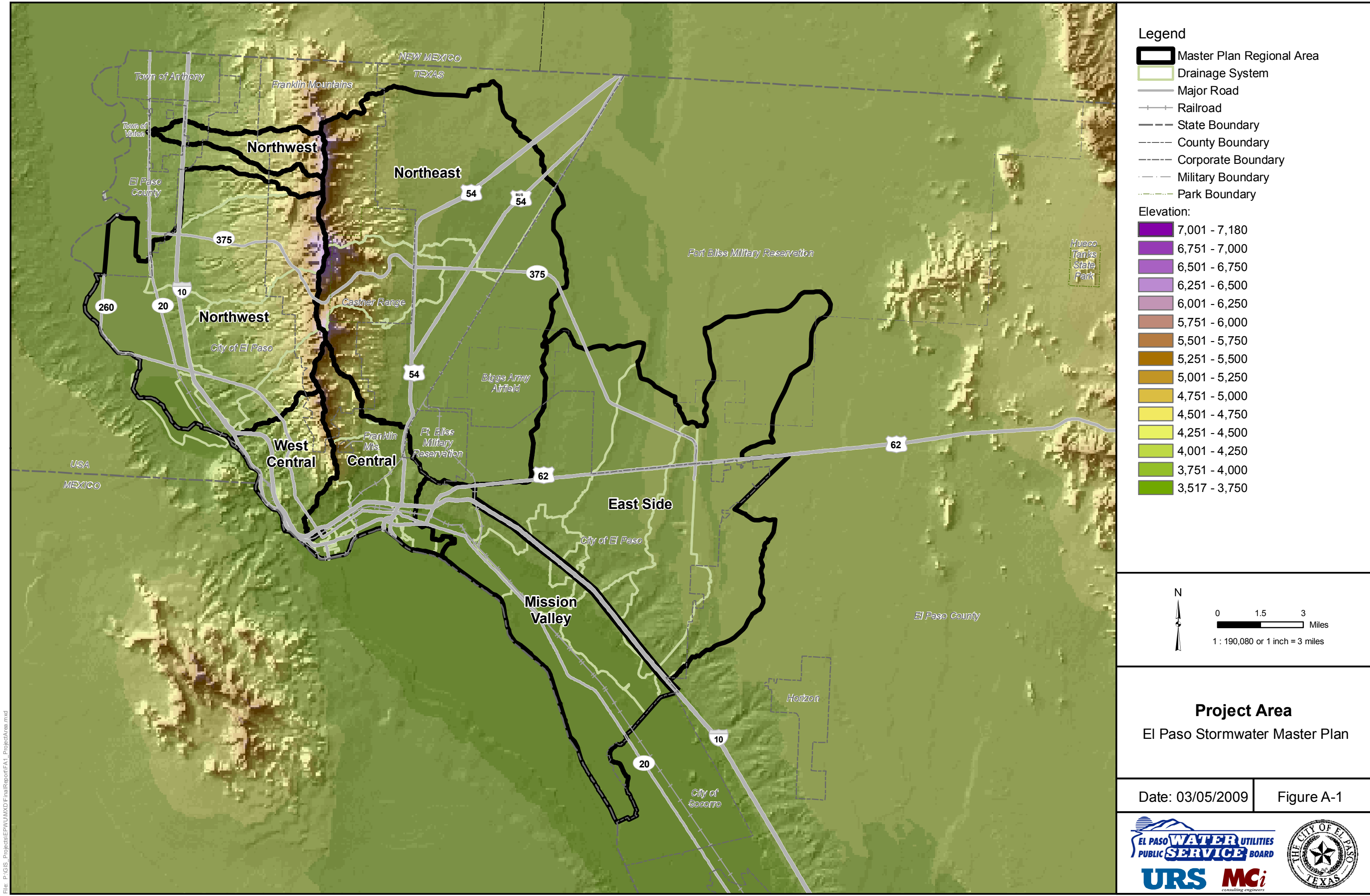
Table A-37. West Central Region Complete HEC-HMS Results for 10 - 100-Year Storms

| WEST CENTRAL REGION - HEC-HMS RESULTS | | | | | | | |
|---------------------------------------|--------------|----------------------------|------------------|------------------|------------------|-------------------|-------------------|
| Schematic Figure Numbers | Element Name | Area (mi ²) | 10-Year (cfs) | 25-Year (cfs) | 50-Year (cfs) | 100-Year (cfs) | 500-Year (cfs) |
| A-56 | Bcanal | 0.80 | 501 | 695 | 868 | 1066 | 1635 |
| A-56 | BCanalUS | 0.80 | 501 | 695 | 868 | 1066 | 1635 |
| A-56 | CBC_1 | 0.89 | 429 | 624 | 802 | 1009 | 1614 |
| A-56 | CBC1,FPN21 | 2.30 | 1071 | 1666 | 2232 | 2908 | 4960 |
| A-56 | FPN20_1 | 0.21 | 175 | 249 | 317 | 394 | 619 |
| A-56 | FPN20_1US | 3.08 | 2702 | 3925 | 5035 | 6318 | 10065 |
| A-56 | FPN20_2 | 1.32 | 1244 | 1819 | 2343 | 2949 | 4723 |
| A-56 | FPN21_1 | 0.24 | 339 | 475 | 596 | 735 | 1133 |
| A-56 | FPN21_2 | 1.41 | 817 | 1292 | 1747 | 2293 | 3957 |
| A-56 | FPN21_C1 | 2.30 | 1025 | 1563 | 2065 | 2700 | 4675 |
| A-56 | FPN21_OUT | 2.54 | 1294 | 1991 | 2650 | 3434 | 5808 |
| A-56 | FPN23_1 | 1.85 | 1429 | 2068 | 2648 | 3319 | 5276 |
| A-56 | FPN23_US | 1.85 | 1429 | 2068 | 2648 | 3319 | 5276 |
| A-56 | Ind_1 | 1.38 | 813 | 1201 | 1558 | 1974 | 3199 |
| A-56 | PC_1 | 1.55 | 1284 | 1857 | 2375 | 2975 | 4723 |
| A-56 | PC1,FPN20_2 | 2.87 | 2528 | 3676 | 4718 | 5924 | 9446 |

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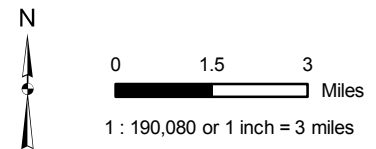
FIGURES

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- Legend**
- Master Plan Regional Area
 - Drainage System
 - Major Road
 - Railroad
 - State Boundary
 - County Boundary
 - Corporate Boundary
 - Military Boundary
 - Park Boundary

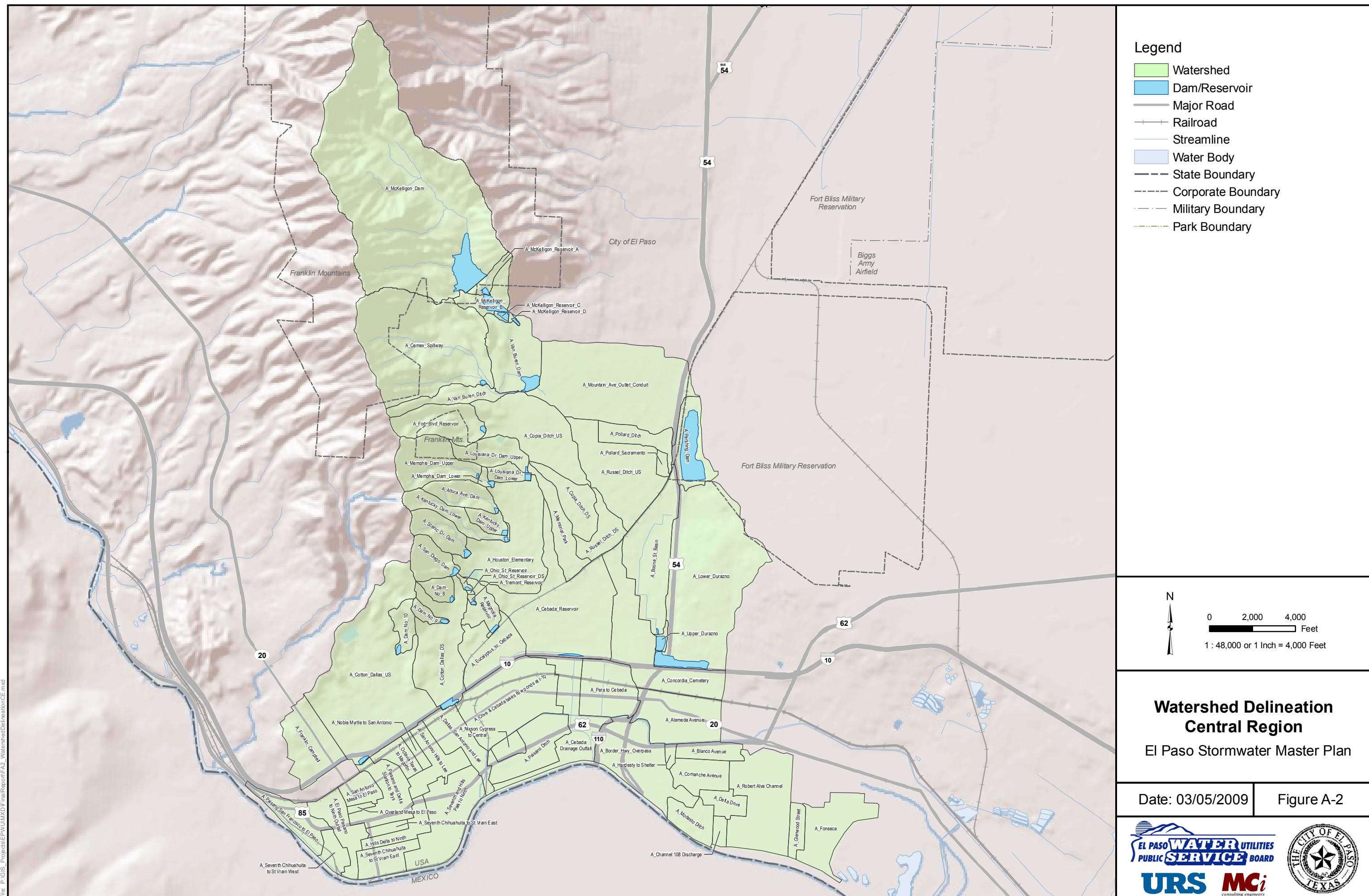
- Elevation:**
- 7,001 - 7,180
 - 6,751 - 7,000
 - 6,501 - 6,750
 - 6,251 - 6,500
 - 6,001 - 6,250
 - 5,751 - 6,000
 - 5,501 - 5,750
 - 5,251 - 5,500
 - 5,001 - 5,250
 - 4,751 - 5,000
 - 4,501 - 4,750
 - 4,251 - 4,500
 - 4,001 - 4,250
 - 3,751 - 4,000
 - 3,517 - 3,750

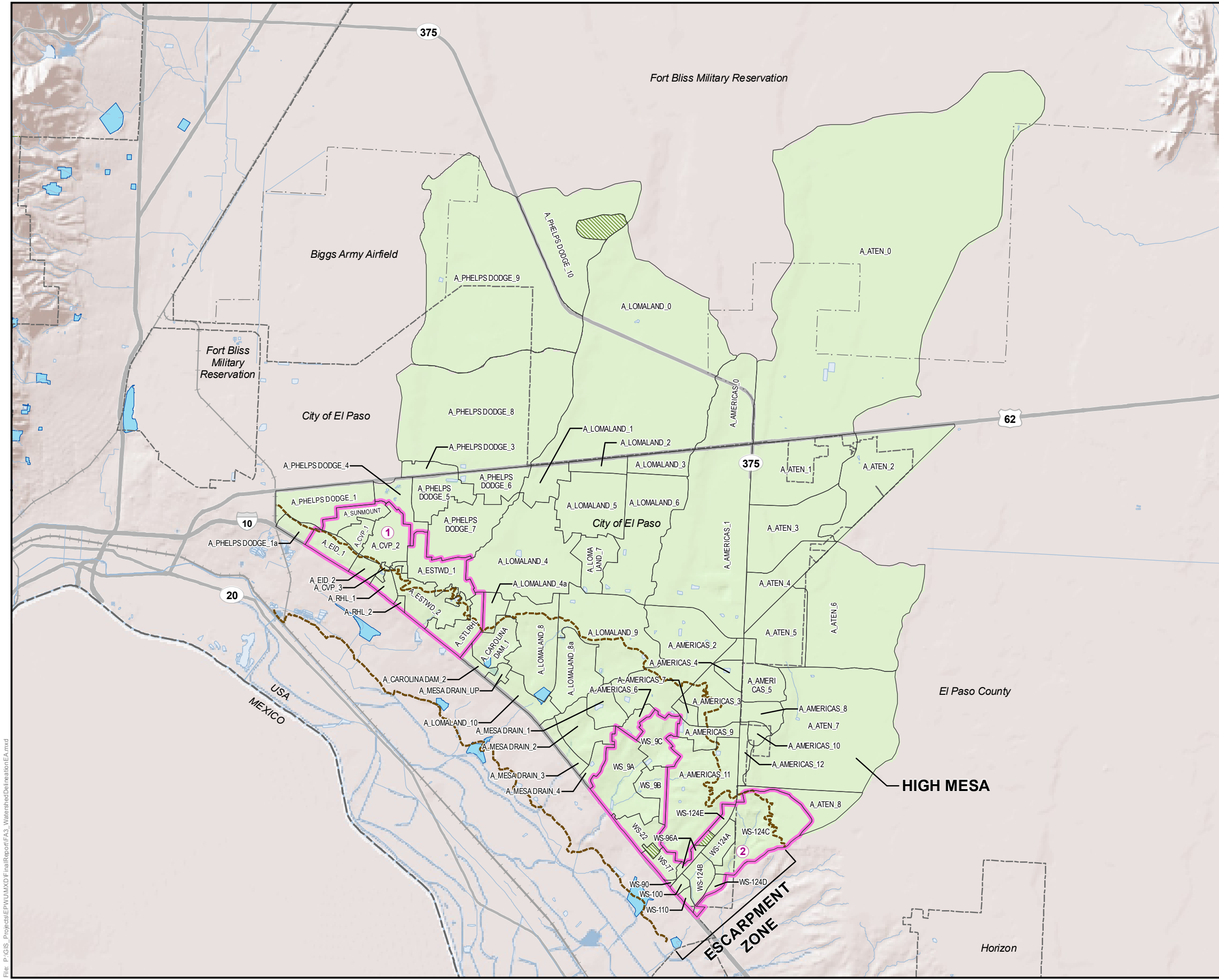


Project Area
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-1







Legend

Watershed

Non-Contributing Watershed

Watershed: Watershed parameters will be referenced from previous TxDOT drainage studies below.

①

Drainage Study and Report for (North Loop Road) Moreno Cardenas Inc. May 2007

②

Drainage Study and Report (Existing Conditions) for Interstate Highway 10, Moreno Cardenas Inc. Feb. 2008

Note: Rainfall Data from El Paso Drainage Design Manual June 2008. Applied for this Master Plan.

Dam/Reservoir

Major Road

Railroad

Streamline

Water Body

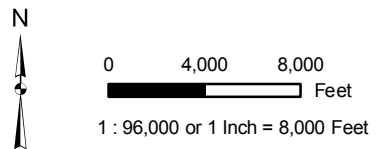
Escarpment Zone

State Boundary

Corporate Boundary

Military Boundary

Park Boundary



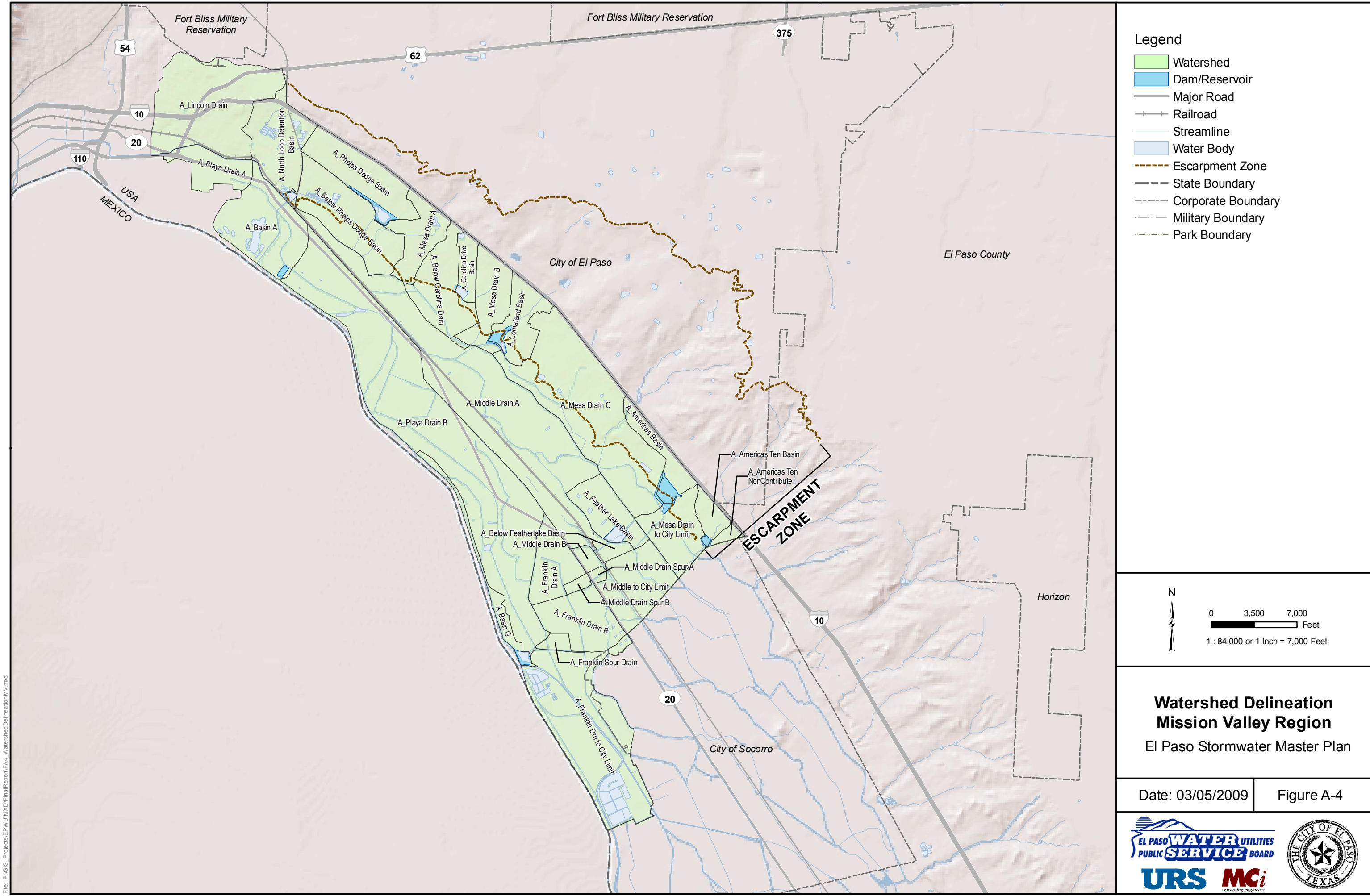
**Watershed Delineation
East Side Region**

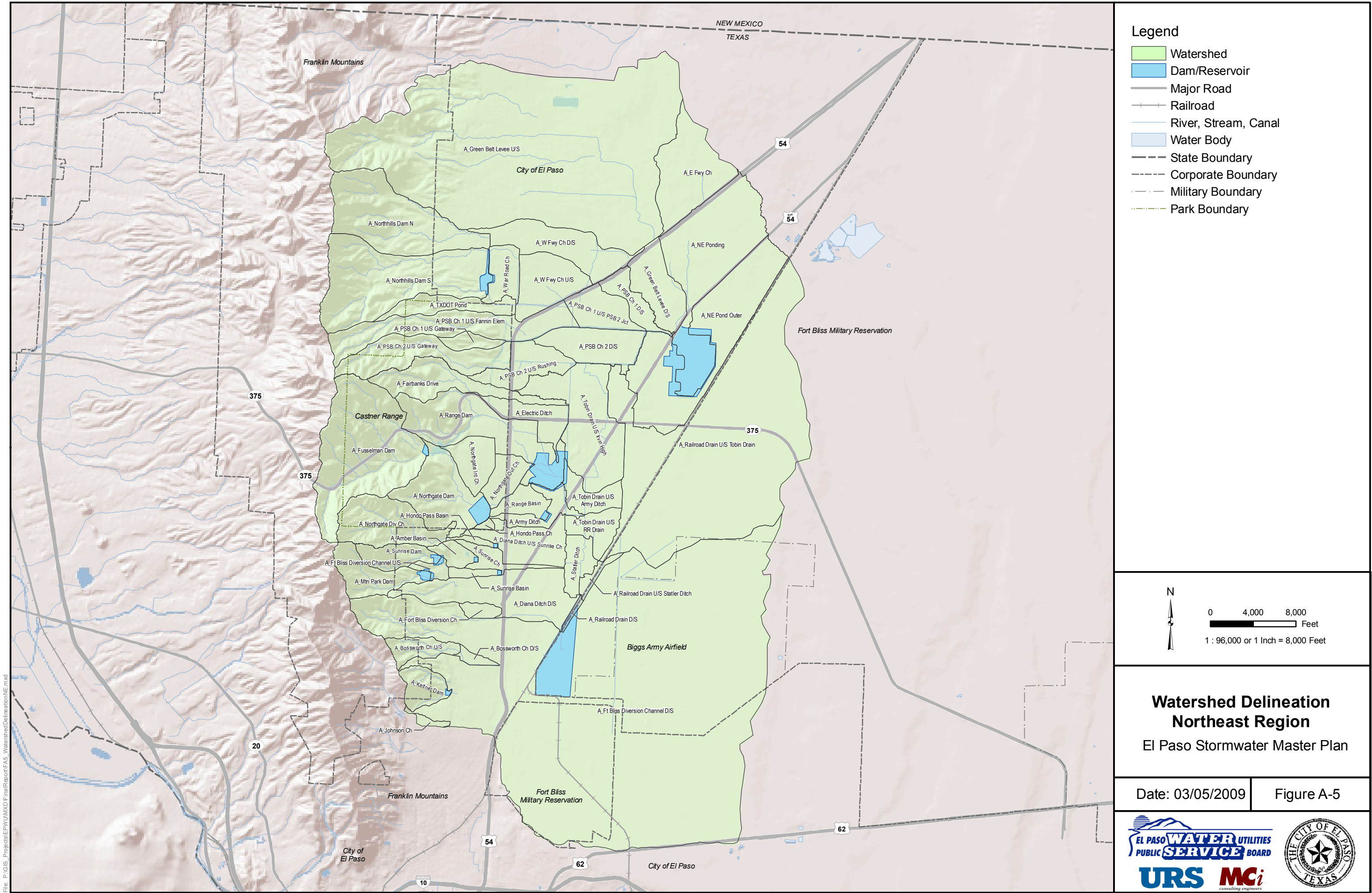
El Paso Stormwater Master Plan

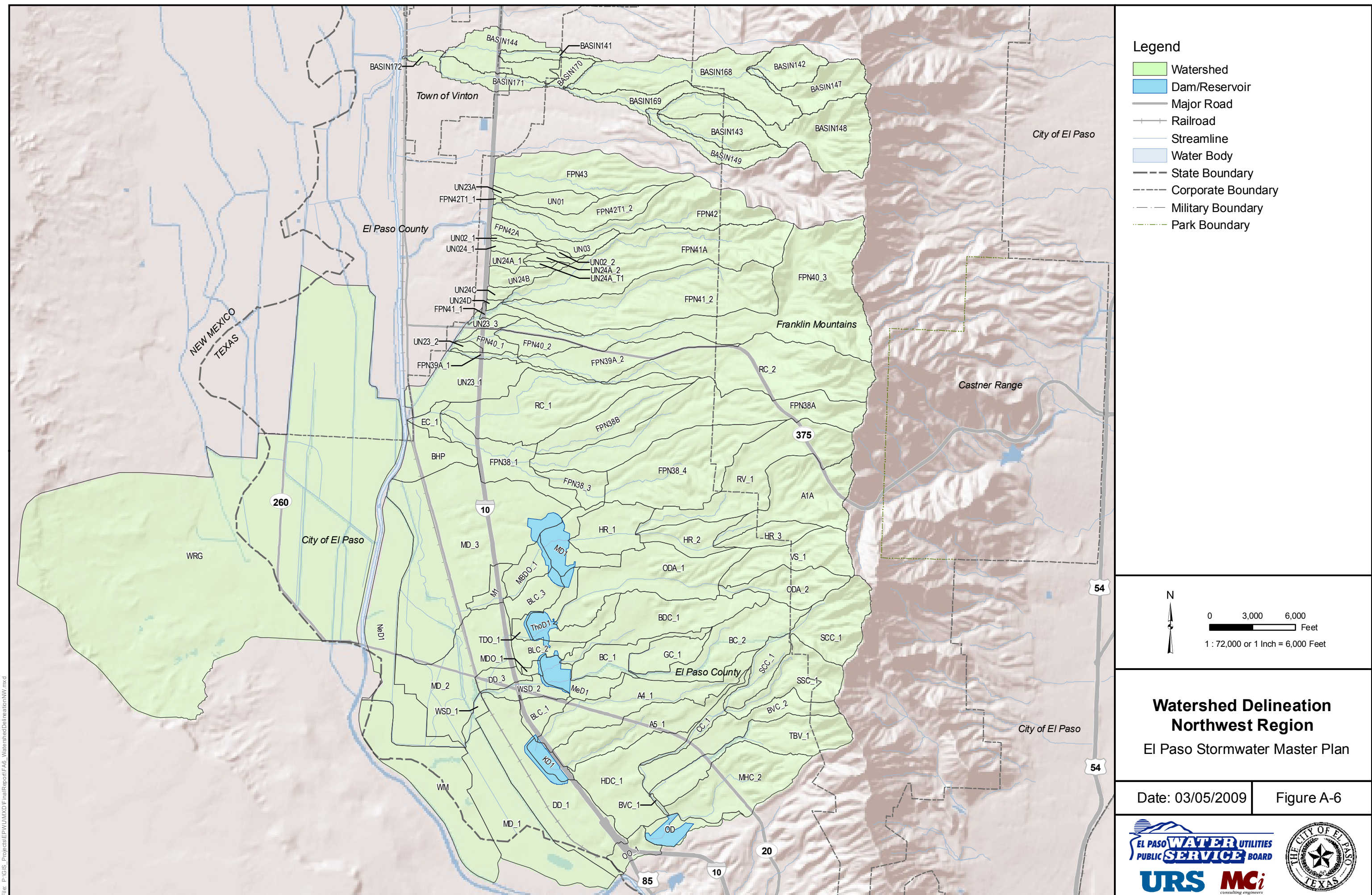
Date: 03/05/2009

Figure A-3

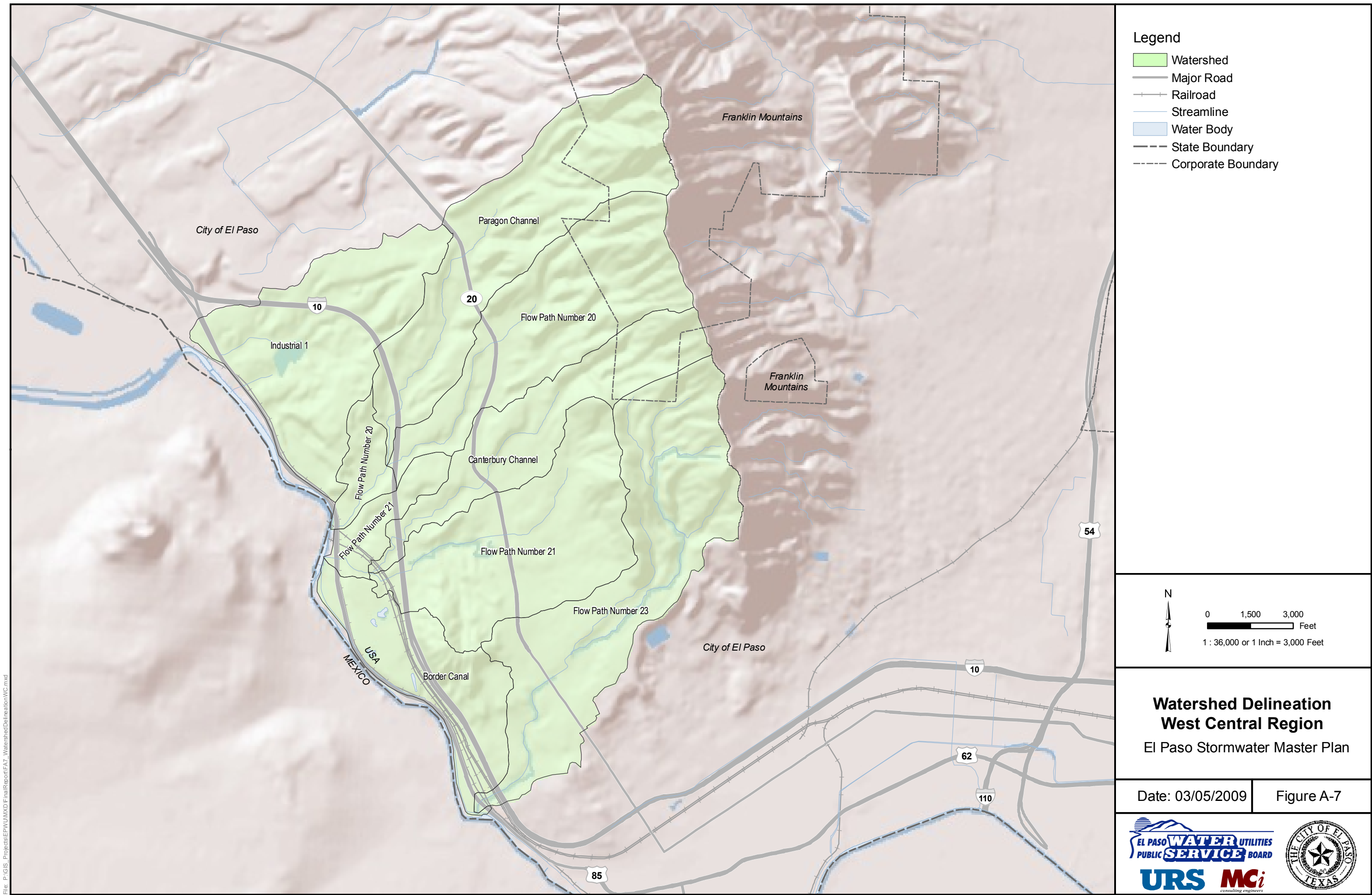








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- Legend**
- Watershed
 - Major Road
 - Railroad
 - Streamline
 - Water Body
 - State Boundary
 - Corporate Boundary

N

0 1,500 3,000 Feet

1 : 36,000 or 1 Inch = 3,000 Feet

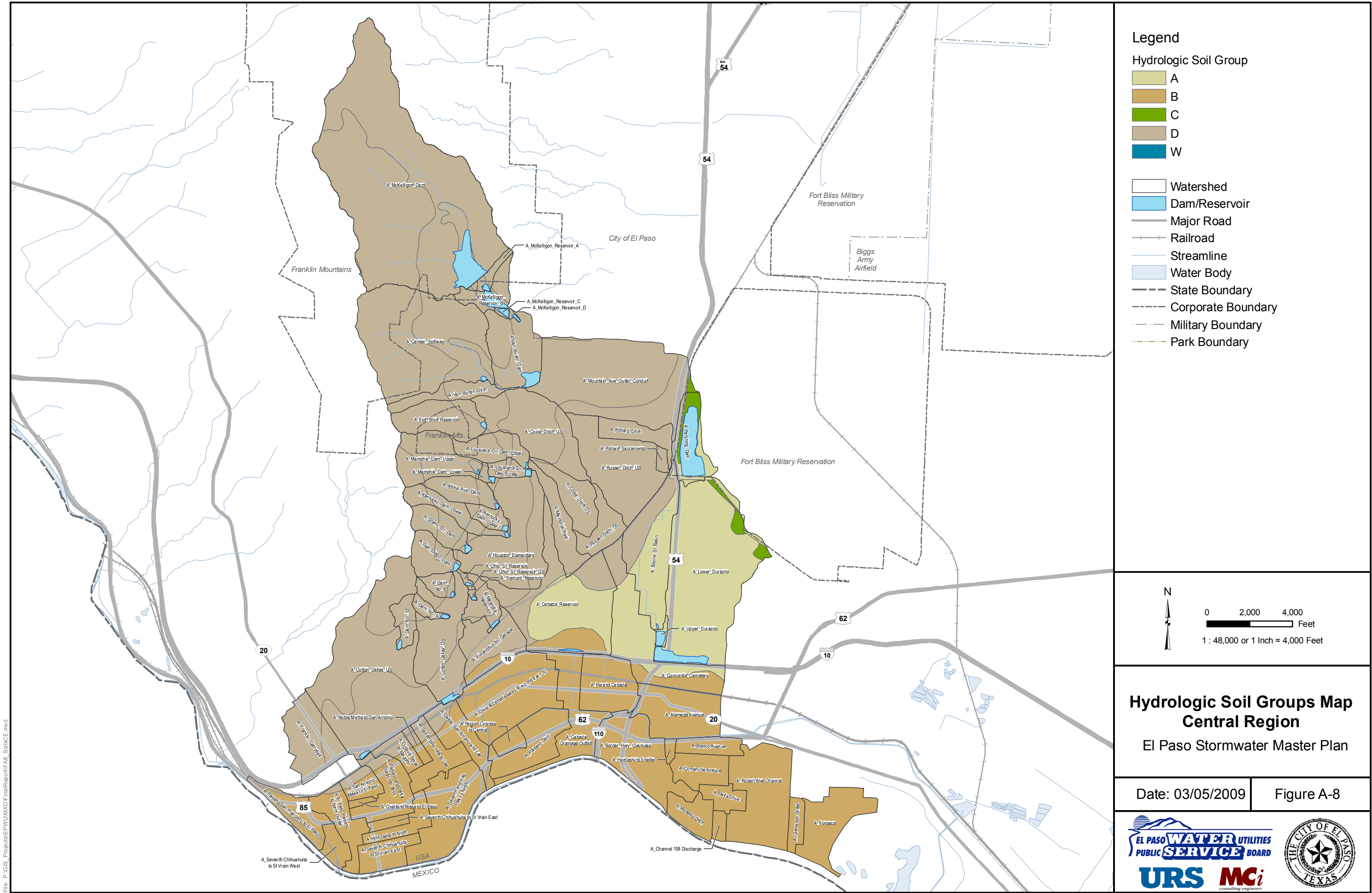
**Watershed Delineation
West Central Region**

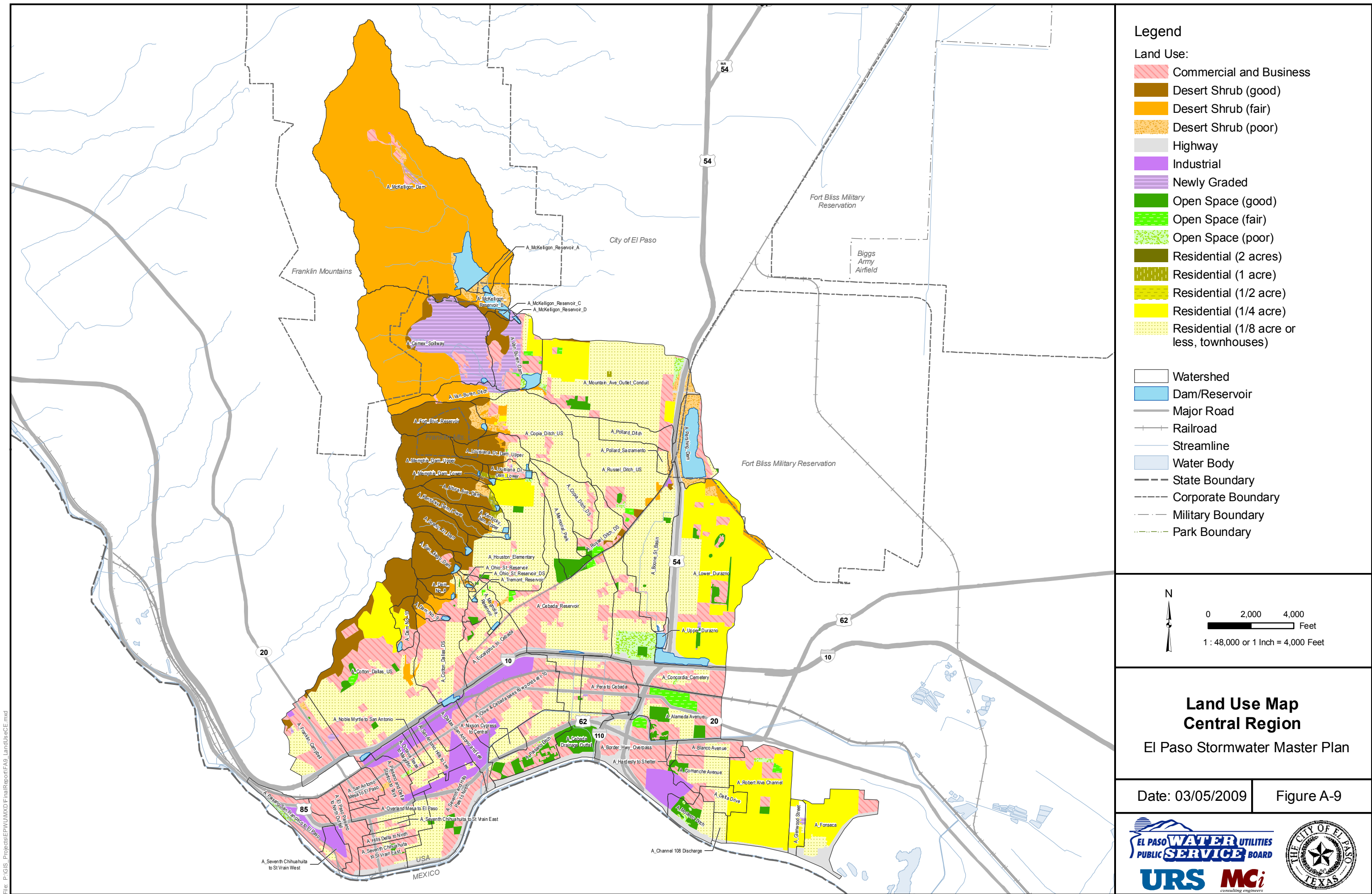
El Paso Stormwater Master Plan

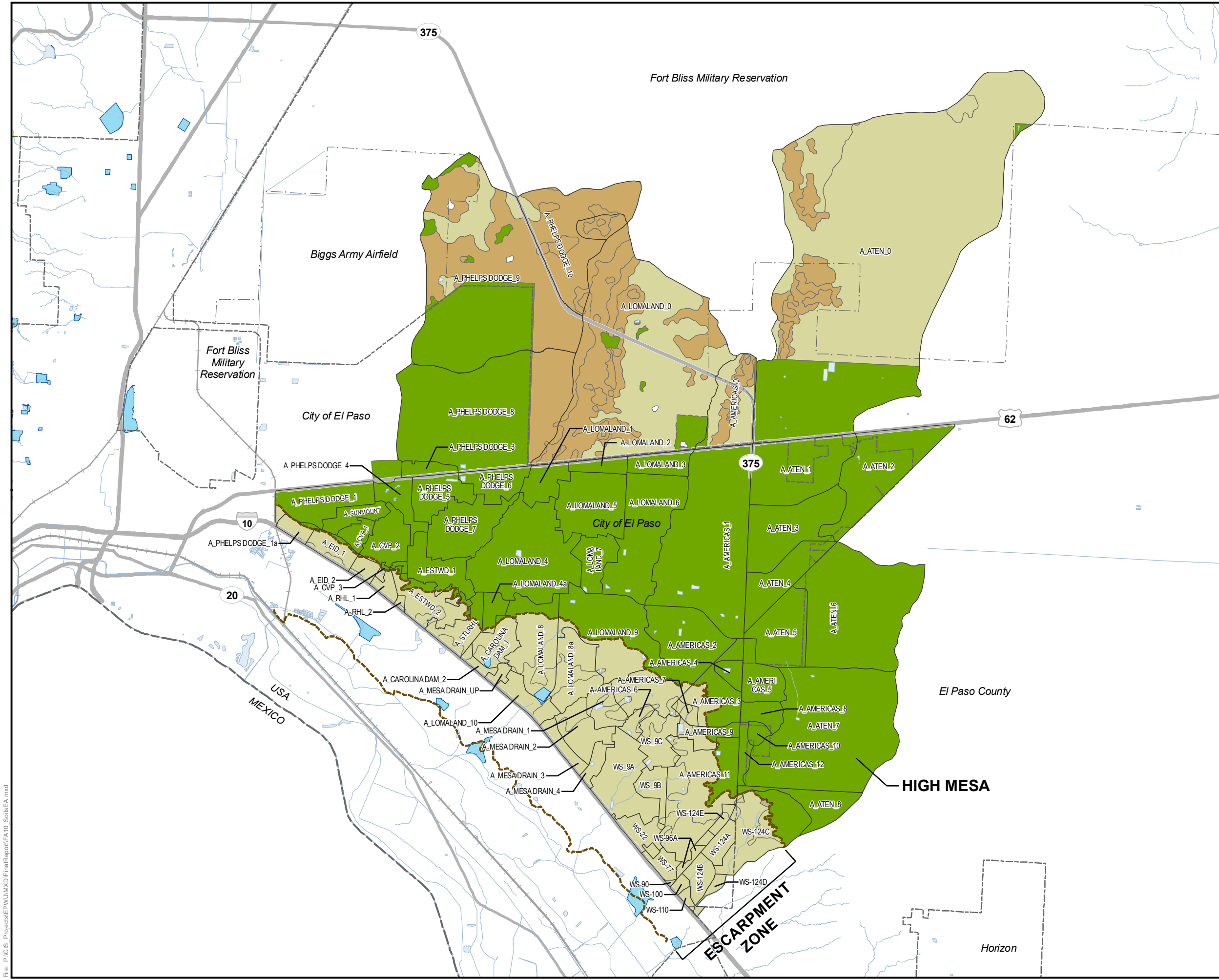
Date: 03/05/2009 Figure A-7



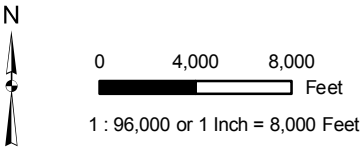
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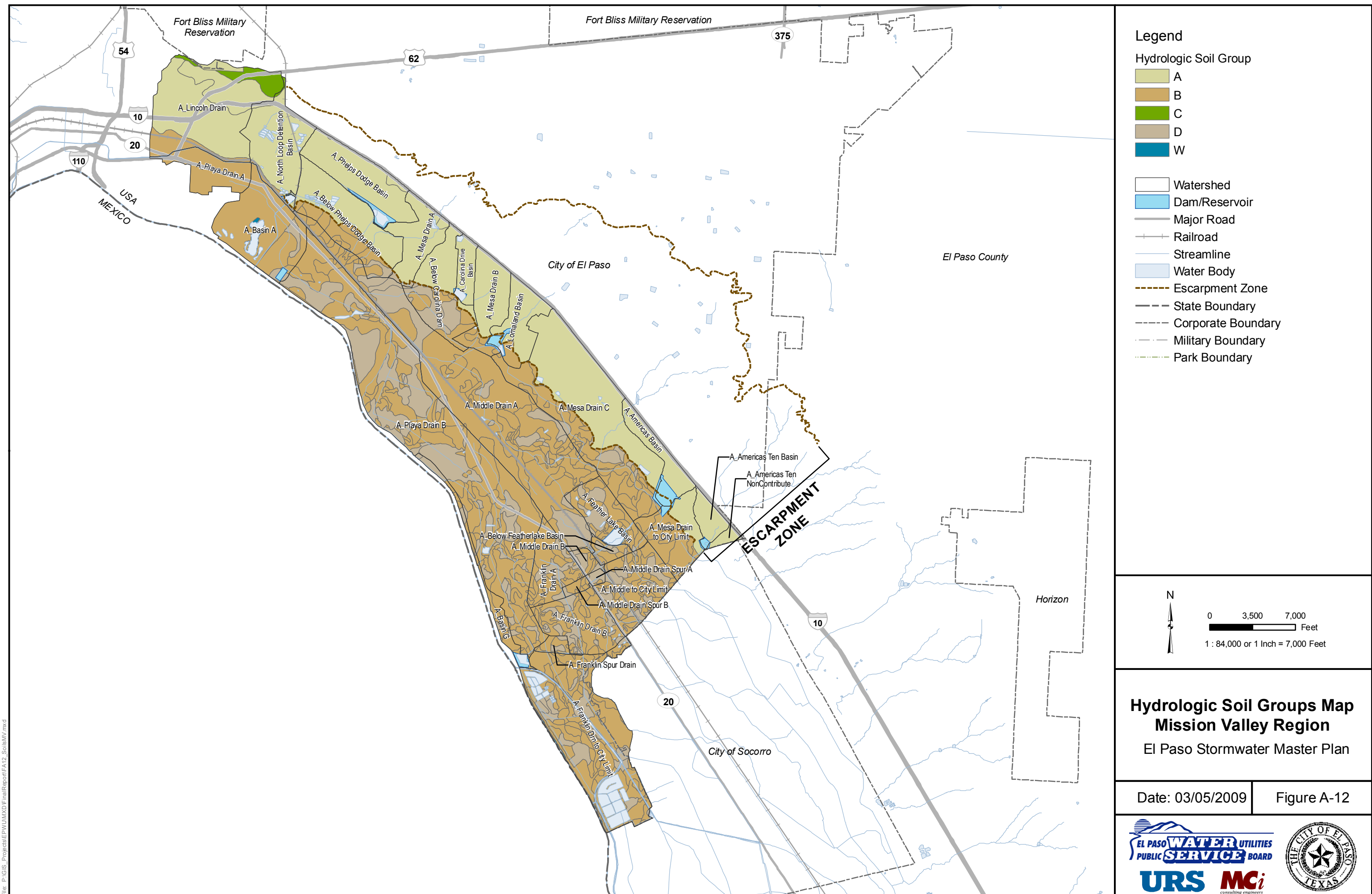
- Legend**
- Hydrologic Soil Group
- A
 - B
 - C
 - D
- Watershed
- Dam/Reservoir
- Major Road
- Railroad
- Streamline
- Water Body
- Escarpment Zone
- State Boundary
- Corporate Boundary
- Military Boundary
- Park Boundary

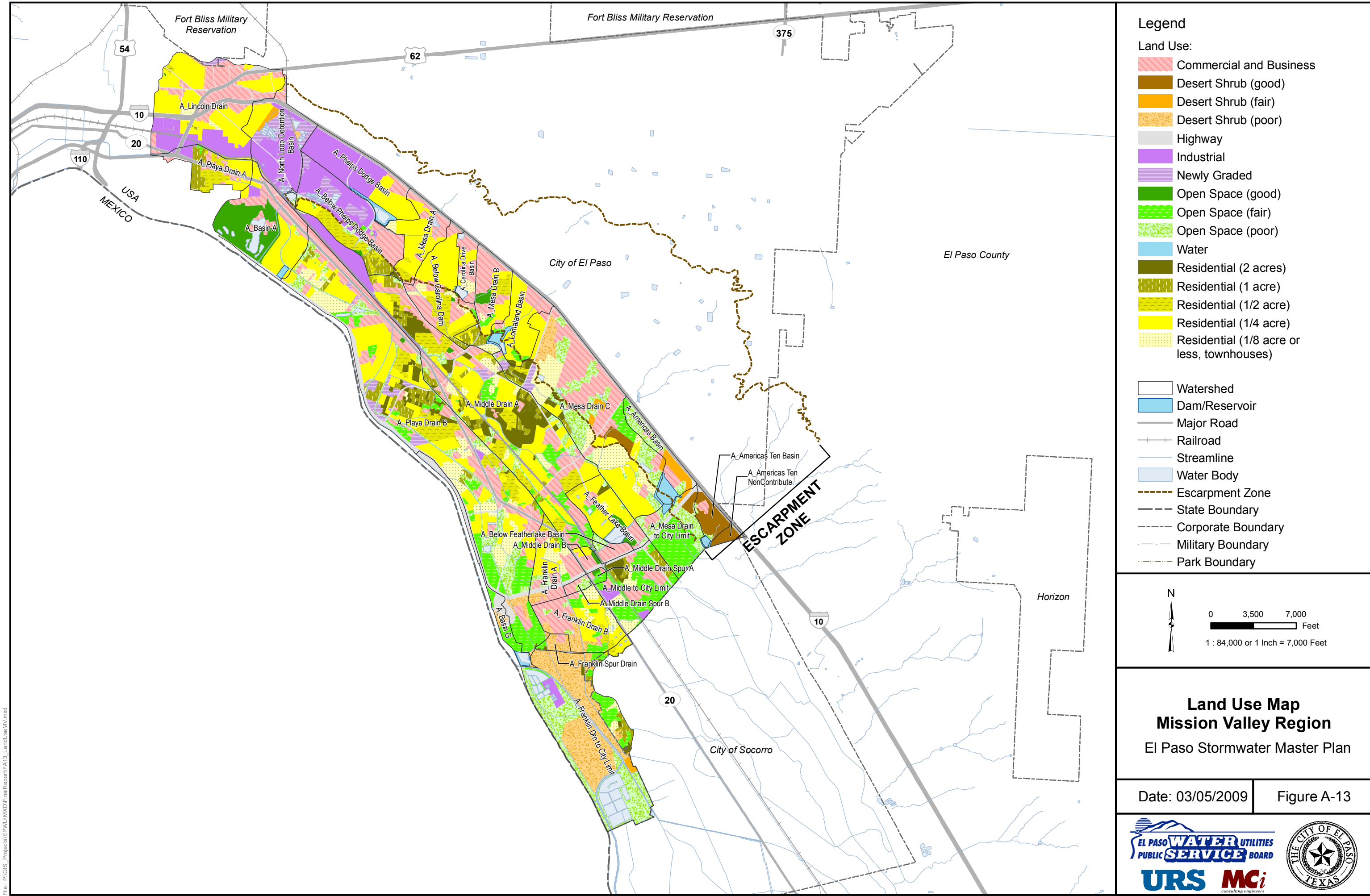


Hydrologic Soil Groups Map
East Side Region
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-10





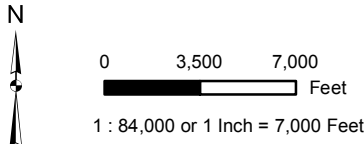


Legend

Land Use:

- Commercial and Business
- Desert Shrub (good)
- Desert Shrub (fair)
- Desert Shrub (poor)
- Highway
- Industrial
- Newly Graded
- Open Space (good)
- Open Space (fair)
- Open Space (poor)
- Water
- Residential (2 acres)
- Residential (1 acre)
- Residential (1/2 acre)
- Residential (1/4 acre)
- Residential (1/8 acre or less, townhouses)

- Watershed
- Dam/Reservoir
- Major Road
- Railroad
- Streamline
- Water Body
- Escarpment Zone
- State Boundary
- Corporate Boundary
- Military Boundary
- Park Boundary

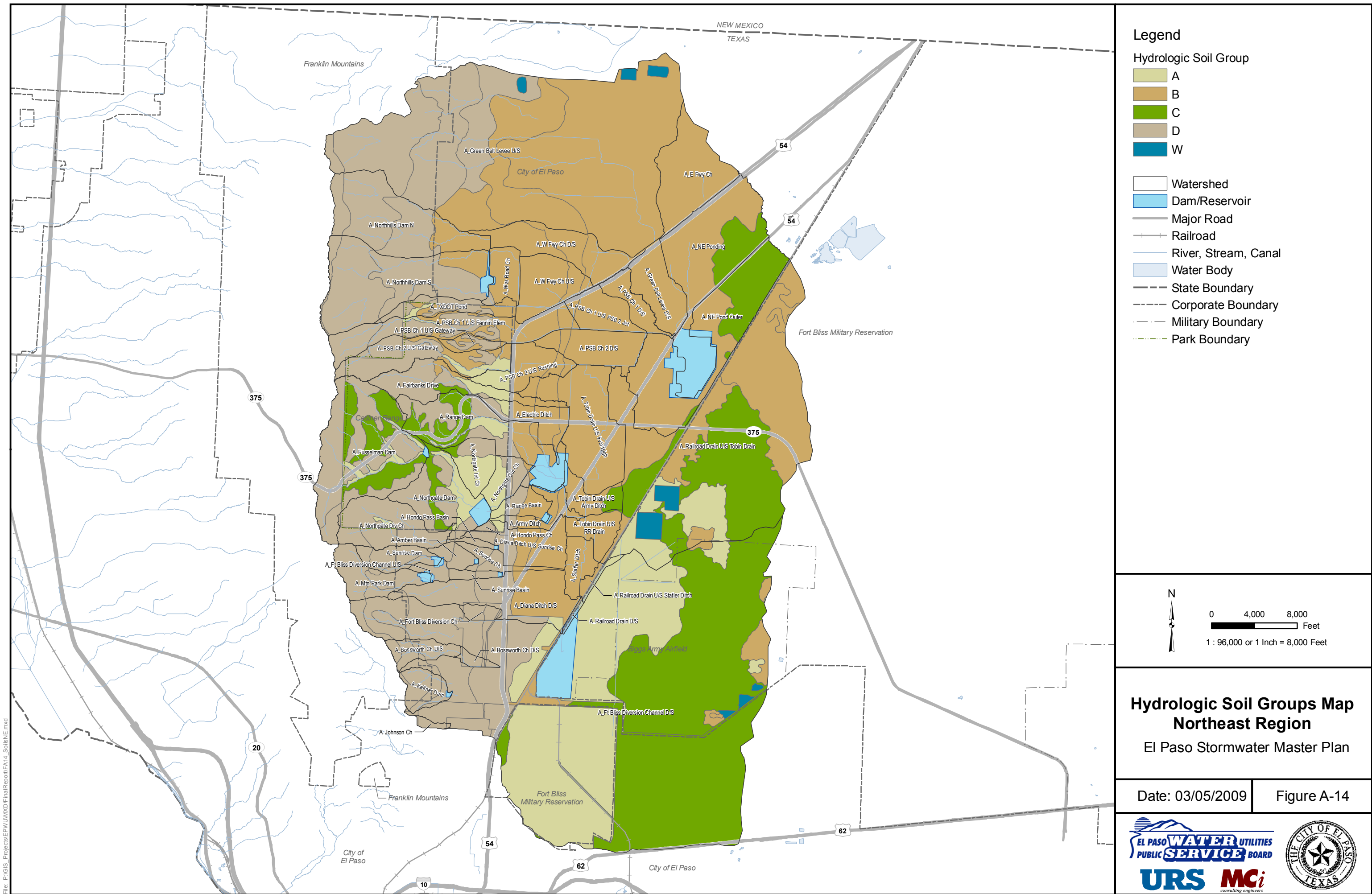


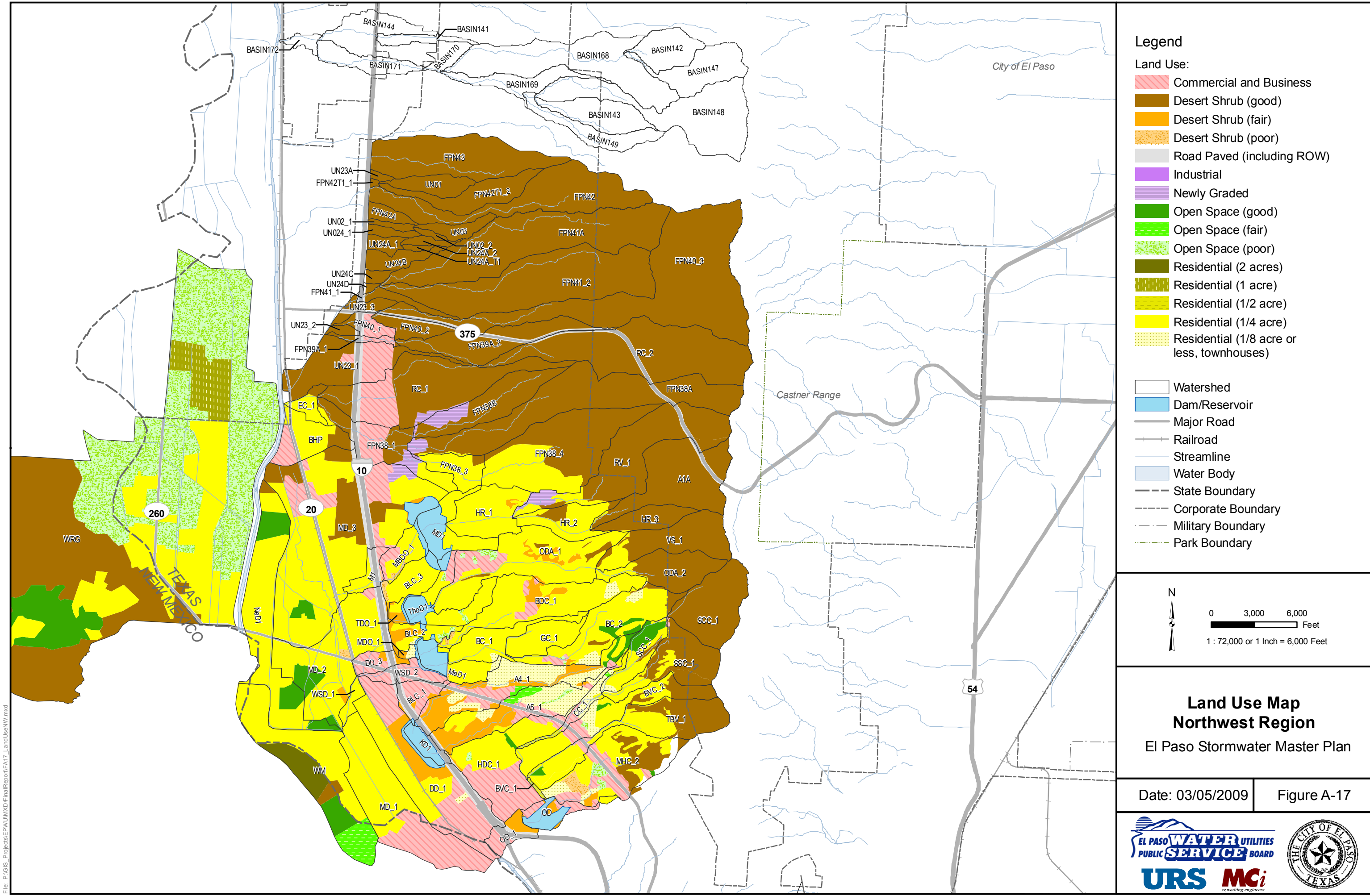
Land Use Map
Mission Valley Region
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-13



File: P:\GIS_Projects\EPW\MXD\FinalReport\F14_SoilsNE.mxd



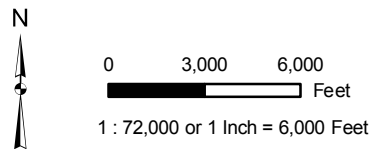


Legend

Land Use:

- Commercial and Business
- Desert Shrub (good)
- Desert Shrub (fair)
- Desert Shrub (poor)
- Road Paved (including ROW)
- Industrial
- Newly Graded
- Open Space (good)
- Open Space (fair)
- Open Space (poor)
- Residential (2 acres)
- Residential (1 acre)
- Residential (1/2 acre)
- Residential (1/4 acre)
- Residential (1/8 acre or less, townhouses)

- Watershed
- Dam/Reservoir
- Major Road
- Railroad
- Streamline
- Water Body
- State Boundary
- Corporate Boundary
- Military Boundary
- Park Boundary

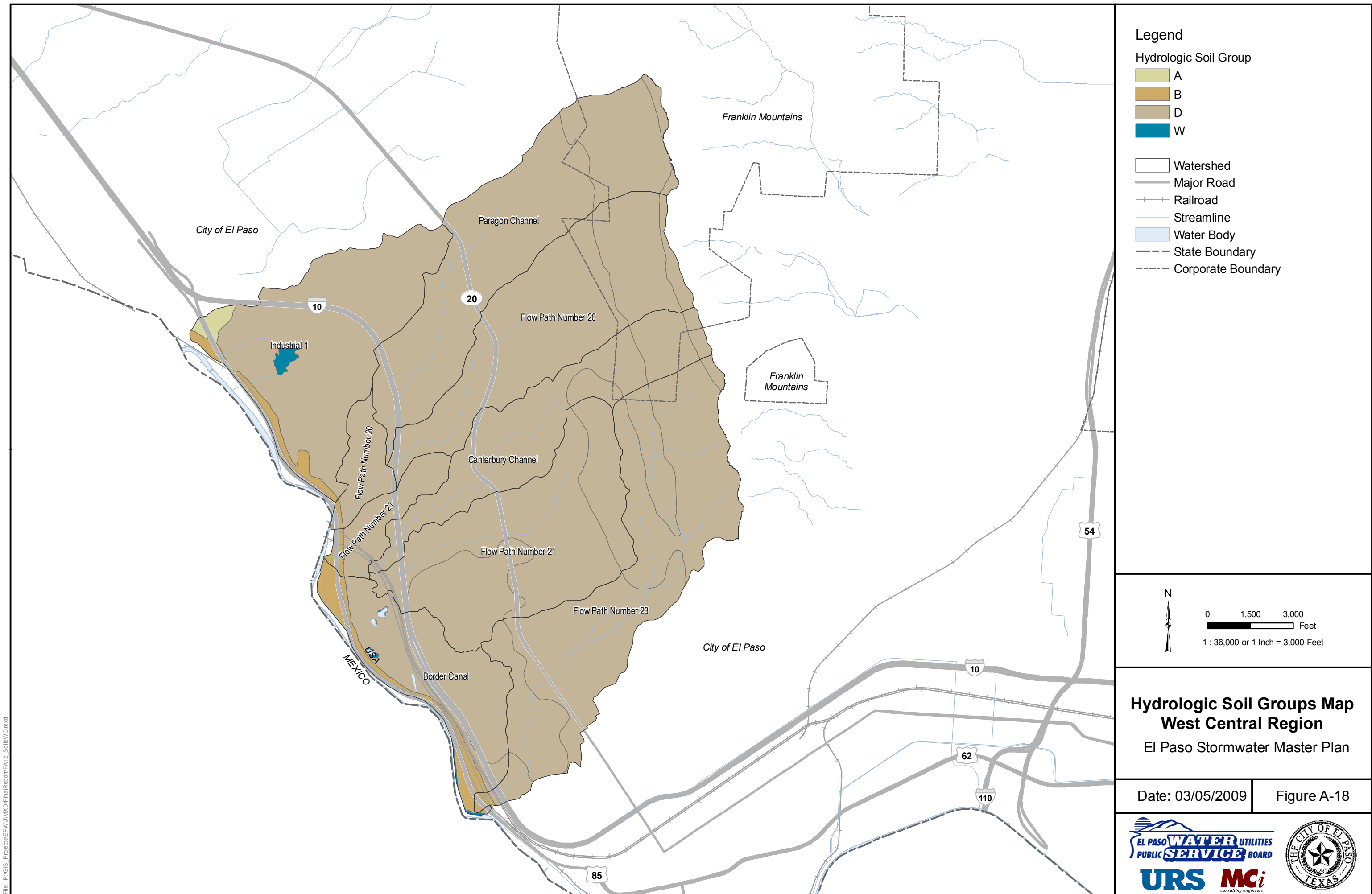


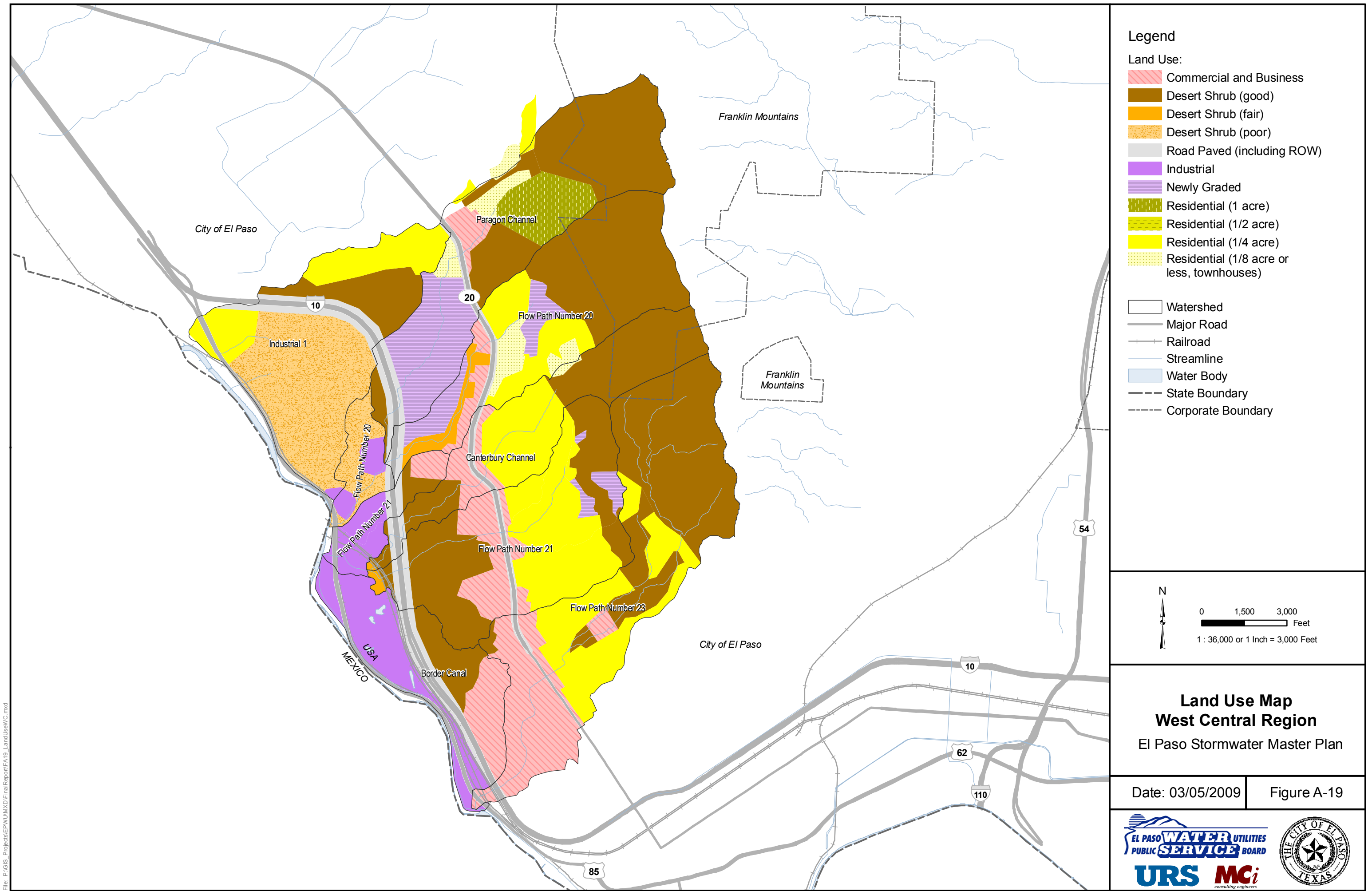
**Land Use Map
Northwest Region**
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-17

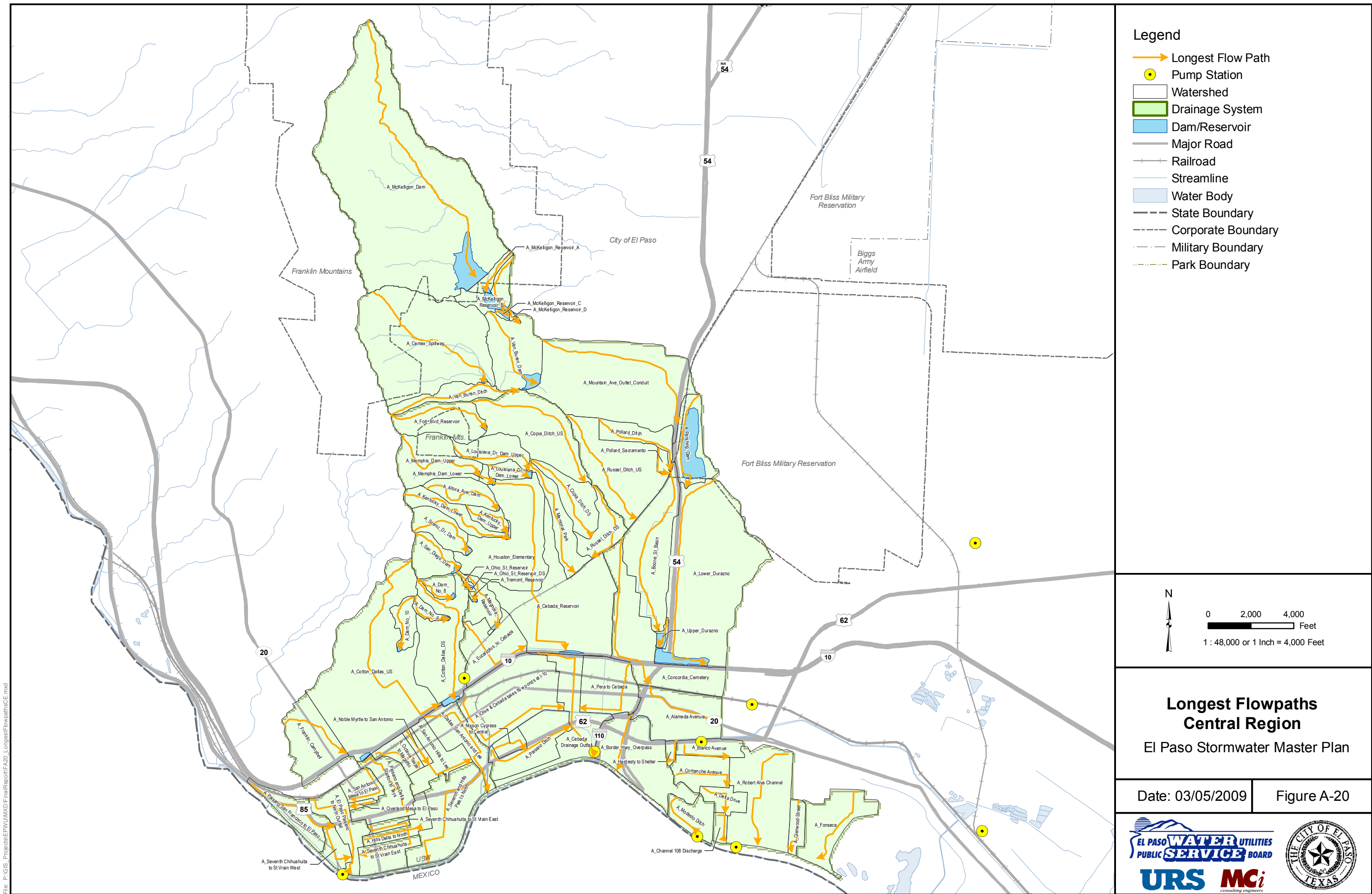


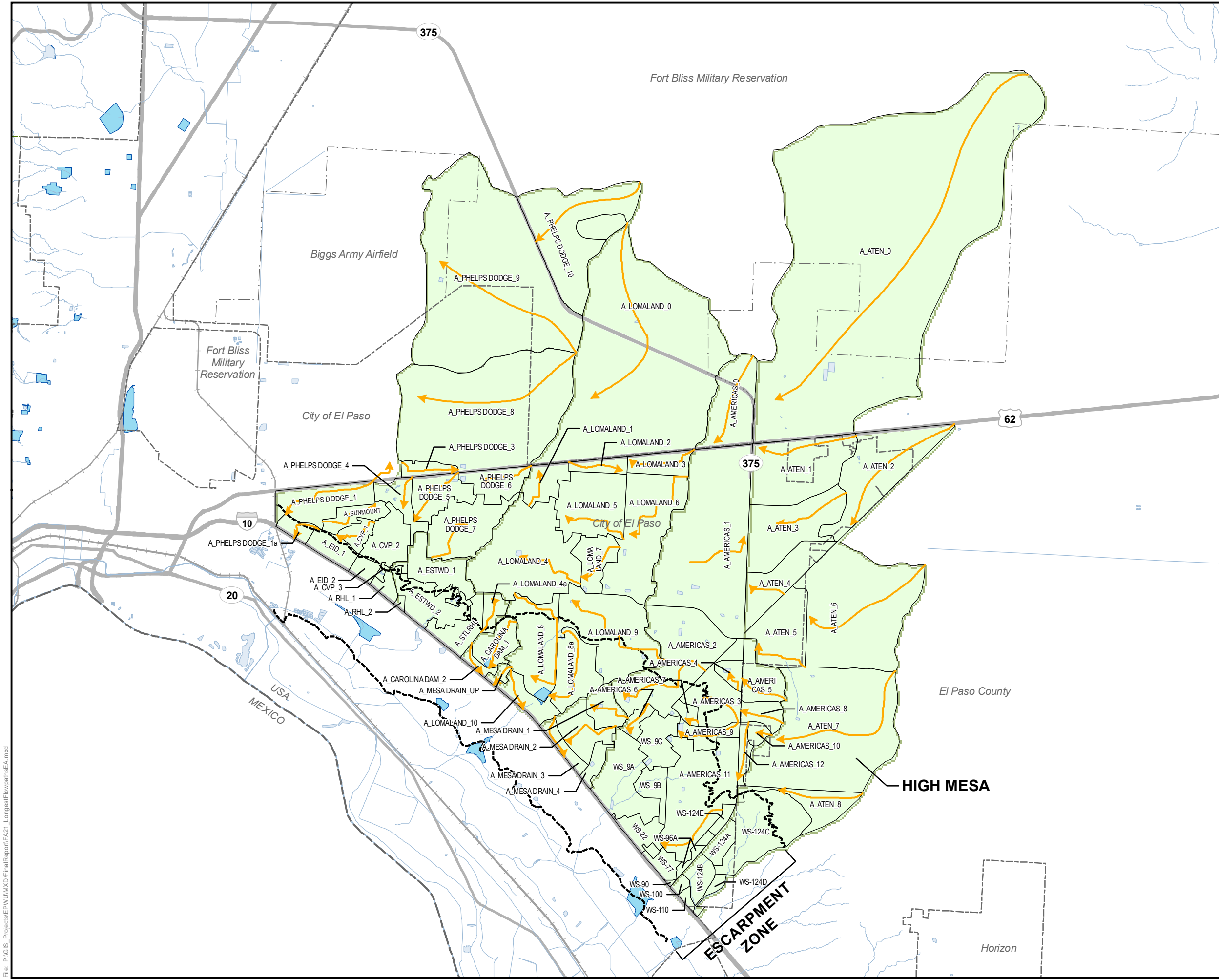
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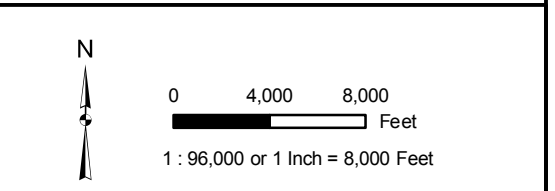


File: P:\GIS_Projects\EPWUMXD\FinalReport\FigA20_LongestFlowpathsCE.mxd





- Legend**
- Longest Flow Path
 - Watershed
 - Drainage System
 - Dam/Reservoir
 - Major Road
 - Railroad
 - Streamline
 - Water Body
 - State Boundary
 - Corporate Boundary
 - Military Boundary
 - Park Boundary

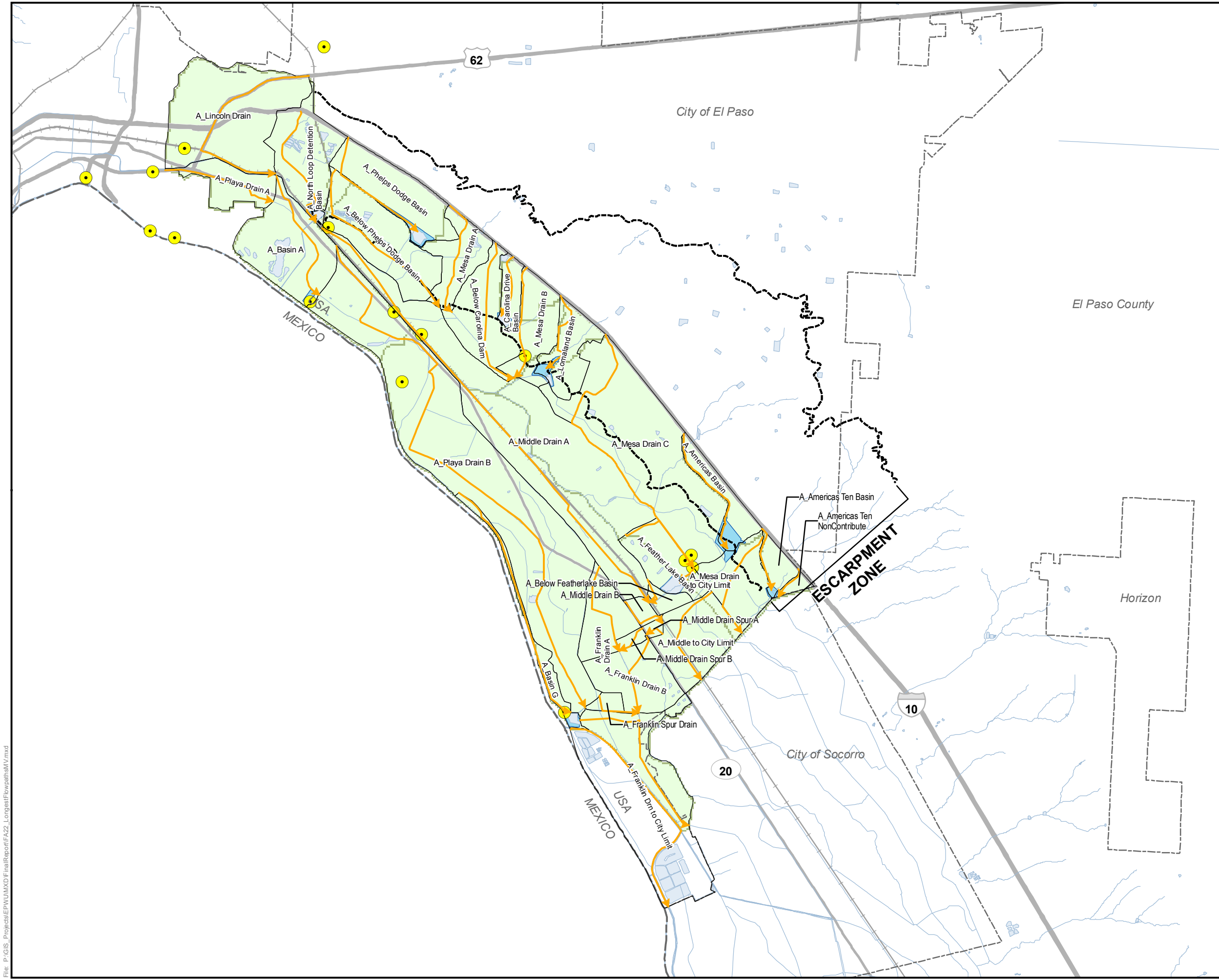


**Longest Flowpaths
East Side Region**

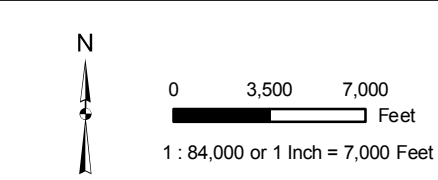
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-21





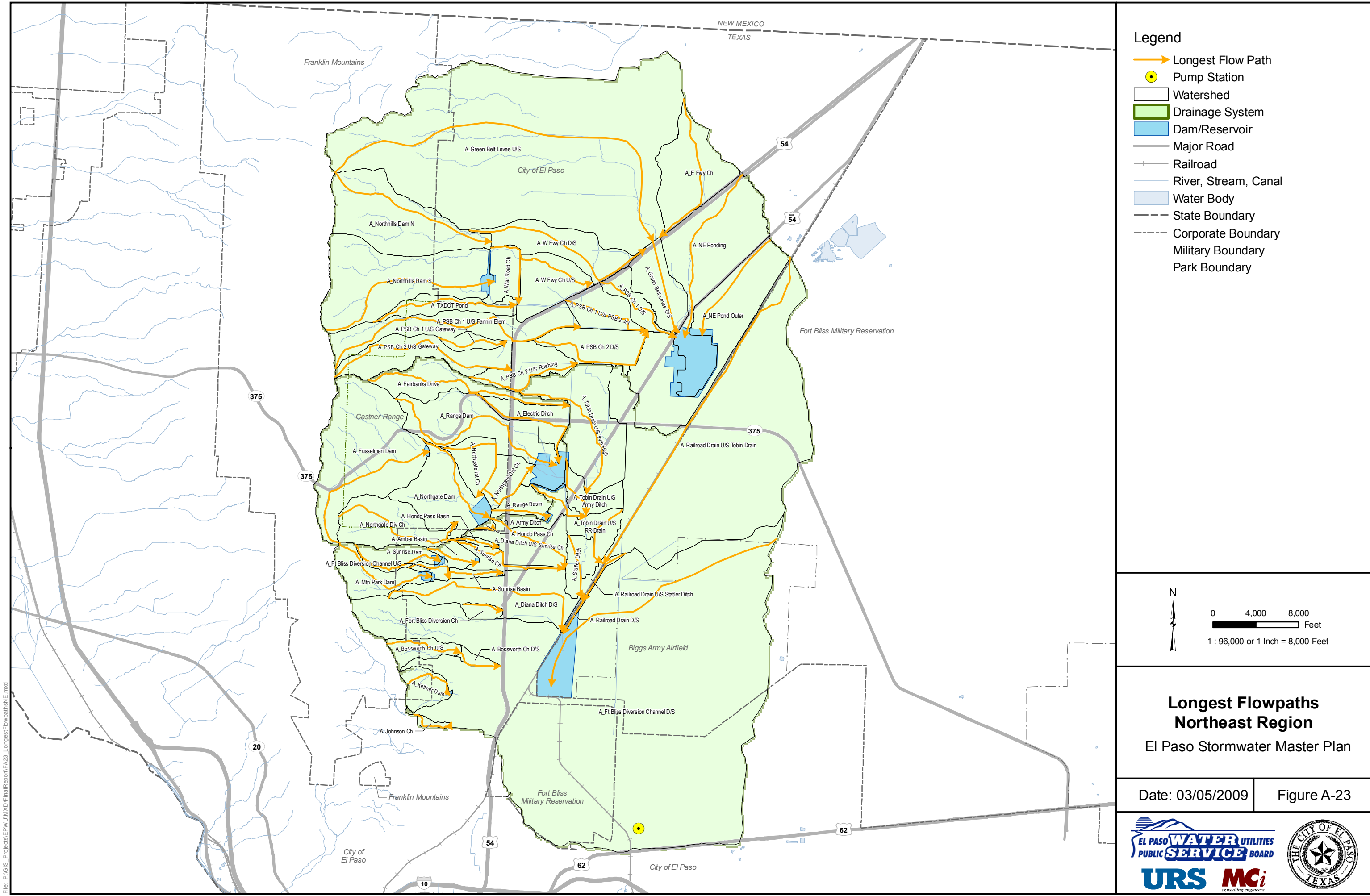
- Legend**
- Longest Flow Path
 - Pump Station
 - Watershed
 - Drainage System
 - Dam/Reservoir
 - Major Road
 - Railroad
 - Streamline
 - Water Body
 - State Boundary
 - Corporate Boundary
 - Military Boundary
 - Park Boundary



**Longest Flowpaths
Mission Valley Region**
El Paso Stormwater Master Plan

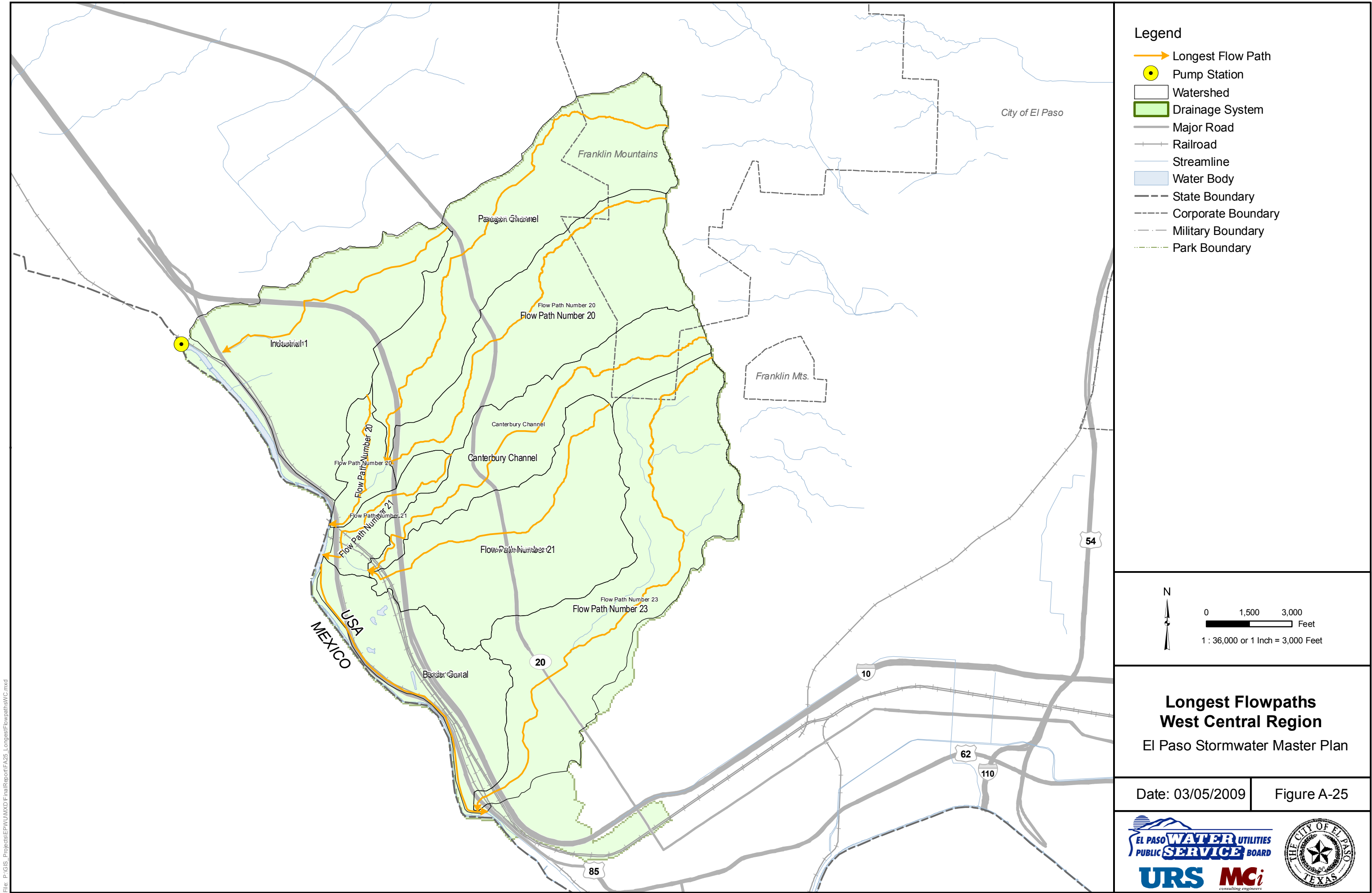
Date: 03/05/2009 Figure A-22



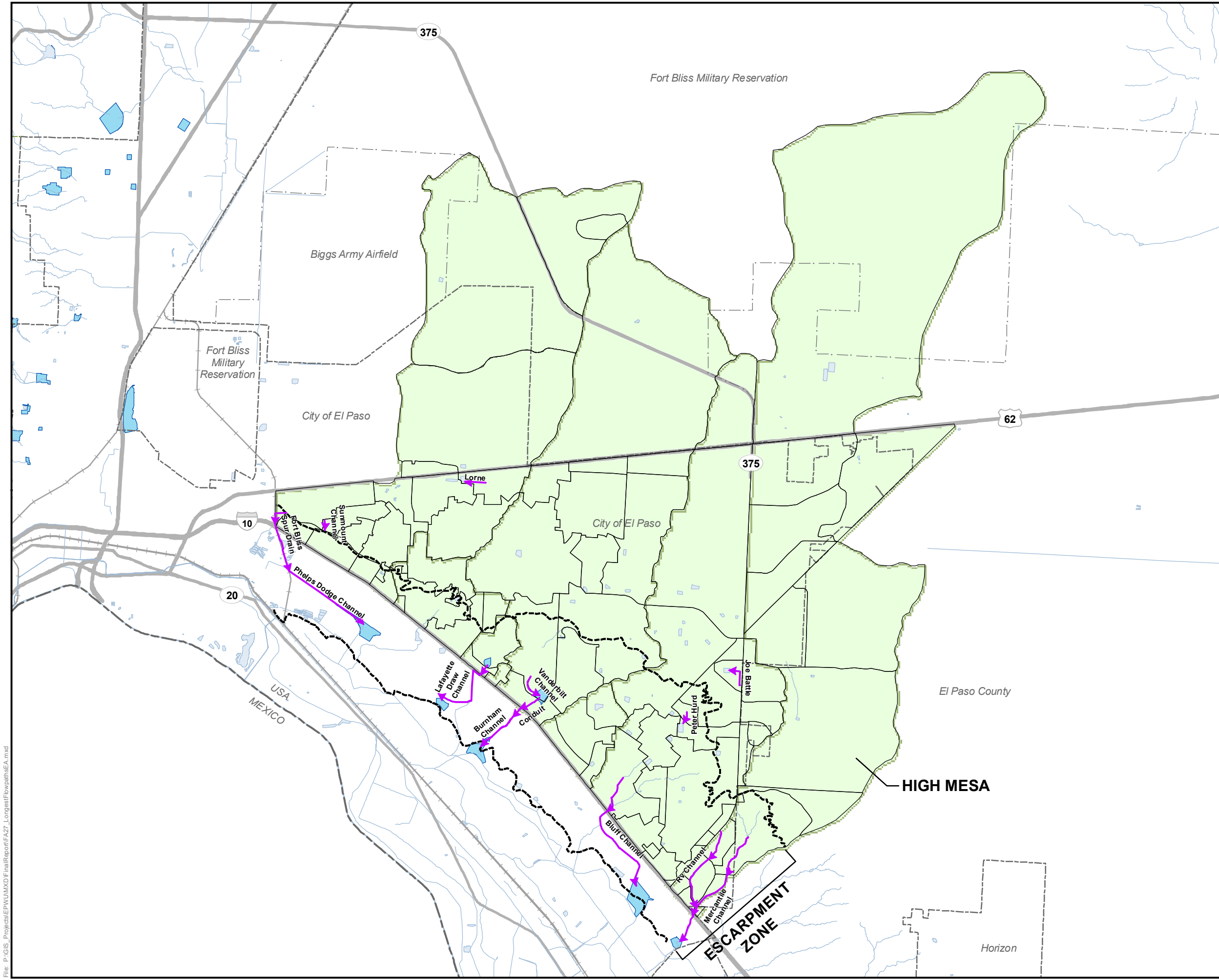


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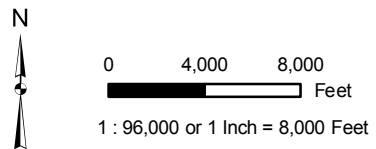
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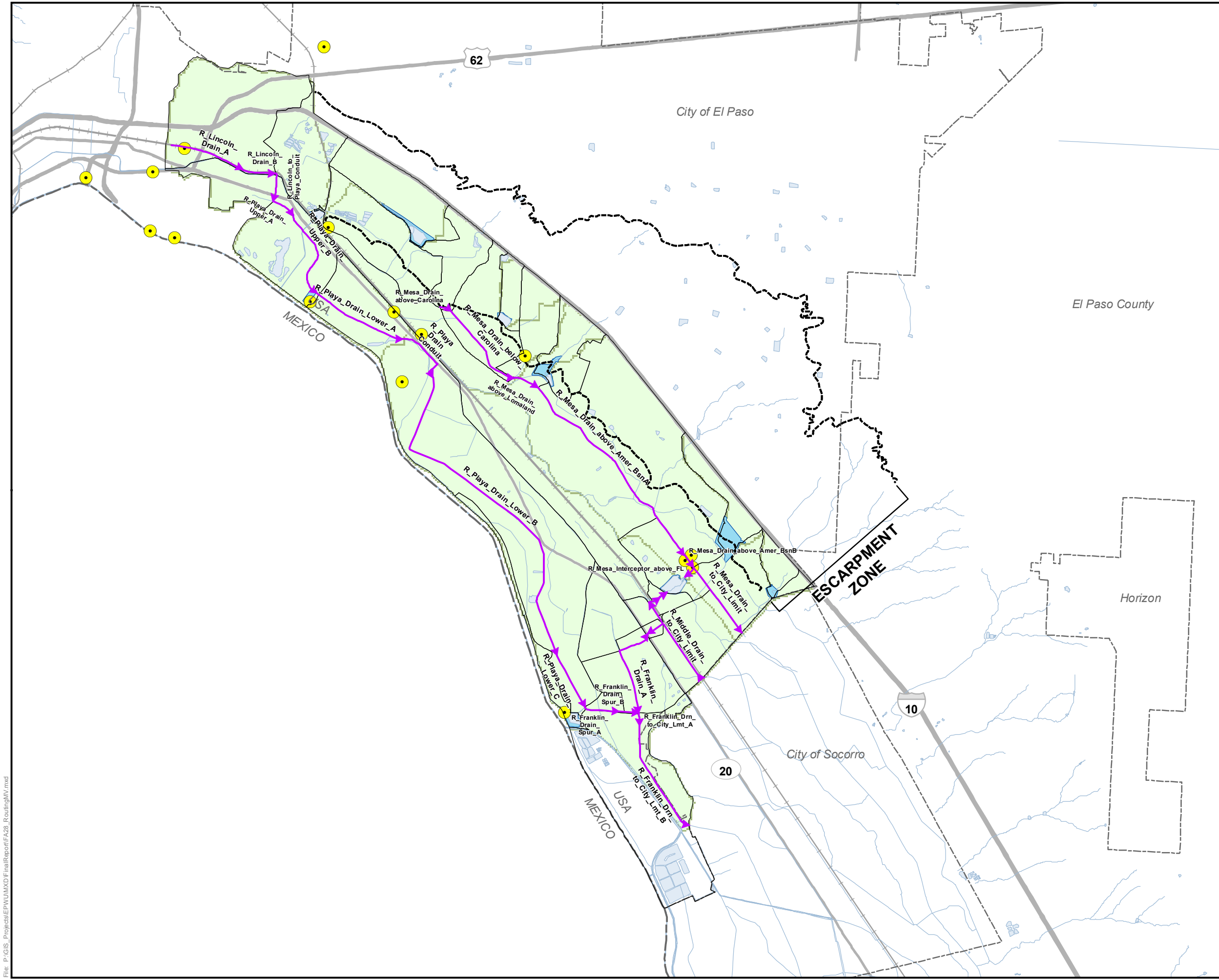
- Legend**
- Routing Reach
 - Watershed
 - Drainage System
 - Dam/Reservoir
 - Major Road
 - Railroad
 - Streamline
 - Water Body
 - State Boundary
 - Corporate Boundary
 - Military Boundary
 - Park Boundary



**Routing Reaches
East Side Region**
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-27





Legend

Routing Reach

Pump Station

Watershed

Drainage System

Dam/Reservoir

Major Road

Railroad

Streamline

Water Body

State Boundary

Corporate Boundary

Military Boundary

Park Boundary

N

03,5007,000

Feet

1 : 84,000 or 1 Inch = 7,000 Feet

Routing Reaches

Mission Valley Region

El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-28

EL PASO WATER UTILITIES

PUBLIC SERVICE BOARD

URS

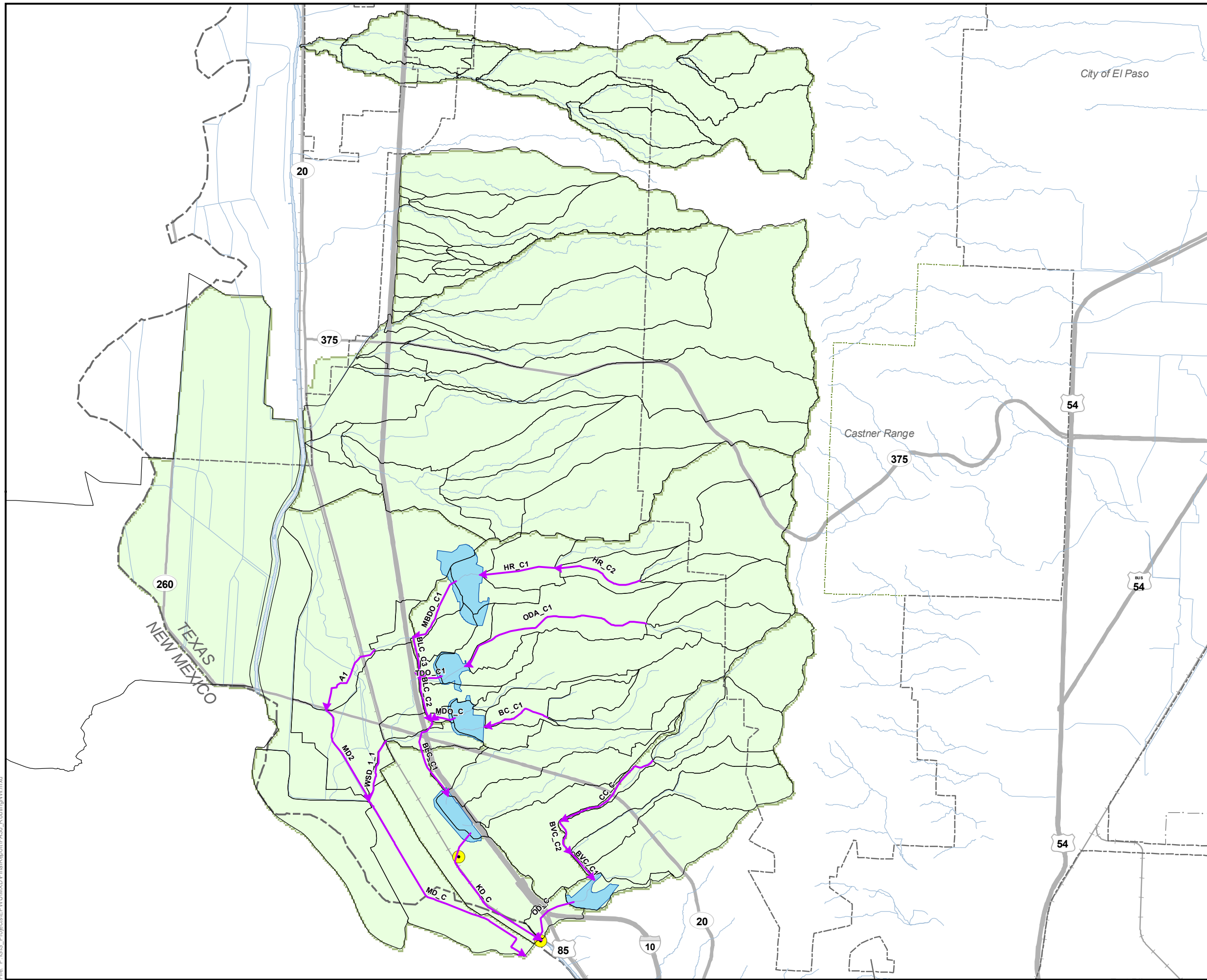
MCi

consulting engineers

THE CITY OF EL PASO

TEXAS

File: P:\GIS_Projects\EPWUMXD\FinalReport\FA30_RoutingNW.mxd



Legend

- Routing Reach
- Pump Station
- Watershed
- Drainage System
- Dam/Reservoir
- Major Road
- Railroad
- Streamline
- Water Body
- State Boundary
- Corporate Boundary
- Military Boundary
- Park Boundary



0 3,000 6,000 Feet
1 : 72,000 or 1 Inch = 6,000 Feet

Routing Reaches Northwest Region

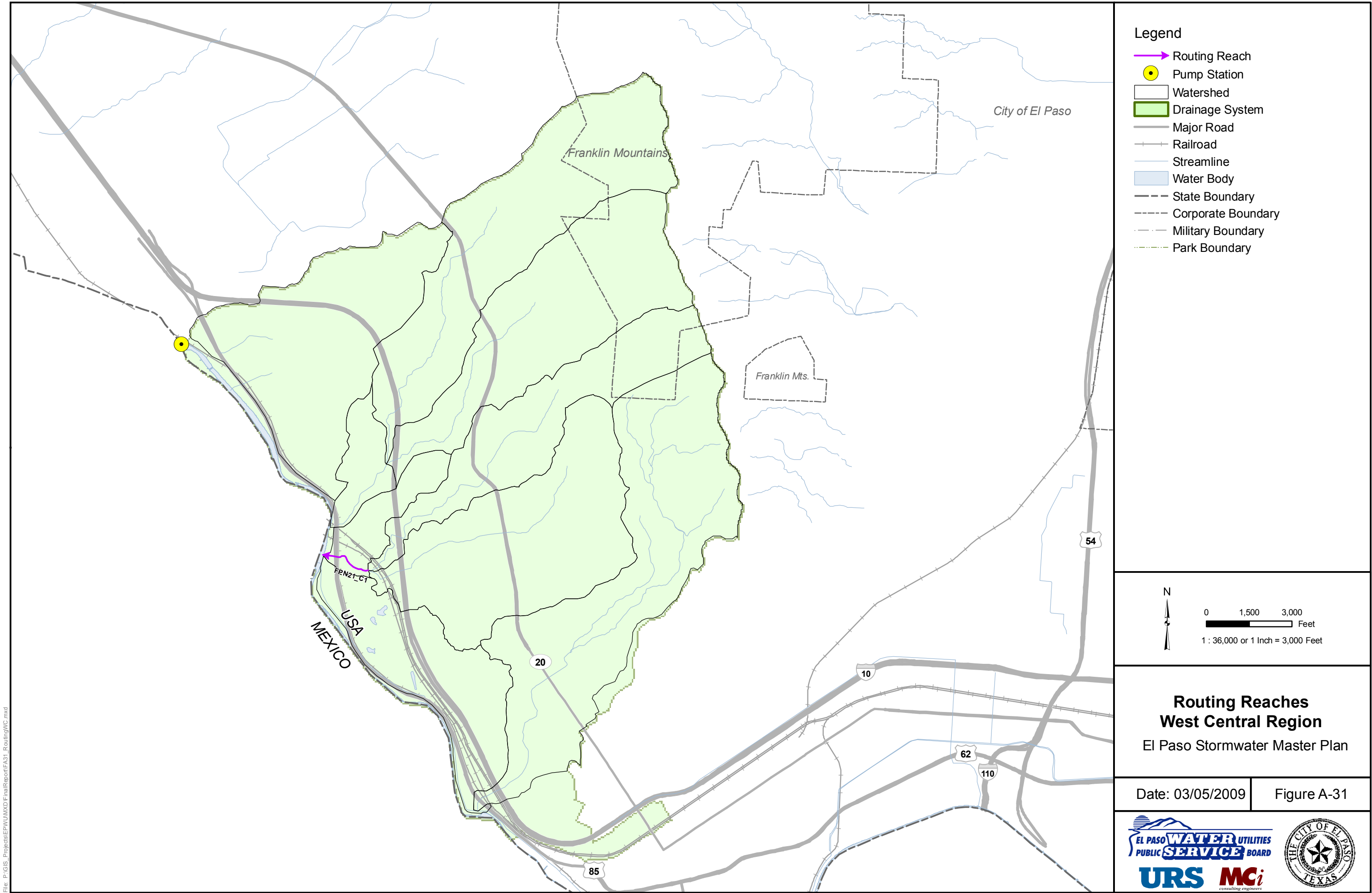
El Paso Stormwater Master Plan

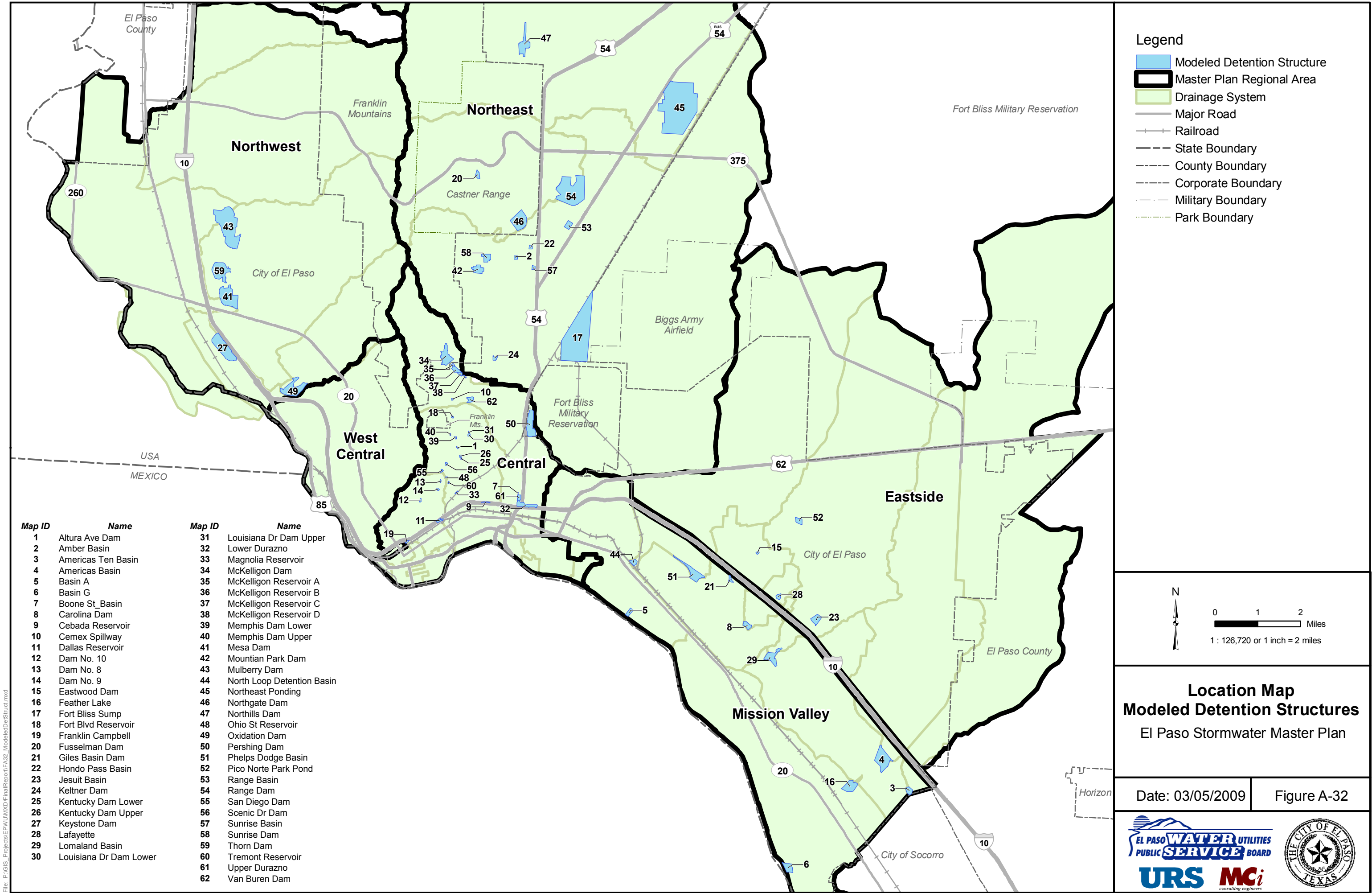
Date: 03/05/2009

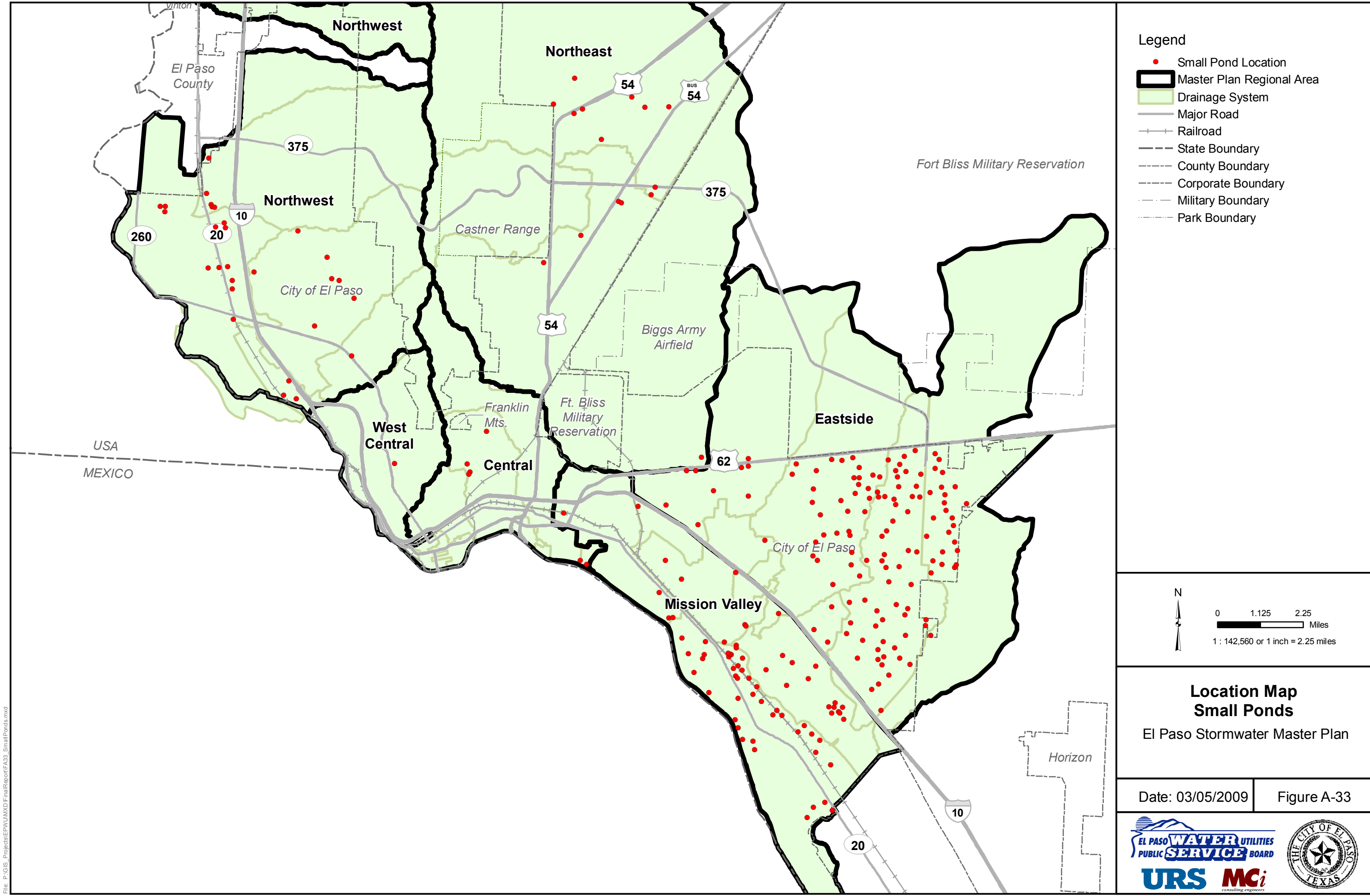
Figure A-30



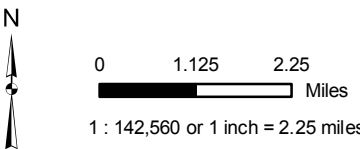
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- Legend**
- Small Pond Location
 - Master Plan Regional Area
 - Drainage System
 - Major Road
 - Railroad
 - State Boundary
 - County Boundary
 - Corporate Boundary
 - Military Boundary
 - Park Boundary

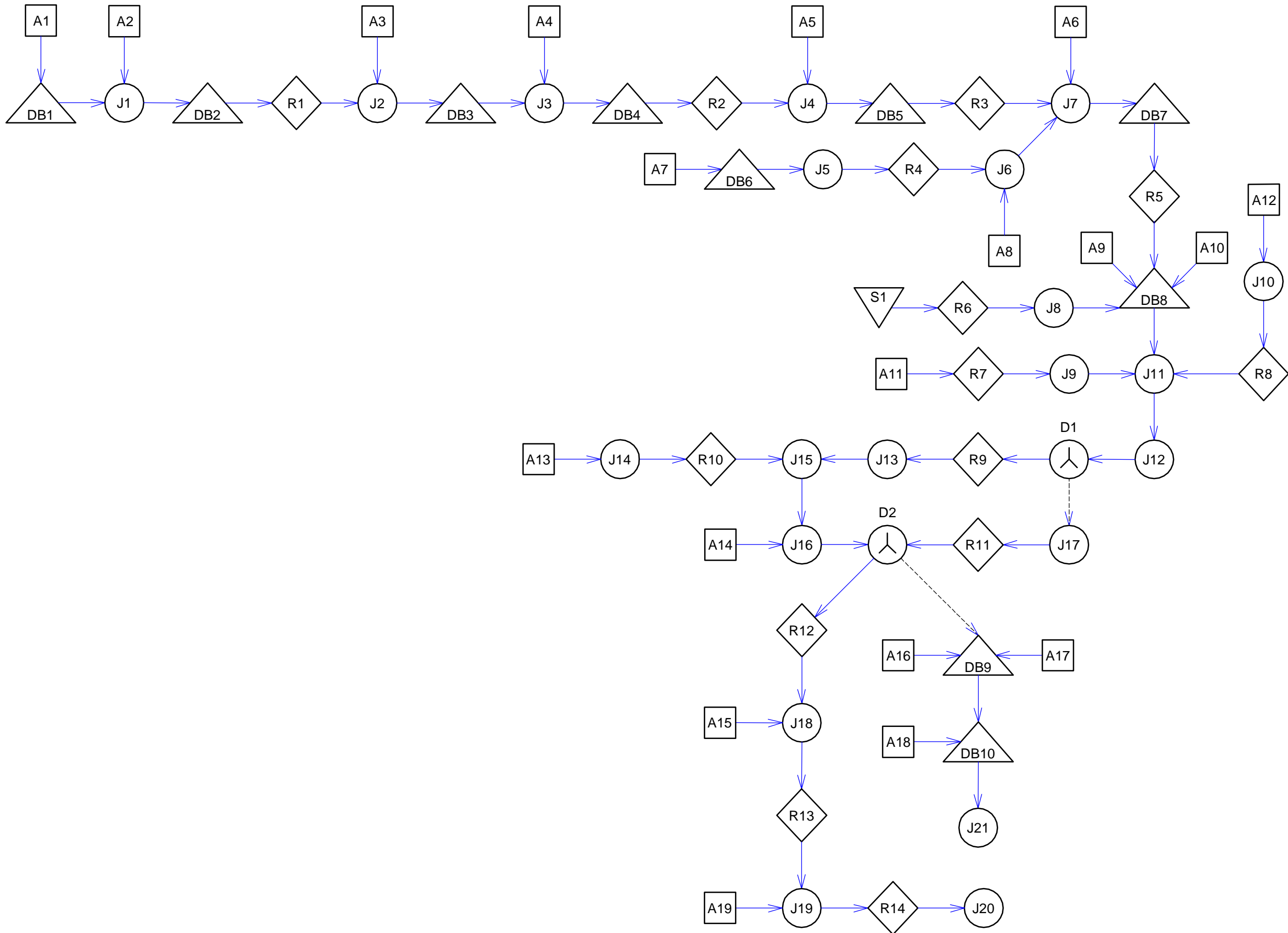


**Location Map
Small Ponds**
El Paso Stormwater Master Plan


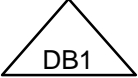


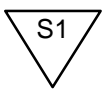



Date: 03/05/2009 Figure A-33



File: Q:\El Paso Master Drainage Plan\Stormwater Master Plan Report\HMS Cad Diagrams\Schematics_App_A_013009.dwg Layout: Fig A-34 User: Scott_Coleman Plotted: Mar 02, 2009 - 10:48am



Legend

-  Basin Areas/Watershed
-  Dams/Basins
-  Reaches
-  Junctions
-  Source
-  Diversions
-  Connecting Lines
-  Diversion Dashed Lines

Government Hills System HEC-HMS Model Layout Central Region

El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-34

| Basin | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| A1 | A_McKelligon_Dam | 2.168 | 1809 | 227.1 |
| A2 | A_McKelligon_Reservoir_A | 0.038 | 80 | 4.1 |
| A3 | A_McKelligon_Reservoir_B | 0.104 | 197 | 11.1 |
| A4 | A_McKelligon_Reservoir_C | 0.009 | 18 | 0.9 |
| A5 | A_McKelligon_Reservoir_D | 0.006 | 16 | 0.8 |
| A6 | A_Van_Buren_Dam | 0.279 | 395 | 35.7 |
| A7 | A_Cemex_Spillway | 0.923 | 1156 | 108.7 |
| A8 | A_Van_Buren_Ditch | 0.120 | 153 | 13.2 |
| A9 | A_Mountain_Ave_Outlet_Condui | 0.876 | 1321 | 112.0 |
| A10 | A_Pershing_Dam | 0.193 | 207 | 16.0 |
| A11 | A_Pollard_Ditch | 0.113 | 211 | 15.4 |
| A12 | A_Pollard_Sacramento | 0.021 | 52 | 2.8 |
| A13 | A_Russel_Ditch_US | 0.434 | 791 | 57.2 |
| A14 | A_Boone_St_Basin | 0.398 | 419 | 36.1 |
| A15 | A_Saipan | 0.152 | 316 | 14.5 |
| A16 | A_Concordia_Cemetery | 0.305 | 388 | 29.2 |
| A17 | A_Upper_Durazno | 0.018 | 28 | 1.4 |
| A18 | A_Lower_Durazno | 1.037 | 485 | 53.7 |
| A19 | A_Hardesty_to_Shelter | 0.018 | 33 | 2.1 |

| Diversion | | | | |
|----------------|---------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| D1 | D_Government6_Hills | 4.850 | 348 | 330.2 |
| D2 | D_Boone_St_Basin | 5.682 | 375 | 604.2 |

| Dams and Basins | | | | |
|-----------------|--------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| DB1 | S_McKelligon_Dam | 2.168 | 111 | 70.5 |
| DB2 | S_McKelligon_Reservoir_A | 2.206 | 112 | 68.6 |
| DB3 | S_McKelligon_Reservoir_B | 2.310 | 186 | 80.3 |
| DB4 | S_McKelligon_Reservoir_C | 2.318 | 103 | 73.1 |
| DB5 | S_McKelligon_Reservoir_D | 2.324 | 95 | 73.7 |
| DB6 | S_Cemex_Spillway | 0.923 | 1148 | 106.3 |
| DB7 | S_Van_Buren_Dam | 3.647 | 1206 | 228.9 |
| DB8 | S_Pershing_Dam | 4.716 | 263 | 554.5 |
| DB9 | S_Upper_Durazno | 0.323 | 222 | 30.1 |
| DB10 | S_Lower_Durazno | 1.360 | 0 | 0.0 |

| Junction | | | | |
|----------------|-----------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| J1 | J_McKelligon_Res_A_Inflow | 2.206 | 113 | 74.6 |
| J2 | J_McKelligon_Res_B_Inflow | 2.310 | 197 | 79.7 |
| J3 | J_McKelligon_Res_C_Inflow | 2.318 | 199 | 81.2 |
| J4 | J_McKelligon_Res_D_Inflow | 2.324 | 102 | 73.9 |
| J5 | J_Van_Buren_Ditch_US | 0.923 | 1148 | 106.3 |
| J6 | J_Van_Buren_Ditch_Inflow | 1.044 | 1272 | 119.5 |
| J7 | J_Inflow_Van_Buren_Dam | 3.647 | 1658 | 228.9 |
| J8 | J_Fort_Bliss_Channel_Inflow | 0.000 | 200 | 324.6 |
| J9 | J_Pollard_Ditch_Inflow | 0.113 | 209 | 15.4 |
| J10 | J_Pollard_Sacramento | 0.021 | 52 | 2.8 |
| J11 | J_Pershing_Dam | 4.850 | 448 | 572.6 |
| J12 | J_Inflow_from_Pershing_Dam | 4.850 | 448 | 572.6 |
| J13 | J_Gov_Hills_North_Inflow | 4.850 | 336 | 328.7 |
| J14 | J_Russel_Ditch | 0.434 | 791 | 57.2 |
| J15 | J_Gov_Hills_Central_Inflow | 5.284 | 1098 | 385.8 |
| J16 | J_Gov_Hills_South_Inflow | 5.682 | 1517 | 421.9 |
| J17 | J_24hr-Emergency_Drain | 0.000 | 100 | 242.4 |
| J18 | J_Concordia_Cemetery | 5.834 | 691 | 618.2 |
| J19 | J_Hardesty_to_Shelter | 5.852 | 705 | 619.1 |
| J20 | J_Gov_Hills_Outfall | 5.852 | 687 | 618.5 |
| J21 | J_Lower_Durazno_Out | 1.360 | 0 | 0.0 |

| Reach | | | | |
|----------------|-----------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| R1 | R_McKelligon_Channel | 2.206 | 112 | 68.5 |
| R2 | R_El_Paso_Rock_Quarries | 2.318 | 102 | 73.1 |
| R3 | R_McKelligon_D_Out | 2.324 | 95 | 73.6 |
| R4 | R_Van_Buren_DS | 0.923 | 1128 | 106.4 |
| R5 | R_Mountain_Avenue_Conduit | 3.647 | 1205 | 228.8 |
| R6 | R_FortBliss_Inflow | 0.000 | 200 | 324.6 |
| R7 | R_Pollard_Ditch | 0.113 | 209 | 15.4 |
| R8 | R_Pollard_Sacramento | 0.021 | 47 | 2.8 |
| R9 | R_Gov_Hills_Conduit | 4.850 | 336 | 328.7 |
| R10 | R_Russel_Ditch | 0.434 | 767 | 57.1 |
| R11 | R_24hr-Emergency_Drain | 0.000 | 100 | 241.7 |
| R12 | R_Boone_to_Concordia | 5.682 | 375 | 603.6 |
| R13 | R_Concordia_to_Hardesty | 5.834 | 673 | 617.0 |
| R14 | R_Hardesty_to_Gov_Hills_Out | 5.852 | 687 | 618.5 |

| Source | | | | |
|----------------|--------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| S1 | Source_NE_Input | Not Specified | 200 | 324.6 |

Legend

A1 Basin Areas/Watershed

DB1 Dams/Basins

R1 Reaches

J1 Junctions

S1 Source

D1 Diversions

Connecting Lines

Diversion Dashed Lines

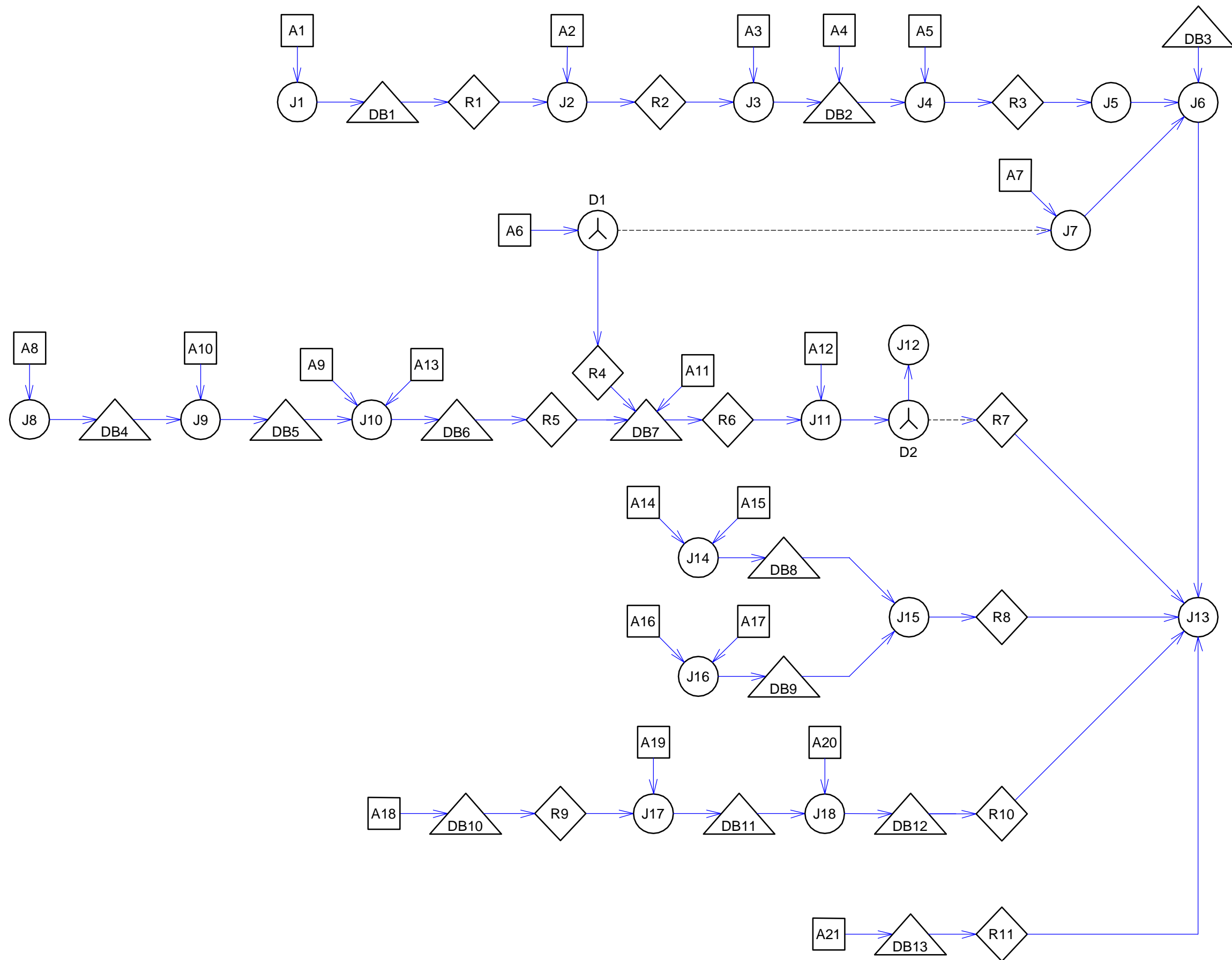
Government Hills System
HEC-HMS Model Table
Central Region

El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-35





Legend

- Basin Areas/Watershed
- Dams/Basins
- Reaches
- Junctions
- Source
- Diversions
- Connecting Lines
- Diversion Dashed Lines

**Cebada System
HEC-HMS Model Layout
Central Region**
El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-36

| Basin | | | | |
|----------------|--------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| A1 | A_Fort_Blvd_Reservoir | 0.219 | 280 | 21.4 |
| A2 | A_Copia_Ditch_US | 0.411 | 670 | 53.2 |
| A3 | A_Copia_Ditch_DS | 0.160 | 320 | 21.4 |
| A4 | A_Memorial_Park | 0.151 | 257 | 18.2 |
| A5 | A_Russet_Ditch_DS | 0.123 | 246 | 15.7 |
| A6 | A_Houston_Elementary | 0.498 | 538 | 62.6 |
| A7 | A_Cebada_Reservoir | 0.699 | 948 | 72.8 |
| A8 | A_San_Diego_Dam | 0.122 | 207 | 12.0 |
| A9 | A_Tremont_Reservoir | 0.005 | 13 | 0.7 |
| A10 | A_Ohio_St_Reservoir | 0.009 | 20 | 1.0 |
| A11 | A_Magnolia_Reservoir | 0.095 | 57 | 3.8 |
| A12 | A_Eucalyptus_to_Cebada | 0.226 | 437 | 32.0 |
| A13 | A_Ohio_St_Reservoir_DS | 0.002 | 0 | 0.0 |
| A14 | A_Louisiana_Dr_Dam_Lower | 0.049 | 118 | 5.8 |
| A15 | A_Louisiana_Dr_Dam_Upper | 0.137 | 231 | 13.8 |
| A16 | A_Memphis_Dam_Lower | 0.015 | 30 | 1.4 |
| A17 | A_Memphis_Dam_Upper | 0.249 | 312 | 23.9 |
| A18 | A_Altura_Ave_Dam | 0.122 | 157 | 11.9 |
| A19 | A_Kentucky_Dam_Upper | 0.057 | 118 | 6.1 |
| A20 | A_Kentucky_Dam_Lower | 0.124 | 140 | 12.3 |
| A21 | A_Scenic_Dr_Dam | 0.126 | 172 | 12.1 |

| Diversion | | | | |
|----------------|--------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| D1 | D_Houston_Elementary | 0.498 | 250 | 49.7 |
| D2 | D_Capacity of 60"Conduit | 0.956 | 568 | 47.4 |

| Dams and Basins | | | | |
|-----------------|-----------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| DB1 | S_Fort_Blvd_Reservoir | 0.219 | 242 | 16.5 |
| DB2 | S_Memorial_Park | 0.941 | 1196 | 110.5 |
| DB3 | S_Cebada_Reservoir | 2.641 | 637 | 325.6 |
| DB4 | S_San_Diego_Dam | 0.122 | 110 | 11.3 |
| DB5 | S_Ohio_St_Reservoir | 0.130 | 97 | 12.3 |
| DB6 | S_Tremont_Reservoir | 0.138 | 54 | 13.0 |
| DB7 | S_Magnolia_Reservoir | 0.731 | 330 | 61.0 |
| DB8 | S_Louisiana_Dam_Lower | 0.186 | 163 | 13.4 |
| DB9 | S_Memphis_Dam_Lower | 0.264 | 308 | 21.0 |
| DB10 | S_Altura_Ave_Dam | 0.122 | 154 | 10.4 |
| DB11 | S_Kentucky_Dam_Upper | 0.179 | 57 | 10.6 |
| DB12 | S_Kentucky_Dam_Lower | 0.303 | 138 | 21.9 |
| DB13 | S_Scenic_Dr_Dam | 0.126 | 43 | 12.0 |

| Junction | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| J1 | J_Inflow_Ft_Blvd_Res | 0.219 | 280 | 21.4 |
| J2 | J_Copia_Ditch_US | 0.630 | 768 | 70.0 |
| J3 | J_Copia_Ditch_DS | 0.790 | 966 | 91.5 |
| J4 | J_Cebada_US | 1.064 | 1393 | 126.1 |
| J5 | J_Cebada_Reservoir_Outfall | 1.064 | 1386 | 126.1 |
| J6 | J_Cebada_Inflow | 2.641 | 3031 | 325.6 |
| J7 | J_Houston_to_Cebada | 0.699 | 1116 | 85.7 |
| J8 | J_Inflow to San Diego Dam | 0.122 | 207 | 12.0 |
| J9 | J_Inflow_Ohio_St_Res | 0.130 | 118 | 12.3 |
| J10 | J_Inflow_Tremont_Reservoir | 0.138 | 99 | 13.0 |
| J11 | J_Eucalyptus_to_Cebada | 0.956 | 668 | 93.0 |
| J12 | J_I-10 Overtopping Flow | 0.956 | 568 | 47.4 |
| J13 | J_Cebada_Total | 0.878 | 732 | 113.8 |
| J14 | J_Inflow_Louisiana_Dam_Lower | 0.186 | 348 | 19.7 |
| J15 | J_Cebada_North | 0.450 | 465 | 34.4 |
| J16 | J_Inflow_Memphis_Dam | 0.264 | 334 | 25.3 |
| J17 | J_Inflow_Kentucky_Dam_Upper | 0.179 | 211 | 16.6 |
| J18 | J_Inflow_Kentucky_Dam_Lower | 0.303 | 140 | 22.8 |

| Reach | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| R1 | R_Fort_Blvd_to_Copia_DitchUS | 0.219 | 241 | 16.8 |
| R2 | R_Copia_Ditch_DS | 0.630 | 751 | 70.0 |
| R3 | R_Cebada_to_Cebada_Reservoir | 1.064 | 1386 | 126.1 |
| R4 | R_Houston_Magnolia | 0.498 | 250 | 49.7 |
| R5 | R_Tremont_to_Magnolia | 0.138 | 54 | 13.0 |
| R6 | R_Magnolia_to_Eucalyptus | 0.731 | 327 | 61.0 |
| R7 | R_Eucalyptus_to_Cebada | 0.000 | 100 | 45.6 |
| R8 | R_Cebada_Reservoir_2 | 0.450 | 457 | 34.3 |
| R9 | R_Altura_to_Kentucky_Upper | 0.122 | 150 | 10.4 |
| R10 | R_Cebada_Reservoir_3 | 0.303 | 137 | 21.9 |
| R11 | R_Cebada_Reservoir_4 | 0.126 | 43 | 12.0 |

Legend

A1 Basin Areas/Watershed

DB1 Dams/Basins

R1 Reaches

J1 Junctions

S1 Source

D1 Diversions

Connecting Lines

Diversion Dashed Lines

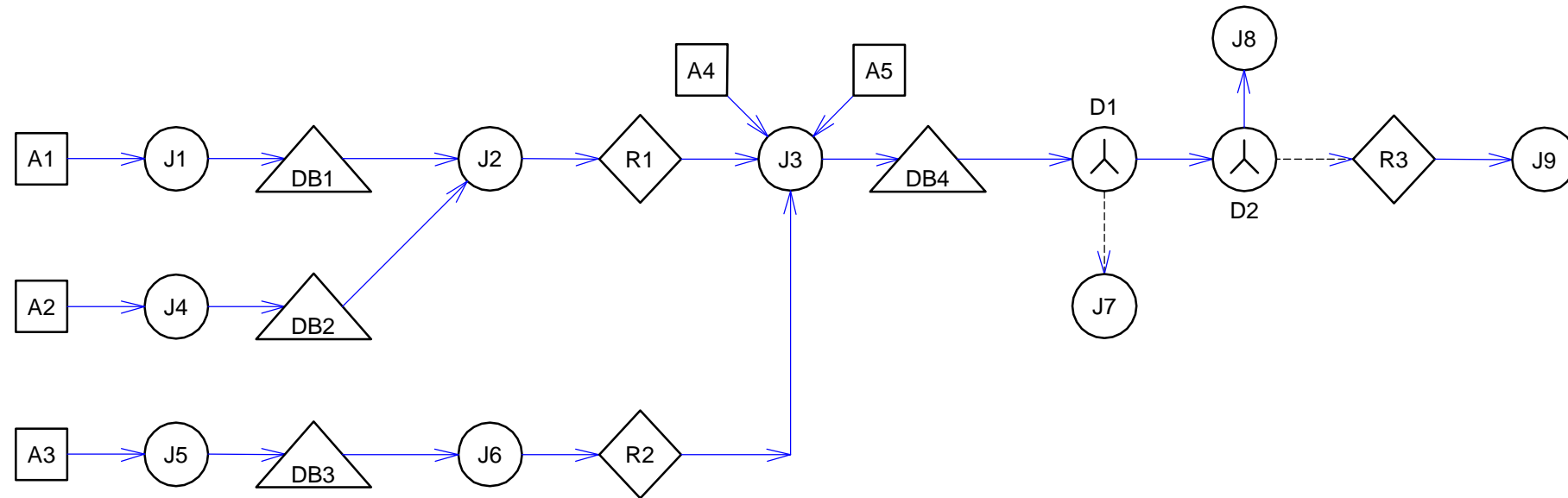
Cebada System
HEC-HMS Model Table
Central Region

El Paso Stormwater Master Plan

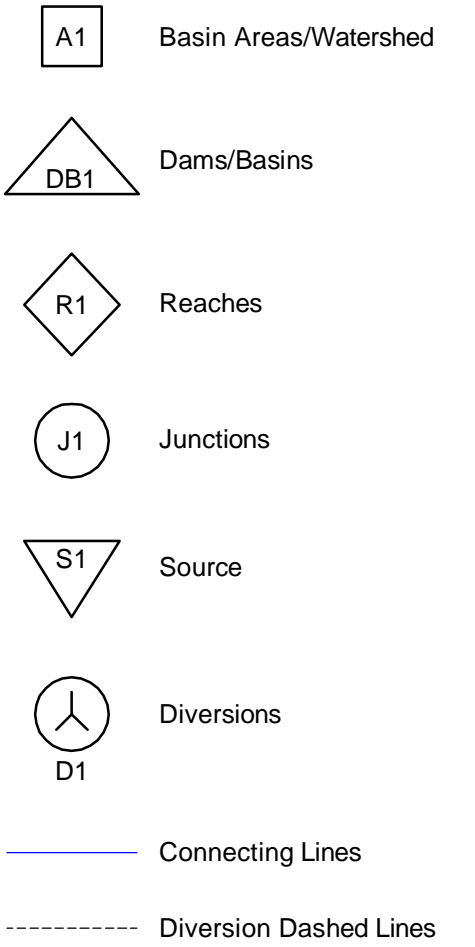
Date: 03/05/2009

Figure A-37





Legend



Dallas System HEC-HMS Model Layout Central Region

El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-38



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| Basin | | | | |
|----------------|--------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| A1 | A_Dam_No_8 | 0.052 | 88 | 4.3 |
| A2 | A_Dam_No_9 | 0.033 | 65 | 3.3 |
| A3 | A_Dam_No_10 | 0.073 | 150 | 6.9 |
| A4 | A_Cotton_Dallas_DS | 0.375 | 670 | 43.3 |
| A5 | A_Cotton_Dallas_US | 1.047 | 1342 | 111.5 |

| Diversion | | | | |
|----------------|--------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| D1 | D_3708 | 1.580 | 530 | 145.4 |
| D2 | D_IH_10_Dallas | 1.580 | 216 | 75.7 |

| Dams and Basins | | | | |
|-----------------|--------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| DB1 | S_Dam_No_8 | 0.052 | 49 | 4.3 |
| DB2 | S_Dam_No_9 | 0.033 | 49 | 3.3 |
| DB3 | S_Dam_No_10 | 0.073 | 0 | 0.0 |
| DB4 | S_Dallas_Reservoir | 1.580 | 690 | 162.4 |

| Junction | | | | |
|----------------|--------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| J1 | J_Inflow_Dam_No_8 | 0.052 | 88 | 4.3 |
| J2 | J_Dam_9_and_8 | 0.085 | 97 | 7.5 |
| J3 | J_Dallas_Reservoir | 1.580 | 1988 | 162.4 |
| J4 | J_Inflow_Dam_No_9 | 0.033 | 65 | 3.3 |
| J5 | J_Inflow_Dam_No_10 | 0.073 | 150 | 6.9 |
| J6 | J_Cotton_Dallas_US | 0.073 | 0 | 0.0 |
| J7 | J_Overflow_3708 | 0.000 | 160 | 16.9 |
| J8 | J_Dallas_West | 1.580 | 216 | 75.7 |
| J9 | J_Diversion | 0.000 | 314 | 69.8 |

| Reach | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| R1 | R_Dam_9_and_8_to_Dallas_Res | 0.085 | 97 | 7.6 |
| R2 | R_CottonDallas_to_Dallas_Res | 0.073 | 0 | 0.0 |
| R3 | R_Dallas_to_Cebada_Connector | 0.000 | 314 | 69.8 |

Legend

A1 Basin Areas/Watershed

DB1 Dams/Basins

R1 Reaches

J1 Junctions

S1 Source

D1 Diversions

Connecting Lines

Diversion Dashed Lines

Dallas System
HEC-HMS Model Table
Central Region

El Paso Stormwater Master Plan

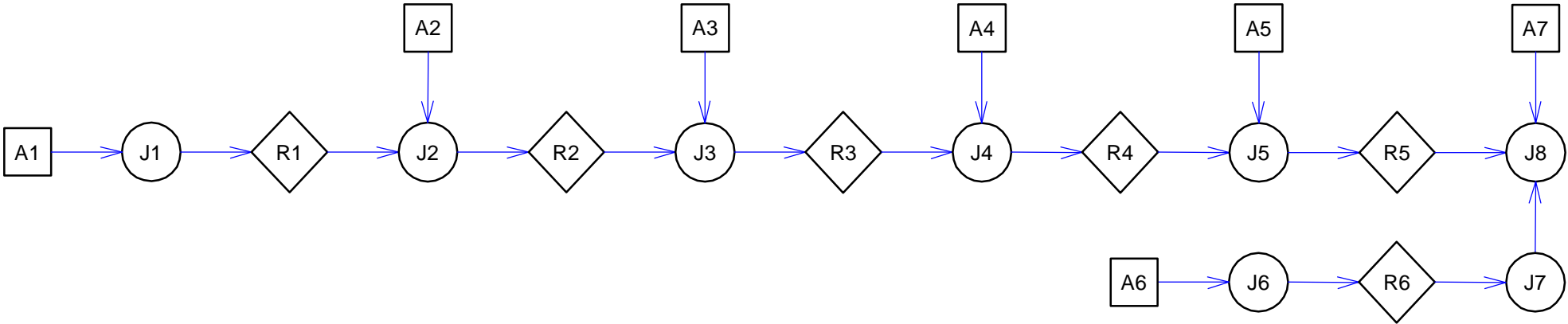
Date: 03/05/2009

Figure A-39

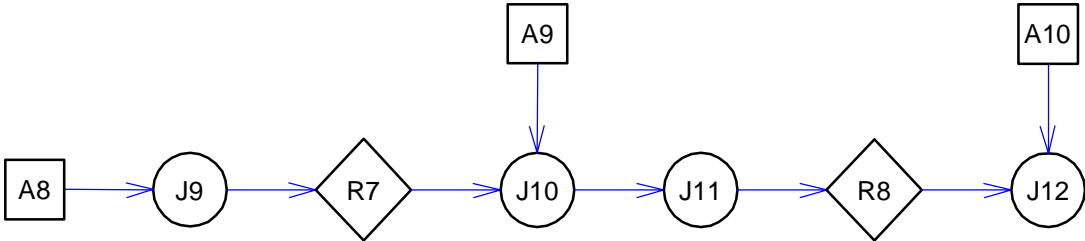


File: Q:\El Paso Master Drainage Plan\Stormwater Master Plan Report\HMS Cad Diagrams\Schematics_App_A_013009.dwg Layout: Fig A-40 User: Scott_Coleman Plotted: Mar 02, 2009 - 10:49am

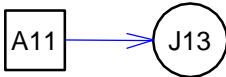
Channel 108 System



Paisano System



Modesto System



Legend

- A1 Basin Areas/Watershed
- DB1 Dams/Basins
- R1 Reaches
- J1 Junctions
- S1 Source
- D1 Diversions
- Connecting Lines
- Diversion Dashed Lines

Modesto, Channel 108, and Paisano Systems
HEC-HMS Model Layout
Central Region
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-40



| Basin | | | | |
|----------------|----------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| A1 | A_Alameda Avenue | 0.299 | 11 | 17.0 |
| A2 | A_Blanco Avenue | 0.087 | 58 | 10.8 |
| A3 | A_Comanche Avenue | 0.136 | 233 | 13.7 |
| A4 | A_Delta Drive | 0.076 | 146 | 6.7 |
| A5 | A_Channel_108_Discharge | 0.031 | 76 | 3.2 |
| A6 | A_Glenwood_Street_48in_RCP | 0.062 | 79 | 3.9 |
| A7 | A_Robert_Alva_Channel | 0.442 | 486 | 32.3 |
| A8 | A_Nixon_Cypress_to_Central | 0.048 | 110 | 5.2 |
| A9 | A_Paisano_Ditch | 0.223 | 347 | 20.2 |
| A10 | A_Cebada_Drainage_Outfall | 0.273 | 341 | 25.7 |
| A11 | A_Modesto Ditch | 0.117 | 218 | 10.1 |

| Junction | | | | |
|----------------|----------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| J1 | J_Alameda Avenue | 0.299 | 11 | 17.0 |
| J2 | J_Blanco Avenue | 0.386 | 59 | 27.8 |
| J3 | J_Comanche Avenue | 0.522 | 249 | 41.5 |
| J4 | J_Delta Drive | 0.599 | 376 | 48.2 |
| J5 | J_Channel 108 | 0.630 | 435 | 51.4 |
| J6 | J_Glenwood_Street_48in_RCP | 0.062 | 79 | 3.9 |
| J7 | J_Outflow from Robert Alva | 0.062 | 75 | 3.9 |
| J8 | J_Robert_Alva_Channel | 1.134 | 971 | 87.5 |
| J9 | J_Nixon_Cypress_to_Central | 0.048 | 110 | 5.2 |
| J10 | J_Paisano_Ditch | 0.271 | 453 | 25.3 |
| J11 | J_Pera | 0.271 | 453 | 25.3 |
| J12 | J_Cebada_Drainage_Outfall | 0.544 | 780 | 51.0 |
| J13 | J_Modesto Ditch | 0.117 | 218 | 10.1 |

| Reach | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| R1 | R_Alameda Avenue | 0.299 | 11 | 16.9 |
| R2 | R_Blanco_to_Comanche | 0.386 | 59 | 27.8 |
| R3 | R_Comanche_to_Delta_Dr | 0.522 | 247 | 41.5 |
| R4 | R_Delta_Dr_to_Channel108_Out | 0.599 | 363 | 48.2 |
| R5 | R_Channel108_to_Robert_Alva | 0.630 | 420 | 51.4 |
| R6 | R_Glenwood_to_Robert_Alva | 0.062 | 75 | 3.9 |
| R7 | R_Paisano_Ditch | 0.048 | 106 | 5.2 |
| R8 | R_Pera_to_Cebada_Outfall | 0.271 | 439 | 25.3 |

Legend

- A1

Basin Areas/Watershed
- DB1

Dams/Basins
- R1

Reaches
- J1

Junctions
- S1

Source
- D1

Diversions
- Connecting Lines
- Diversion Dashed Lines

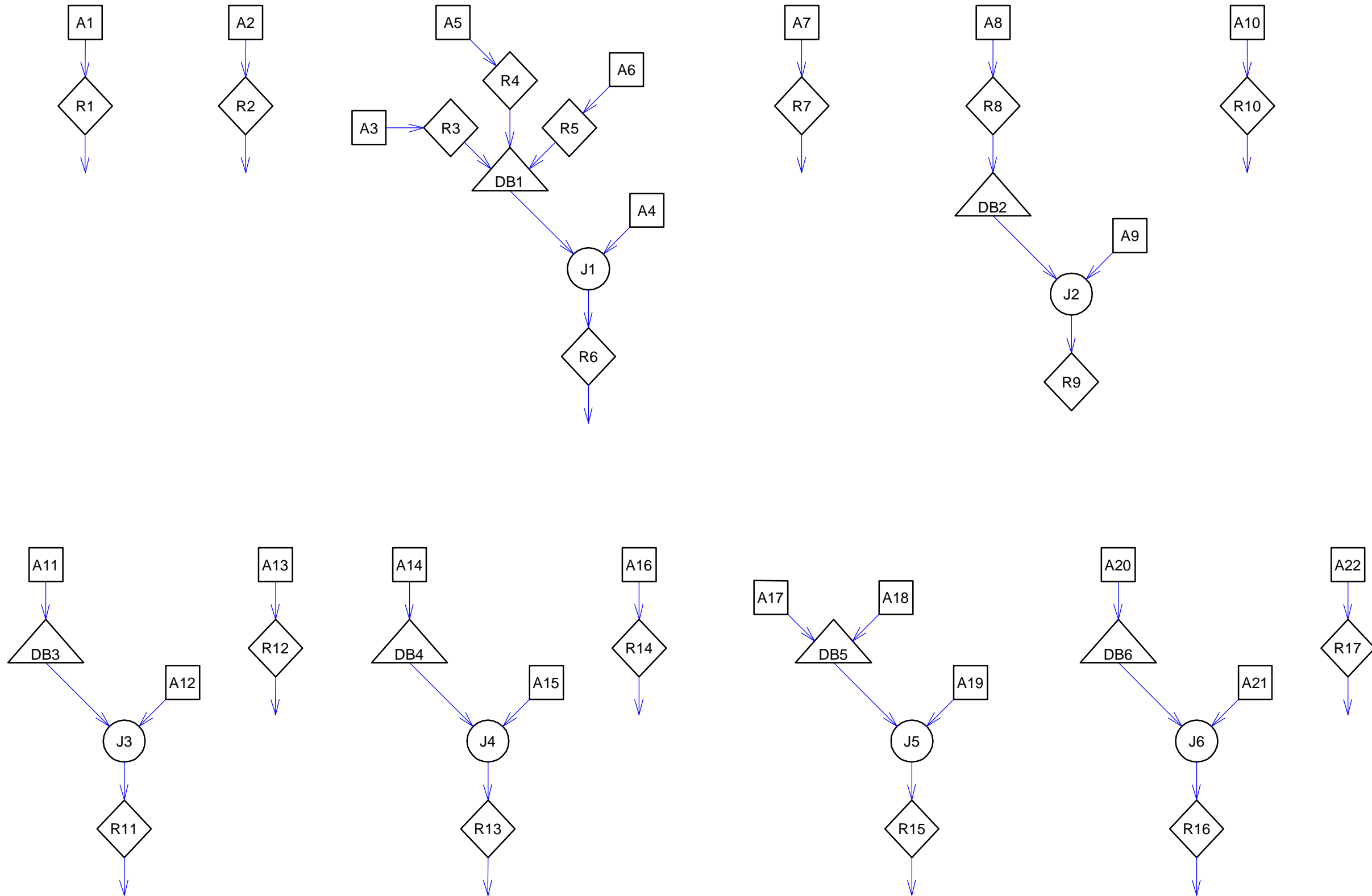
Modesto, Channel 108, and
Paisano Systems
HEC-HMS Model Table
Central Region
El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-41



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Legend

A1 Basin Areas/Watershed

DB1 Dams/Basins

R1 Reaches

J1 Junctions

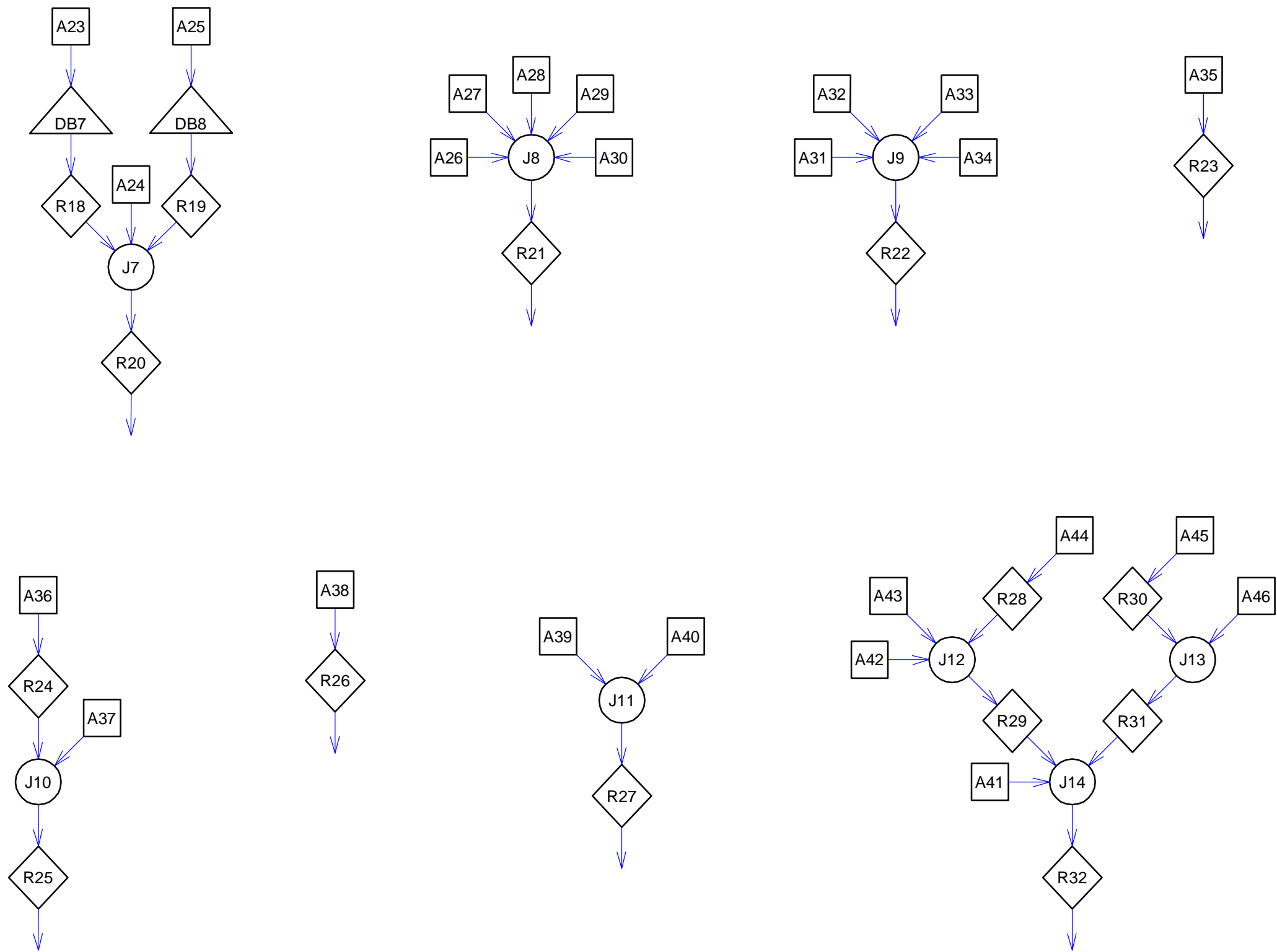
Connecting Lines

HEC-HMS Model Layout East Side Region

El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-42



Legend

- A1 Basin Areas/Watershed
- DB1 Dams/Basins
- R1 Reaches
- J1 Junctions

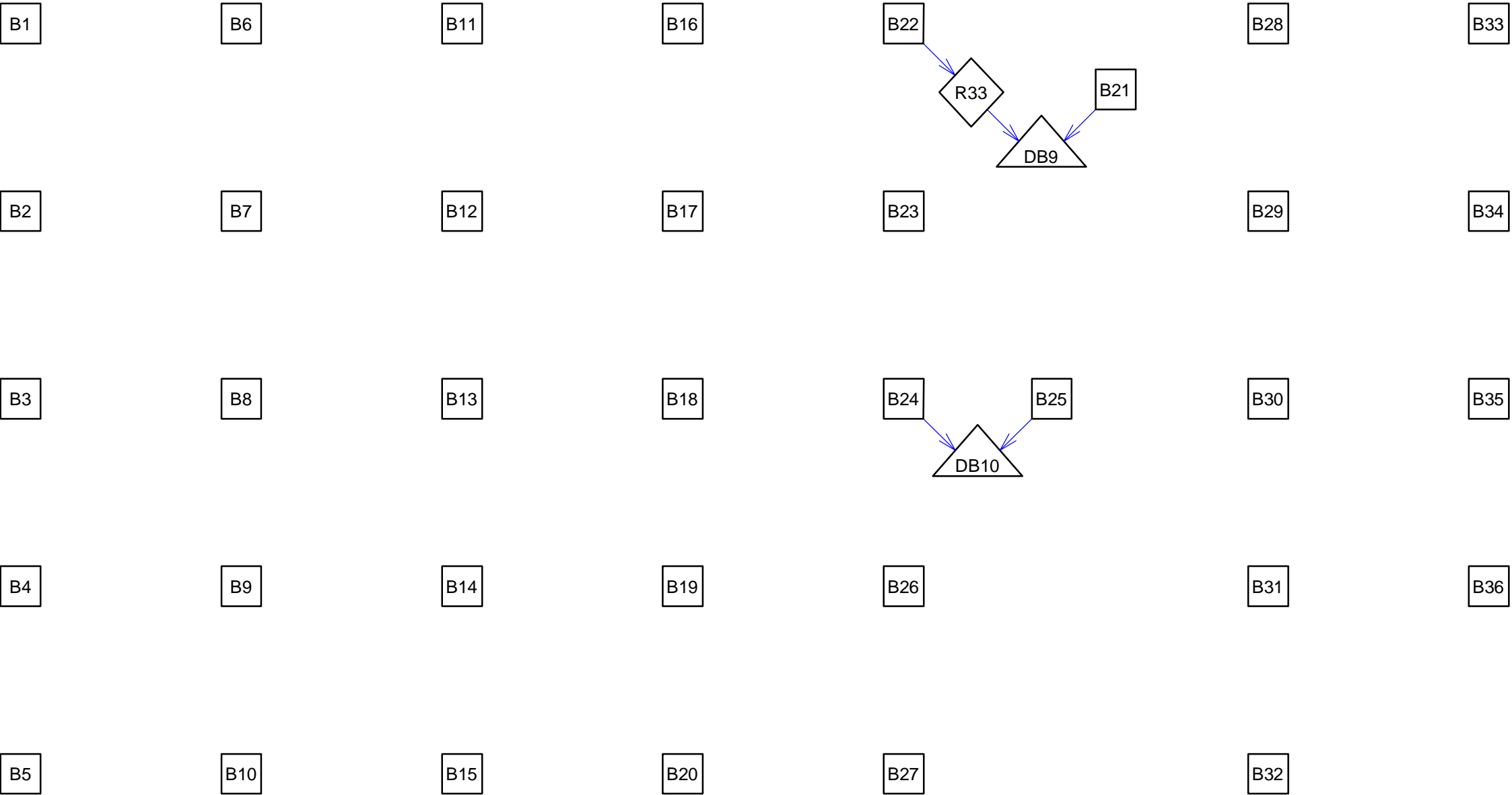
Connecting Lines

HEC-HMS Model Layout
for Referenced Study ★
East Side Region
El Paso Stormwater Master Plan






Date: 03/05/2009 Figure A-43

★ Model XX returned from: Drainage Study and report (existing conditions) for Interstate highway 10, Moreno Cardenas Inc. February 2008.





Legend

-  Basin Areas/Watershed
-  Dams/Basins
-  Reaches
-  Junctions
-  Connecting Lines

High Mesa (Closed Basins)
HEC-HMS Model Layout
East Side Region
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-44



| BASIN | | | | |
|---------------|--------------------|--------------------|----------------|--------------|
| Model XX NAME | HYDROLOGIC ELEMENT | DRAINAGE AREA | PEEK DISCHARGE | VOLUME |
| | | (MI ²) | (CFS) | (ACRE- FEET) |
| A1 | A-PD-1 | 0.7542 | 763.00 | 72.00 |
| A2 | A-PD-1A | 0.1608 | 323.70 | 18.20 |
| A3 | A_SUNMOUNT | 0.2858 | 360.60 | 25.10 |
| A4 | EID-1 | 0.3002 | 381.70 | 51.90 |
| A5 | CVP-1 | 0.1859 | 219.80 | 24.20 |
| A6 | CVP-2 | 0.5040 | 594.60 | 65.60 |
| A7 | EID-2 | 0.1395 | 143.00 | 24.10 |
| A8 | CVP-3 | 0.0630 | 76.70 | 8.20 |
| A9 | RLH-1 | 0.1246 | 100.70 | 16.20 |
| A10 | RLH_2 | 0.0319 | 46.70 | 2.30 |
| A11 | ESTWD1 | 0.6150 | 815.20 | 92.10 |
| A12 | ESTWD2 | 0.6680 | 1929.00 | 104.90 |
| A13 | SLTRHL | 0.4390 | 431.10 | 57.10 |
| A14 | A-CAR DAM-1 | 0.4161 | 189.50 | 14.80 |
| A15 | A_CAR DAM-2 | 0.1015 | 205.50 | 11.90 |
| A16 | A_MESADRAIN_UP | 0.0735 | 142.30 | 8.00 |
| A17 | A-LL-8 | 1.0568 | 626.00 | 51.00 |
| A18 | A-LL-8A | 0.7243 | 596.10 | 50.40 |
| A19 | A-LL-10 | 0.3416 | 686.80 | 38.60 |
| A20 | A-MESA-2 | 0.5021 | 442.80 | 31.70 |
| A21 | A_MESA_3 | 0.2018 | 393.70 | 23.70 |
| A22 | A_MESA_4 | 0.1603 | 145.20 | 10.70 |
| A23 | 9C | 0.444 | 1066.4 | 77.9 |
| A24 | 9A | 0.934 | 1724.5 | 163.7 |
| A25 | 9B | 0.262 | 693.9 | 46 |
| A26 | 29 | 0.0270 | 82.60 | 4.40 |
| A27 | 22 | 0.0440 | 135.30 | 6.80 |
| A28 | 34 | 0.0480 | 145.80 | 7.30 |
| A29 | 46 | 0.1180 | 363.80 | 19.80 |
| A30 | 52 | 0.045 | 138.2 | 7.5 |
| A31 | 58 | 0.009 | 27.5 | 1.4 |
| A32 | 66 | 0.03 | 92.4 | 4.8 |
| A33 | 77 | 0.087 | 267.7 | 13.8 |
| A34 | 83 | 0.044 | 131.4 | 5.5 |
| A35 | 90 | 0.009 | 26.7 | 1 |
| A36 | 96A | 0.05 | 153.5 | 7.4 |
| A37 | 96B | 0.006 | 17.8 | 0.7 |
| A38 | 100 | 0.0490 | 145.40 | 5.70 |
| A39 | 106 | 0.0220 | 67.70 | 3.40 |
| A40 | 110 | 0.0150 | 46.10 | 2.30 |
| A41 | 124F | 0.0160 | 49.20 | 2.40 |
| A42 | 124B | 0.2380 | 605.50 | 40.20 |
| A43 | 124E | 0.0690 | 14.70 | 8.40 |
| A44 | 124A | 0.1990 | 598.60 | 27.50 |
| A45 | 124C | 1.1480 | 1180.90 | 124.10 |
| A46 | 124D | 0.0870 | 127.80 | 10.70 |

| DAMS AND BASINS | | | | |
|-----------------|--------------------|--------------------|----------------|--------------|
| Model XX NAME | HYDROLOGIC ELEMENT | DRAINAGE AREA | PEEK DISCHARGE | VOLUME |
| | | (MI ²) | (CFS) | (ACRE- FEET) |
| DB1 | CVB-A | NOT SPECIFIED | 32.00 | 38.70 |
| DB2 | CVB-B | NOT SPECIFIED | 26.00 | 8.20 |
| DB3 | ED | NOT SPECIFIED | 465.70 | 83.20 |
| DB4 | LAF-B | NOT SPECIFIED | 26.00 | 14.70 |
| DB5 | JESUIT BASIN | NOT SPECIFIED | 22.00 | 22.00 |
| DB6 | PENDALE BASIN | NOT SPECIFIED | 32.00 | 30.90 |
| DB7 | 9C_P | NOT SPECIFIED | 226.2 | 24.3 |
| DB8 | 9B_P | NOT SPECIFIED | 5 | 4.7 |
| DB9 | PETER HURD POND | NOT SPECIFIED | 185.2 | 24.5 |
| DB10 | QUAIL SUB POND | NOT SPECIFIED | 602.3 | 62 |

| JUNCTION | | | | |
|---------------|--------------------|--------------------|----------------|--------------|
| Model XX NAME | HYDROLOGIC ELEMENT | DRAINAGE AREA | PEEK DISCHARGE | VOLUME |
| | | (MI ²) | (CFS) | (ACRE- FEET) |
| J1 | CLB_A_JN | NOT SPECIFIED | 413.70 | 90.60 |
| J2 | CLB_B_JN | NOT SPECIFIED | 126.70 | 24.40 |
| J3 | NODE19 | NOT SPECIFIED | 1948.60 | 188.10 |
| J4 | CARDAM@H-10 | NOT SPECIFIED | 231.50 | 26.60 |
| J5 | LOMALAND@1H-10 | NOT SPECIFIED | 708.80 | 60.60 |
| J6 | MESA-JN | NOT SPECIFIED | 425.70 | 54.60 |
| J7 | 9J | NOT SPECIFIED | 1725.7 | 192.6 |
| J8 | WS-22 | NOT SPECIFIED | 865.6 | 45.7 |
| J9 | WS-77 | NOT SPECIFIED | 519 | 25.6 |
| J10 | 96J | NOT SPECIFIED | 170.6 | 8.1 |
| J11 | WS-110 | NOT SPECIFIED | 113.8 | 5.7 |
| J12 | 124JW | NOT SPECIFIED | 1230.30 | 76.00 |
| J13 | 124JE | NOT SPECIFIED | 1279.10 | 134.60 |
| J14 | JB | NOT SPECIFIED | 1753.8 | 212.7 |

| BASIN | | | | |
|---------------|--------------------|--------------------|----------------|--------------|
| Model XX NAME | HYDROLOGIC ELEMENT | DRAINAGE AREA | PEEK DISCHARGE | VOLUME |
| | | (MI ²) | (CFS) | (ACRE- FEET) |
| B1 | A-PD-2 | 0.148594 | 353.6 | 21.2 |
| B2 | A-PD-3 | 0.185453 | 189.7 | 17 |
| B3 | A-PD-4 | 0.367969 | 251.4 | 24.4 |
| B4 | A-PD-5 | 0.545313 | 577.8 | 54.3 |
| B5 | A-PD-6 | 0.44422 | 476.8 | 38.9 |
| B6 | A-PD-7 | 0.941047 | 1557 | 82.6 |
| B7 | A-PD-8 | 4.475078 | 1889.8 | 368.2 |
| B8 | A-PD-9 | 6.086 | 1509.3 | 490.5 |
| B9 | A-PD-10 | 1.915484 | 865.3 | 158.7 |
| B10 | A-LL-1 | 0.380719 | 616.9 | 34.9 |
| B11 | A-LL-2 | 0.206188 | 234.2 | 12.4 |
| B12 | A-LL-3 | 0.347156 | 372.7 | 22 |
| B13 | A-LL-4 | 2.332031 | 2178.5 | 221.8 |
| B14 | A-LL-5 | 1.092469 | 1471.1 | 104.4 |
| B15 | A-LL-6 | 1.632359 | 2118.5 | 155.8 |
| B16 | A-LL-7 | 0.455859 | 601.5 | 41.8 |
| B17 | A-LL-9 | 1.600547 | 1264.1 | 111.2 |
| B18 | A-AM-1 | 3.529938 | 4480.4 | 307.7 |
| B19 | A-AM-2 | 1.820891 | 1898.1 | 159.2 |
| B20 | A-AM-3 | 0.69725 | 1059.6 | 63.9 |
| B21 | A-AM-4 | 0.161688 | 280.8 | 14.2 |
| B22 | A-AM-5 | 0.480344 | 477.6 | 47.8 |
| B23 | A-AM-6 | 0.143594 | 43.5 | 3.8 |
| B24 | A-AM-7 | 0.105219 | 56.4 | 3.7 |
| B25 | A-AM-8 | 0.260047 | 165.2 | 20.8 |
| B26 | A-AM-9 | 0.2859533 | 165.1 | 13.8 |
| B27 | A-AM-10 | 0.107359 | 143.8 | 8.2 |
| B28 | A-AM-11 | 1.724141 | 987.8 | 78.3 |
| B29 | A-AM-12 | 0.158297 | 163.8 | 13.9 |
| B30 | A-AMTEN-1 | 1.504406 | 1535.9 | 143.4 |
| B31 | A-AMTEN-2 | 1.535656 | 1673.4 | 165.8 |
| B32 | A-AMTEN-3 | 1.262859 | 1544.7 | 115.5 |
| B33 | A-AMTEN-4 | 0.772672 | 1037.6 | 77 |
| B34 | A-AMTEN-5 | 0.821422 | 1690 | 88.2 |
| B35 | A-AMTEN-6 | 3.006453 | 928.9 | 257 |
| B36 | A-AMTEN-7 | 3.861875 | 1570.1 | 332.1 |

| REACH | | | | |
|---------------|--------------------|--------------------|----------------|--------------|
| Model XX NAME | HYDROLOGIC ELEMENT | DRAINAGE AREA | PEEK DISCHARGE | VOLUME |
| | | (MI ²) | (CFS) | (ACRE- FEET) |
| R1 | MV#1 | NOT SPECIFIED | 763.00 | 72.00 |
| R2 | MV#2 | NOT SPECIFIED | 323.70 | 18.20 |
| R3 | SUNMOUNT CHANNEL | NOT SPECIFIED | 356.60 | 24.80 |
| R4 | VCNT-1 | NOT SPECIFIED | 219.70 | 24.20 |
| R5 | VCNT-2 | NOT SPECIFIED | 594.60 | 65.60 |
| R6 | MV#3 | NOT SPECIFIED | 413.70 | 90.50 |
| R7 | MV#4 | NOT SPECIFIED | 143.00 | 24.10 |
| R8 | VCNT-3 | NOT SPECIFIED | 76.60 | 8.20 |
| R9 | MV#5 | NOT SPECIFIED | 126.70 | 24.40 |
| R10 | MV#6 | NOT SPECIFIED | 46.70 | 2.30 |
| R11 | MV#7 | NOT SPECIFIED | 1948.60 | 188.10 |
| R12 | MV#8 | NOT SPECIFIED | 431.10 | 57.10 |
| R13 | MV#9 | NOT SPECIFIED | 231.50 | 26.60 |
| R14 | MV#10 | NOT SPECIFIED | 142.30 | 8.00 |
| R15 | MV#11 | NOT SPECIFIED | 705.90 | 60.50 |
| R16 | MV#12 | NOT SPECIFIED | 425.70 | 54.60 |
| R17 | MV#13 | NOT SPECIFIED | 145.20 | 10.70 |
| R18 | 9CR | NOT SPECIFIED | 226 | 24.2 |
| R19 | 9BR | NOT SPECIFIED | 5 | 4.7 |
| R20 | MV#14 | NOT SPECIFIED | 1724.9 | 192.5 |
| R21 | MV#15 | NOT SPECIFIED | 865.6 | 45.7 |
| R22 | MV#16 | NOT SPECIFIED | 519 | 25.6 |
| R23 | MV#17 | NOT SPECIFIED | 26.5 | 1 |
| R24 | RCP375 | NOT SPECIFIED | 153 | 7.4 |
| R25 | MV#17A | NOT SPECIFIED | 169.4 | 8.1 |
| R26 | MV#18 | NOT SPECIFIED | 144.5 | 5.7 |
| R27 | MV#19 | NOT SPECIFIED | 113.8 | 5.7 |
| R28 | ARROYO WEST | NOT SPECIFIED | 591.9 | 27.4 |
| R29 | ARROYO WEST2 | NOT SPECIFIED | 1196.7 | 75.8 |
| R30 | ARROYO-EAST | NOT SPECIFIED | 1180 | 124 |
| R31 | ARROYO-EAST2 | NOT SPECIFIED | 1278.2 | 134.5 |
| R32 | MV#20 | NOT SPECIFIED | 1753.2 | 212.7 |
| R33 | JOE BATTLE | NOT SPECIFIED | 477.3 | 47.8 |

Legend



Basin Areas/Watershed



Dams/Basins



Reaches



Junctions

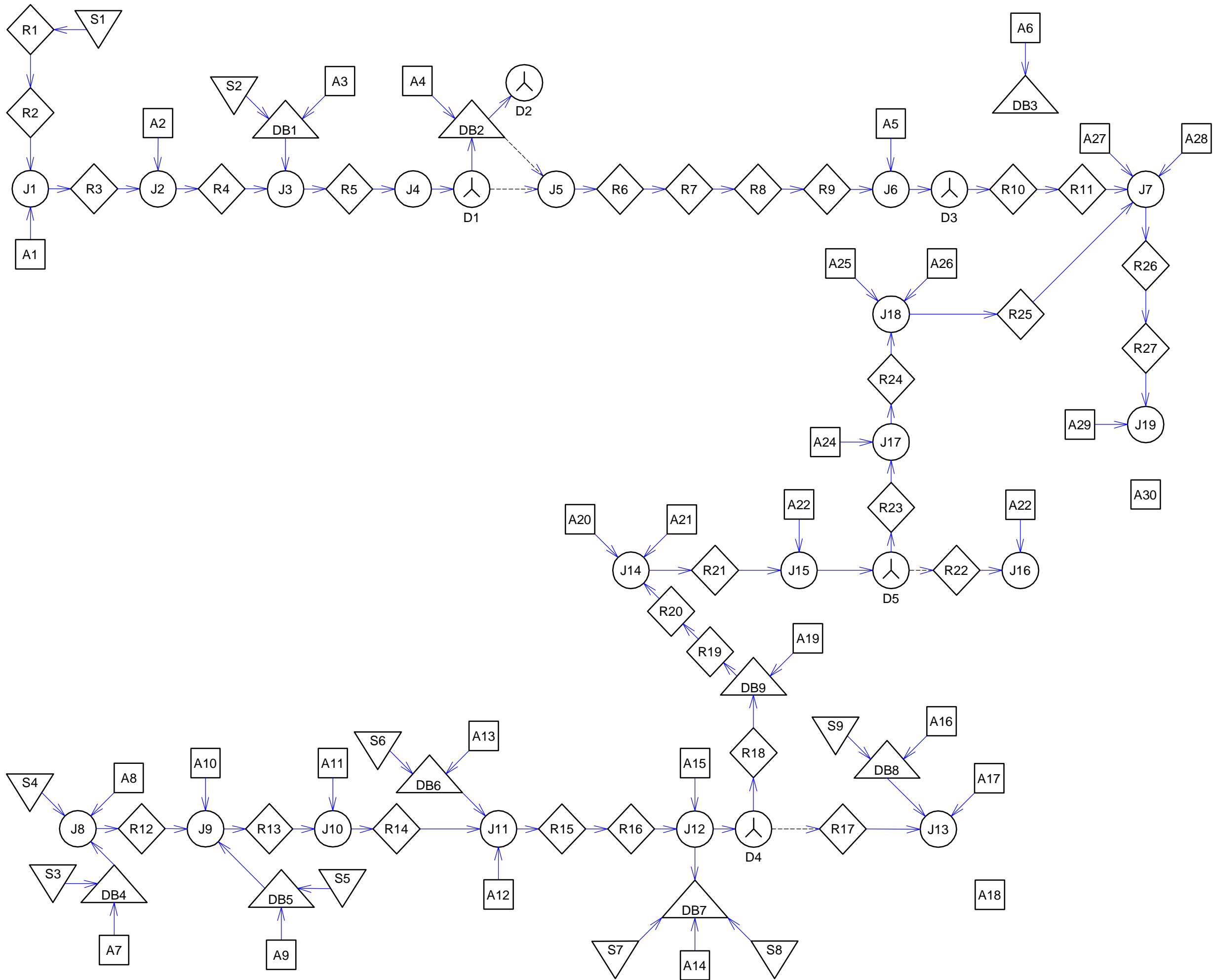
Connecting Lines

High Mesa (Closed Basins)
HEC-HMS Model Table
East Side Region
El Paso Stormwater Master Plan


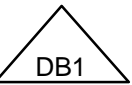






Date: 03/05/2009

Figure A-45





Legend

-  Basin Areas/Watershed
-  Dams/Basins
-  Reaches
-  Junctions
-  Source
-  Diversions
-  Connecting Lines
-  Diversion Dashed Lines

HEC-HMS Model Layout Mission Valley Region

El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-46

| Basin | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| A1 | A_Lincoln Drain | 2.330 | 1364 | 167.2 |
| A2 | A_Playa Drain A | 0.571 | 388 | 43.3 |
| A3 | A_North Loop Detention Basin | 1.129 | 7 | 2.6 |
| A4 | A_Basin A | 1.421 | 644 | 89.3 |
| A5 | A_Playa Drain B | 5.842 | 1014 | 275.9 |
| A6 | A_Basin G | 0.356 | 241 | 38.1 |
| A7 | A_Phelps Dodge Basin | 1.081 | 627 | 58.1 |
| A8 | A_Below Phelps Dodge Basin | 1.386 | 44 | 10.4 |
| A9 | A_Carolina Drive Basin | 0.291 | 0 | 0.0 |
| A10 | A_Mesa Drain A | 0.663 | 0 | 0.0 |
| A11 | A_Below Carolina Dam | 1.024 | 684 | 69.2 |
| A12 | A_Mesa Drain B | 0.740 | 196 | 23.5 |
| A13 | A_Lomaland Basin | 0.663 | 204 | 19.8 |
| A14 | A_Americas Basin | 0.498 | 138 | 25.9 |
| A15 | A_Mesa Drain C | 3.185 | 320 | 66.0 |
| A16 | A_Americas Ten Basin | 0.261 | 25 | 4.6 |
| A17 | A_Mesa Drain to City Limit | 0.803 | 238 | 43.4 |
| A18 | A_Americas Ten NonContribute | 0.085 | 3 | 0.7 |
| A19 | A_Feather Lake Basin | 0.704 | 4 | 1.7 |
| A20 | A_Below Featherlake Basin | 0.153 | 66 | 7.1 |
| A21 | A_Middle Drain A | 4.306 | 807 | 195.7 |
| A22 | A_Middle Drain B | 0.123 | 185 | 13.9 |
| A23 | A_Middle to City Limit | 1.013 | 896 | 81.8 |
| A24 | A_Middle Drain Spur A | 0.055 | 129 | 5.6 |
| A25 | A_Middle Drain Spur B | 0.074 | 143 | 8.1 |
| A26 | A_Franklin Drain A | 0.668 | 691 | 68.8 |
| A27 | A_Franklin Spur Drain | 0.114 | 115 | 9.3 |
| A28 | A_Franklin Drain B | 0.908 | 847 | 74.8 |
| A29 | A_Franklin Drn to City Limit | 2.884 | 523 | 190.5 |
| A30 | A_Below Basin G to Cty Limit | 1.878 | 682 | 151.2 |

| Diversion | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| D1 | D_Basin A 42inch Culvert | Not Specified | 1644 | 277.1 |
| D2 | D_Basin A Pumps | 0.000 | 0 | 0.0 |
| D3 | D_Playa and Playa Intercepto | Not Specified | 2552 | 523.2 |
| D4 | D_Mesa to Mesa Interceptor | Not Specified | 2728 | 1161.8 |
| D5 | D_Middle and Middle Int | Not Specified | 1243 | 1336.1 |


| Dams and Basins | | | | |
|-----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| DB1 | S_North Loop Detention Basin | Not Specified | 55 | 91.9 |
| DB2 | S_Basin A | Not Specified | 1578 | 222.5 |
| DB3 | S_Basin G | 0.356 | 0 | 0.0 |
| DB4 | S_Phelps Dodge Basin | Not Specified | 138 | 260.9 |
| DB5 | S_Carolina Drive Basin | Not Specified | 132 | 65.0 |
| DB6 | S_Lomaland Basin | Not Specified | 110 | 124.0 |
| DB7 | S_Americas Basin | Not Specified | 135 | 348.1 |
| DB8 | S_Americas Ten Basin | Not Specified | 885 | 159.1 |
| DB9 | S_Featherlake Basin | Not Specified | 907 | 1120.5 |

| Junction | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| J1 | J_Lincoln Drain Outlet | Not Specified | 1364 | 167.2 |
| J2 | J_Playa Drain with Conduit | Not Specified | 1744 | 210.5 |
| J3 | J_Playa Drn with North Loop | Not Specified | 1773 | 302.4 |
| J4 | J_Playa Drain w Basin A | Not Specified | 1747 | 302.3 |
| J5 | J_Playa Drain Outlet Basin A | Not Specified | 1672 | 247.7 |
| J6 | J_Playa Drain with Intercept | Not Specified | 2552 | 523.2 |
| J7 | J_Franklin and Franklin Spur | Not Specified | 3733 | 2023.3 |
| J8 | J_Mesa Drain w Phelps Dodge | Not Specified | 1999 | 471.1 |
| J9 | J_Mesa Drain w Carolina Bsn | Not Specified | 1868 | 536.0 |
| J10 | J_Mesa Drain w Lafayette Drw | Not Specified | 2318 | 604.2 |
| J11 | J_Mesa Drain w Lomaland | Not Specified | 2596 | 751.4 |
| J12 | J_Mesa Drain w Americas Bsn | Not Specified | 2728 | 1161.8 |
| J13 | J_Mesa Drain w Americas Ten | Not Specified | 1112 | 202.5 |
| J14 | J_Mesa Int w Middle Drain | Not Specified | 1252 | 1336.7 |
| J15 | J_Middle Drain w Middle Int | Not Specified | 1243 | 1336.1 |
| J16 | J_Middle Drain City Limit | 1.013 | 896 | 81.8 |
| J17 | J_Middle Int w Franklin Canl | Not Specified | 1240 | 1341.3 |
| J18 | J_Middle Int w Franklin Drn | Not Specified | 1311 | 1417.2 |
| J19 | J_Franklin Drain City Limit | Not Specified | 4150 | 2213.3 |


| Reach | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| R1 | R_Lincoln Drain A | Not Specified | 0 | 0.0 |
| R2 | R_Lincoln Drain B | Not Specified | 0 | 0.0 |
| R3 | R_Lincoln to Playa Conduit | Not Specified | 1359 | 167.2 |
| R4 | R_Playa Drain Upper_A | Not Specified | 1720 | 210.4 |
| R5 | R_Playa Drain Upper_B | Not Specified | 1747 | 302.3 |
| R6 | R_Playa Drain Lower_A | Not Specified | 1628 | 247.4 |
| R7 | R_Playa Drain Conduit | Not Specified | 1628 | 247.3 |
| R8 | R_Playa Drain Lower_B | Not Specified | 1591 | 247.4 |
| R9 | R_Playa Drain Lower_C | Not Specified | 1581 | 247.3 |
| R10 | R_Franklin Drain Spur A | Not Specified | 2390 | 522.4 |
| R11 | R_Franklin Drain Spur B | Not Specified | 2341 | 522.4 |
| R12 | R_Mesa Drain above Carolina | Not Specified | 1868 | 471.0 |
| R13 | R_Mesa Drain below Carolina | Not Specified | 1713 | 535.0 |
| R14 | R_Mesa Drain above Lomaland | Not Specified | 2298 | 603.9 |
| R15 | R_Mesa Drain above Amer BsnA | Not Specified | 2359 | 747.9 |
| R16 | R_Mesa Drain above Amer BsnB | Not Specified | 2287 | 747.7 |
| R17 | R_Mesa Drain to City Limit | 0.000 | 0 | 0.0 |
| R18 | R_Mesa Interceptor above FL | Not Specified | 2725 | 1161.5 |
| R19 | R_Mesa Interceptor blw FL A | Not Specified | 905 | 1120.3 |
| R20 | R_Mesa Interceptor blw FL B | Not Specified | 904 | 1120.0 |
| R21 | R_Middle Drain to Intercept | Not Specified | 1243 | 1336.1 |
| R22 | R_Middle Drain to City Limit | 0.000 | 0 | 0.0 |
| R23 | R_Middle Interceptor A | Not Specified | 1237 | 1335.8 |
| R24 | R_Middle Interceptor B | Not Specified | 1234 | 1340.3 |
| R25 | R_Franklin Drain A | Not Specified | 1309 | 1416.8 |
| R26 | R_Franklin Drn to City Lmt A | Not Specified | 3720 | 2023.3 |
| R27 | R_Franklin Drn to City Lmt B | Not Specified | 3711 | 2022.8 |


| Source | | | | |
|----------------|-------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| S1 | Source_CE Input | Not Specified | 0 | 0.0 |
| S2 | Source_MV# 1,2 | Not Specified | 885 | 90.5 |
| S3 | Source_MV# 3,4,5 | Not Specified | 646 | 202.9 |
| S4 | Source_MV#6,7 | Not Specified | 1913 | 199.7 |
| S5 | Source_MV#8,9,10 | Not Specified | 552 | 92.0 |
| S6 | Source_MV#11 | Not Specified | 696 | 104.2 |
| S7 | Source_MV#12,13 | Not Specified | 558 | 66.3 |
| S8 | Source_MV#14, 15,16,17a | Not Specified | 2615 | 286.7 |
| S9 | Source_MV#17a,18,19,20 | Not Specified | 1992 | 233.9 |


Legend

 Basin Areas/Watershed

 Dams/Basins


 Reaches

 Junctions

 Source

 Diversions

 Connecting Lines

 Diversion Dashed Lines

HEC-HMS Model Table
Mission Valley Region

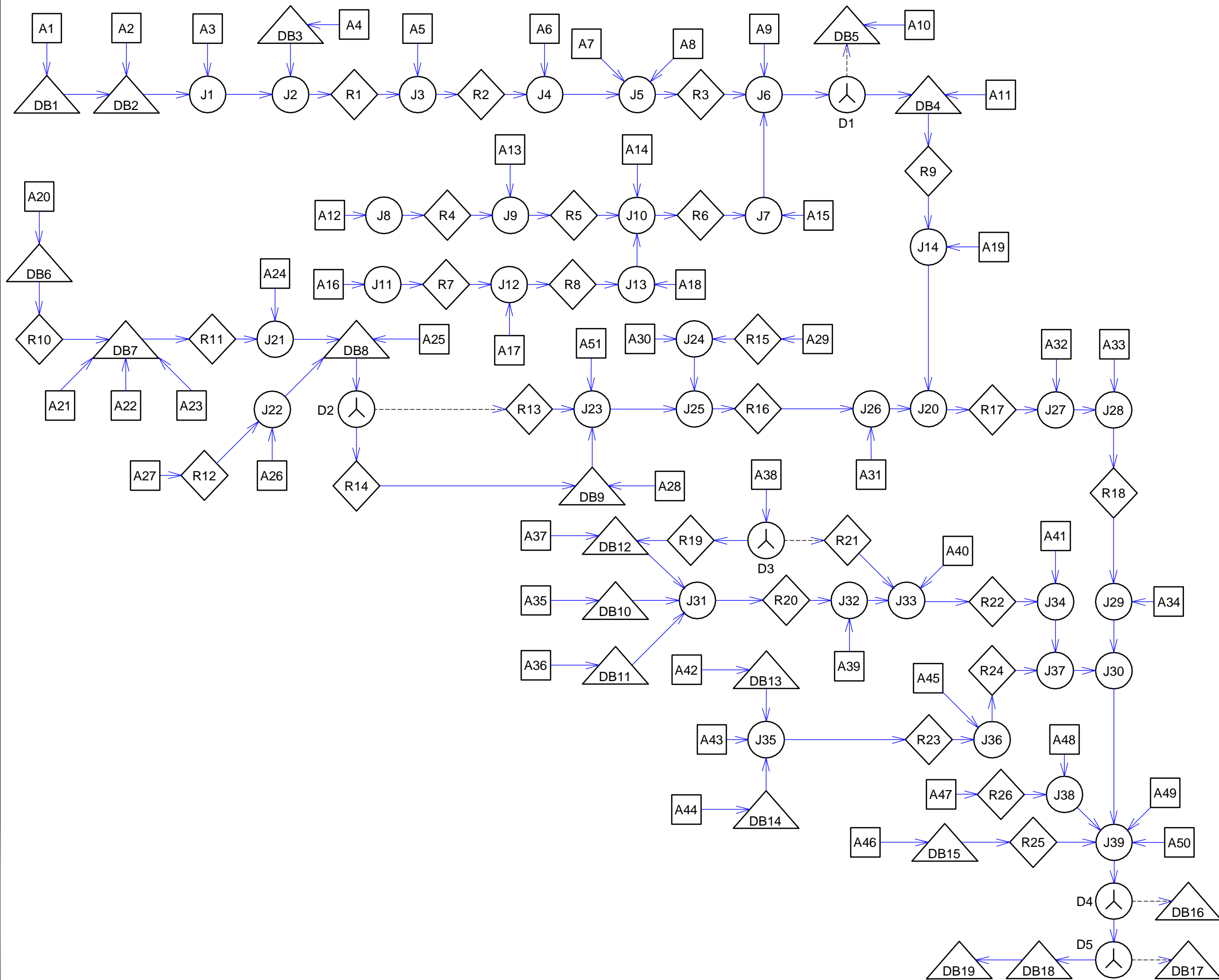
El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-47



File: Q:\El Paso Master Drainage Plan\Stormwater Master Plan Report\HMS Cad Diagrams\Schematics_App_A_013009.dwg Layout: Fig A-48 User: Scott_Coleman Plotted: Mar 02, 2009 - 10:49am



Legend

- A1 Basin Areas/Watershed
- DB1 Dams/Basins
- R1 Reaches
- J1 Junctions
- S1 Source
- D1 Diversions
- Connecting Lines
- Diversion Dashed Lines

HEC-HMS Model Layout Northeast Region

El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-48

| Basin | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| A1 | A_Northhills Dam N | 2.446 | 1555 | 230.2 |
| A2 | A_Northhills Dam S | 3.087 | 1923 | 301.3 |
| A3 | A_War Road Channel | 0.524 | 423 | 34.3 |
| A4 | A_TXDOT Pond | 0.614 | 379 | 48.4 |
| A5 | A_W_Fwy Ch U/S | 1.031 | 378 | 39.6 |
| A6 | A_W_Fwy Ch D/S | 1.336 | 318 | 74.1 |
| A7 | A_E Fwy Channel | 1.674 | 386 | 92.3 |
| A8 | A_Green Belt Levee U/S | 14.301 | 3735 | 1015.4 |
| A9 | A_Green Belt Levee D/S | 0.968 | 288 | 54.8 |
| A10 | A_NE Ponding | 3.133 | 878 | 196.0 |
| A11 | A_NE_Pond Outer | 3.201 | 2584 | 267.3 |
| A12 | A_PSB Ch 1 U/S Gateway | 0.239 | 166 | 18.3 |
| A13 | A_PSB Ch 1 U/S Fannin | 1.798 | 478 | 97.0 |
| A14 | A_PSB Ch 1 U/S PSB2 | 0.701 | 597 | 58.2 |
| A15 | A_PSB Ch 1 D/S | 0.460 | 127 | 15.8 |
| A16 | A_PSB Ch 2 U/S Gateway | 1.371 | 705 | 106.8 |
| A17 | A_PSB Ch 2 U/S Rushing | 0.803 | 509 | 51.0 |
| A18 | A_PSB Ch 2 D/S | 0.992 | 525 | 63.0 |
| A19 | A_Railroad Drain U/S Tobin | 9.876 | 1734 | 698.2 |
| A20 | A_Fusselman Dam | 3.371 | 2283 | 301.4 |
| A21 | A_Northgate Dam | 1.472 | 805 | 101.1 |
| A22 | A_Northgate Int Ch | 0.599 | 127 | 23.5 |
| A23 | A_Northgate Div Ch | 1.293 | 940 | 128.0 |
| A24 | A_Northgate Outlet Channel | 0.472 | 195 | 26.9 |
| A25 | A_Range Dam | 2.210 | 1066 | 186.4 |
| A26 | A_Electric Ditch | 0.626 | 519 | 54.6 |
| A27 | A_Fairbanks Drive | 1.114 | 558 | 94.1 |
| A28 | A_Range Basin | 0.391 | 373 | 28.5 |
| A29 | A_Tobin Drain U/S Irvin H | 2.190 | 1120 | 132.4 |
| A30 | A_Tobin Drain at U/S Army | 0.501 | 677 | 49.9 |
| A31 | A_Tobin Drain U/S RR Drain | 0.503 | 348 | 33.2 |
| A32 | A_Railroad Drain U/S Statler | 0.152 | 56 | 8.8 |
| A33 | A_Statler Ditch | 0.448 | 283 | 31.8 |
| A34 | A_Railroad Drain D/S | 0.053 | 12 | 1.5 |
| A35 | A_Amber Basin | 0.248 | 404 | 26.7 |
| A36 | A_Sunrise Basin | 0.135 | 204 | 14.5 |
| A37 | A_Hondo Pass Basin | 0.079 | 130 | 8.8 |
| A38 | A_Hondo Pass Ch | 0.047 | 67 | 4.5 |
| A39 | A_Sunrise Channel | 0.318 | 299 | 31.5 |
| A40 | A_Diana Ditch US Sunrise Ch | 0.960 | 891 | 79.8 |
| A41 | A_Diana Ditch DS Sunrise Ch | 1.859 | 1420 | 166.8 |
| A42 | A_Mtn Park Dam | 0.806 | 749 | 84.1 |
| A43 | A_Fort Bliss Div Ch U/S | 0.154 | 242 | 16.3 |
| A44 | A_Sunrise Dam | 0.499 | 510 | 52.0 |
| A45 | A_Fort Bliss Div Ch | 0.166 | 282 | 18.7 |
| A46 | A_Keltner Dam | 0.486 | 572 | 52.3 |
| A47 | A_Bossworth U/S | 0.417 | 408 | 43.7 |
| A48 | A_Bossworth D/S | 0.120 | 139 | 13.3 |
| A49 | A_Johnson Channel | 0.075 | 135 | 9.5 |
| A50 | A_Fort Bliss Div Ch D/S | 24.625 | 17154 | 2185.5 |
| A51 | A_Army Ditch | 0.423 | 359 | 31.7 |

| Diversion | | | | |
|----------------|--------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| D1 | D_NE Ponding | 32.347 | 0 | 0.0 |
| D2 | D_Range Dam | 11.157 | 0 | 0.0 |
| D3 | D_Hondo Pass | 0.047 | 67 | 4.5 |
| D4 | D_Ft Bliss Outflow | 92.239 | 22557 | 3436.4 |
| D5 | D_Ft Bliss Sump | 92.239 | 437 | 65.3 |

| Dams and Basins | | | | |
|-----------------|-----------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| DB1 | S_Northhills Dam N | 2.446 | 69 | 118.1 |
| DB2 | S_Northhills Dam S | 5.533 | 74 | 143.3 |
| DB3 | TXDOT Pond | 0.614 | 340 | 48.4 |
| DB4 | S_NE Pond Outer | 35.548 | 0 | 0.0 |
| DB5 | S_NE Ponding | 3.133 | 7376 | 2096.6 |
| DB6 | S_Fusselman Dam | 3.371 | 66 | 125.2 |
| DB7 | S_Northgate Dam | 6.735 | 81 | 98.5 |
| DB8 | S_Range Dam | 11.157 | 15 | 8.3 |
| DB9 | S_Range Basin | 11.549 | 1 | 1.6 |
| DB10 | S_Amber Basin | 0.248 | 8 | 14.0 |
| DB11 | S_Sunrise Basin | 0.135 | 4 | 6.9 |
| DB12 | S_Hondo Pass Basin | 0.127 | 3 | 4.4 |
| DB13 | S_Mtn Park Dam | 0.806 | 168 | 47.9 |
| DB14 | S_Sunrise Dam | 0.499 | 173 | 39.4 |
| DB15 | S_Keltner Dam | 0.486 | 97 | 49.6 |
| DB16 | S_Pershing Dam | 0.000 | 200 | 285.0 |
| DB17 | S_Ft Bliss Sump | 0.000 | 22557 | 3371.0 |
| DB18 | S_Ft Bliss Outer Sump | 92.239 | 0 | 0.0 |
| DB19 | Sink - Gov Hill Ch | 92.239 | 0 | 0.0 |

| Junction | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| J1 | J_War Road Channel | 6.058 | 445 | 177.7 |
| J2 | J_W_Fwy Ch @ War Road | 6.672 | 671 | 226.0 |
| J3 | J_W_Fwy Ch U/S | 7.703 | 902 | 262.0 |
| J4 | J_W_Fwy D/S | 9.039 | 1175 | 333.6 |
| J5 | J_Green Belt Levee | 25.014 | 5109 | 1441.2 |
| J6 | J_Green Belt Levee D/S | 32.347 | 6576 | 1900.7 |
| J7 | J_PSB Ch 1 D/S | 6.365 | 2317 | 409.9 |
| J8 | J_PSB Ch1 Jct1 | 0.239 | 166 | 18.3 |
| J9 | J_PSB Ch1 Jct2 | 2.037 | 602 | 115.3 |
| J10 | J_PSB Ch1 Jct3 | 5.905 | 2227 | 394.1 |
| J11 | J_PSB Ch 2 at Gateway | 1.371 | 705 | 106.8 |
| J12 | J_PSB Ch 2 at Rushing | 2.175 | 966 | 157.6 |
| J13 | J_PSB Ch 2 D/S | 3.167 | 1337 | 220.7 |
| J14 | J_RR Drain U/S of Tobin | 45.424 | 1734 | 698.2 |
| J20 | J_RR and Tobin Drain | 60.590 | 2252 | 953.5 |
| J21 | J_Northgate Dam Out | 7.207 | 195 | 123.7 |
| J22 | J_Electric Ditch | 1.740 | 836 | 148.7 |
| J23 | J_Army Ditch | 11.972 | 359 | 40.6 |
| J24 | J_Tobin Drain U/S Army Ditch | 2.691 | 1422 | 181.9 |
| J25 | J_Tobin Drain at Army Ditch | 14.663 | 1720 | 222.5 |
| J26 | J_Tobin Drain D/S | 15.166 | 2003 | 256.3 |
| J27 | J_RR Dr U/S Statler Ch | 60.742 | 2296 | 962.0 |
| J28 | J_RR Ditch at Statler Ditch | 61.190 | 2542 | 993.8 |
| J29 | J_RR Ditch Downstream | 61.243 | 2516 | 994.6 |
| J30 | J_Ft Bliss Sump Upper | 66.515 | 5065 | 1419.8 |
| J31 | J_Sunrise Ch U/S | 0.510 | 14 | 25.4 |
| J32 | J_Sunrise Ch D/S | 0.828 | 308 | 56.7 |
| J33 | J_Diana Ditch U/S | 1.788 | 1193 | 136.4 |
| J34 | J_Diana Ditch D/S | 3.647 | 2563 | 303.0 |
| J35 | J_Ft Bliss Div Ch U/S | 1.459 | 357 | 103.7 |
| J36 | J_Ft Bliss Div Ch Dyer St | 1.624 | 447 | 122.3 |
| J37 | J_Diana Ditch and FB Div | 5.272 | 3009 | 425.2 |
| J38 | J_Bossworth Ch D/S | 0.538 | 531 | 57.1 |
| J39 | J_Ft Bliss Sump | 92.239 | 22757 | 3721.4 |

| Reach | | | | |
|----------------|------------------------------|-------------------------------------|-------------------------|-----------------------|
| Schematic Name | Hydrologic Element | Drainage Area (mi ²) | Peak Discharge (cfs) | Volume (acre-feet) |
| R1 | R_W_Fwy Ch U/S | 6.672 | 657 | 222.4 |
| R2 | R_W_Fwy Ch D/S | 7.703 | 891 | 259.5 |
| R3 | R_Green Belt Levee | 25.014 | 5099 | 1436.0 |
| R4 | R_PSB Ch1 a | 0.239 | 166 | 18.3 |
| R5 | R_PSB Ch 1 b | 2.037 | 602 | 115.3 |
| R6 | R_PSB Ch 1 c | 5.905 | 2226 | 394.1 |
| R7 | R_PSB Ch 2 a | 1.371 | 695 | 106.6 |
| R8 | R_PSB Ch 2 b | 2.175 | 966 | 157.6 |
| R9 | R_NE Pond Overflow | 35.548 | 0 | 0.0 |
| R10 | R_Fusselman Out | 3.371 | 66 | 123.2 |
| R11 | R_Northgate Dam Out | 6.735 | 81 | 96.7 |
| R12 | R_Electric Ditch | 1.114 | 556 | 94.1 |
| R13 | R_Army Ditch | 0.000 | 14 | 7.2 |
| R14 | R_Range Dam Overflow | 11.157 | 0 | 0.0 |
| R15 | R_Tobin Drain U/S Army Ditch | 2.190 | 1085 | 132.0 |
| R16 | R_Tobin Drain U/S RR Drain | 14.663 | 1708 | 222.1 |
| R17 | R_RR Dr U/S Statler Ch | 60.590 | 2242 | 953.1 |
| R18 | R_RR Dr D/S | 61.190 | 2507 | 993.1 |
| R19 | R_Hondo Pass Channel | 0.047 | 67 | 4.5 |
| R20 | R_Sunrise Channel | 0.510 | 14 | 25.2 |
| R21 | R_Hondo Pass Diversion | 0.000 | 0 | 0.0 |
| R22 | R_Diana Ditch | 1.788 | 1145 | 136.2 |
| R23 | R_Ft Bliss Div Ch U/S | 1.459 | 357 | 103.6 |
| R24 | R_Ft Bliss Div Ch D/S | 1.624 | 447 | 122.2 |
| R25 | R_Keltner Dam Out | 0.486 | 97 | 49.6 |
| R26 | R_Bossworth U/S | 0.417 | 408 | 43.7 |

Legend

- A1

Basin Areas/Watershed
- DB1

Dams/Basins
- R1

Reaches
- J1

Junctions
- S1

Source
- D1

Diversions
- Connecting Lines
- Diversion Dashed Lines

HEC-HMS Model Table
Northeast Region

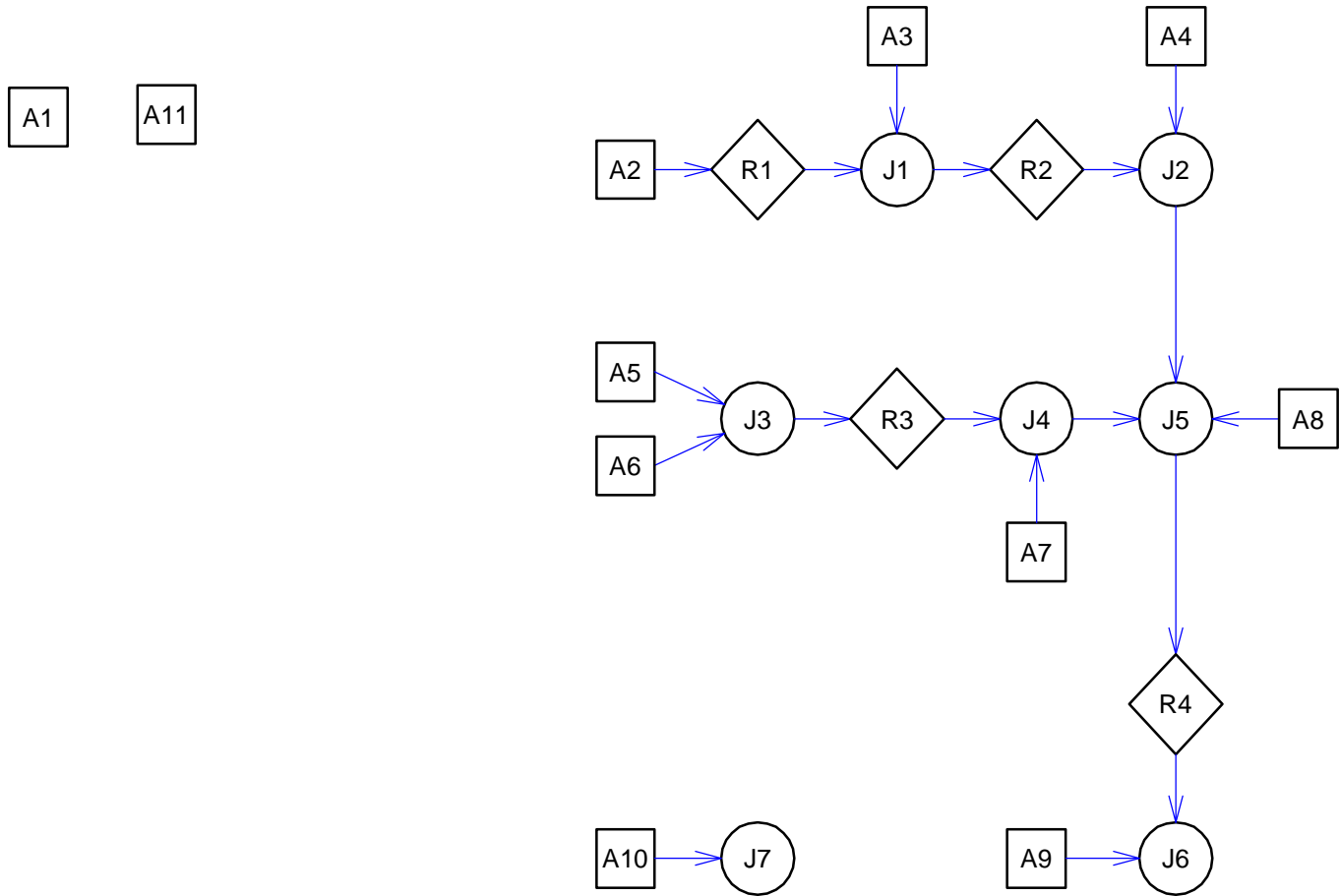
El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-49



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| Symbol | Name | Description | Area (mi ²) | Peak Discharge (cfs) | Volume (ac-ft) |
|--------|--------------|---|----------------------------|-------------------------|-------------------|
| A1 | WRG | West of Rio Grande Basin | 14.5600 | 3366 | 880.96 |
| A2 | M1(A1_2) | Mace_1 (Arroyo 1_2) Basin | 0.1580 | 0 | 0.01 |
| A3 | MD_3 | Montoya Drain_3 Basin | 3.3300 | 1049 | 294.44 |
| A4 | MD_2 | Montoya Drain_2 Basin | 1.4300 | 817 | 86.52 |
| A5 | DD_3 | Doniphan Ditch_3 Basin | 0.1560 | 408 | 22.55 |
| A6 | WSD_2 | White Spur Drain_2 Basin | 0.2070 | 620 | 34.12 |
| A7 | WSD_1 | White Spur Drain_1 Basin | 0.0840 | 155 | 9.10 |
| A8 | NeD1 | Nemexas Drain Basin | 1.2900 | 643 | 119.00 |
| A9 | MD_1 | Montoya Drain_1Basin | 1.3570 | 640 | 176.82 |
| A10 | DD_1 | Doniphan Ditch_1 Basin | 1.5300 | 968 | 178.81 |
| A11 | WM | West Montoya Basin | 1.4609 | 973 | 158.27 |
| J1 | M1 DS | Junction of Montoya Drain_3 Basin and Mace_1 Reach | 3.4880 | 1049 | 294.45 |
| J2 | MD_2,C2 | Junction of Montoya Drain_2 Basin and Montoya Drain_2 Reach | 4.9180 | 1090 | 380.20 |
| J3 | DD3,WSD2 | Junction of Doniphan Ditch_3 Basin and White Spur Drain_2 Basin | 0.3630 | 1029 | 56.66 |
| J4 | WSD_1,WSD1_1 | Junction of White Spur Drain_1 Basin and White Spur Drain 1_1 Reach | 0.4470 | 907 | 65.49 |
| J5 | MD2,WSD1 | Junction of Montoya Drain_2 Basin and White Spur Drain_1 Basin | 6.6550 | 2155 | 564.69 |
| J6 | MD_OUT | Montoya Drain Outlet | 8.0120 | 959 | 751.52 |
| J7 | DD_OUT | Doniphan Ditch Outlet | 1.5300 | 968 | 178.81 |
| R1 | A1 | Mace_1 Reach | 0.1580 | 0 | 0.01 |
| R2 | MD2 | Montoya Drain_2 Reach | 3.4880 | 1018 | 293.68 |
| R3 | WSD_1_1 | White Spur Drain 1_1 Reach | 0.3630 | 832 | 56.39 |
| R4 | MD_C | Montoya Drain_C Reach | 6.6550 | 618 | 574.70 |

Legend

- Basin Areas/Watershed
- Dams/Basins
- Reaches
- Junctions
- Source
- Diversions
- Connecting Lines
- Diversion Dashed Lines

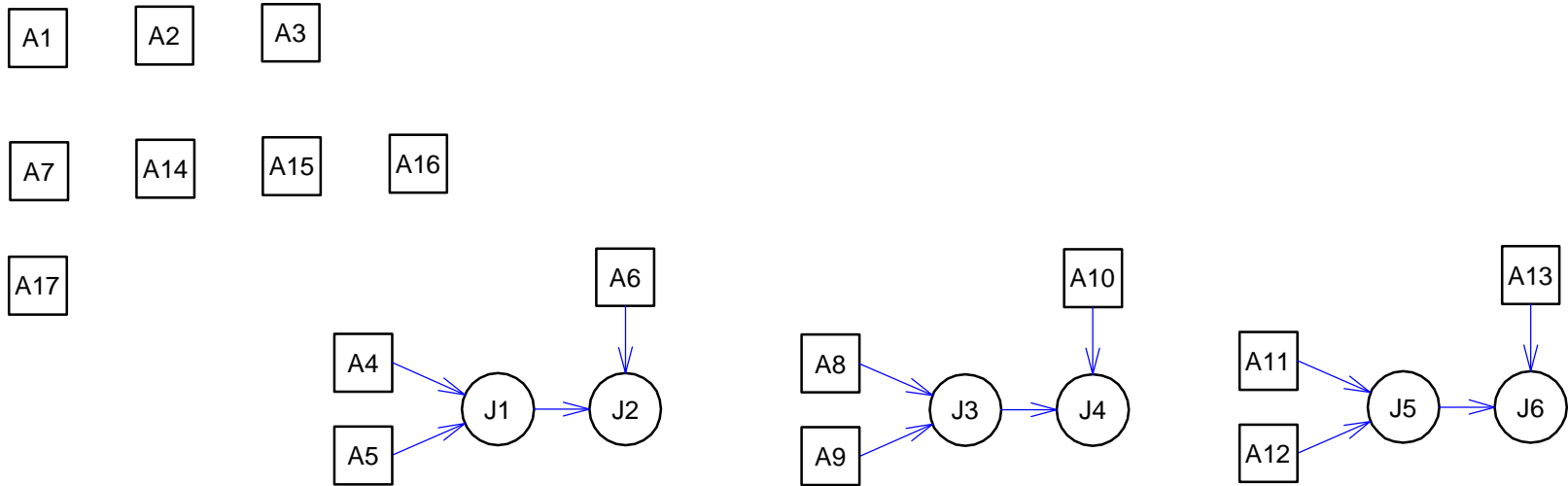
Doniphan & Montoya Drain Systems HEC-HMS Model Layout and Table Northwest Region

El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-50



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| Symbol | Name | Description | Area (mi²) | Peak Discharge (cfs) | Volume (ac-ft) |
|--------|----------------|--|------------|----------------------|----------------|
| A1 | FPN43 | Flow Path Number 43 Basin | 1.1163 | 1090 | 150.64 |
| A2 | UN23A | Unnamed Stream 23A Basin | 0.0294 | 71 | 3.97 |
| A3 | UN024_1 | Unknown 24_1 Basin | 0.0742 | 133 | 10.01 |
| A4 | FPN42T1_2 | Flow Path Number 42 Tributary 1_2 Basin | 0.4390 | 462 | 59.25 |
| A5 | UN01 | Unknown 1 Basin | 0.2391 | 335 | 32.27 |
| A6 | FPN42T1_1 | Flow Path Number 42 Tributary 1_1 Basin | 0.1108 | 273 | 14.96 |
| A7 | FPN42A | Flow Path Number 42A Basin | 0.1068 | 197 | 14.41 |
| A8 | UN03 | Unknown 3 Basin | 0.1561 | 238 | 21.07 |
| A9 | UN02_2 | Unknown 2_2 Basin | 0.0339 | 78 | 4.58 |
| A10 | UN02_1 | Unknown 2_1 Basin | 0.4972 | 94 | 6.71 |
| A11 | UN24A2 | Unnamed Stream 24A_2 Basin | 0.0661 | 113 | 8.92 |
| A12 | UN24AT1 | Unnamed Stream 24A Tributary 1 Basin | 0.0289 | 70 | 3.91 |
| A13 | UN24A1 | Unnamed Stream 24A_1 Basin | 0.0960 | 202 | 12.95 |
| A14 | UN24B | Unnamed Stream 24B Basin | 0.1930 | 290 | 26.05 |
| A15 | UN24C | Unnamed Stream 24C Basin | 0.0561 | 138 | 7.84 |
| A16 | UN24D | Unnamed Stream 24D Basin | 0.0205 | 54 | 2.96 |
| A17 | FPN42 | Flow Path Number 42 Basin | 1.2002 | 937 | 161.97 |
| J1 | UN01,FPN42T1_2 | Junction of Unknown 1 Basin and Flow Path Number 42 Tributary 1_2 Basin | 0.6782 | 797 | 91.52 |
| J2 | FPN42T1_1OUT | Flow Path Number 42 Tributary 1_1 Outlet | 0.7890 | 851 | 106.48 |
| J3 | UN03,02_2 | Junction of Unknown 3 Basin and Unknown 2_2 Basin | 0.1901 | 302 | 25.65 |
| J4 | UN02_1OUT | Unknown 2_1 Outlet | 0.2398 | 395 | 32.36 |
| J5 | UN24A2,T1 | Junction of Unnamed Stream 24A_2 Basin and Unknown 24A Tributary 1 Basin | 0.0951 | 183 | 12.83 |
| J6 | UN24A1OUT | Unnamed Stream 24A_1 Outlet | 0.1910 | 385 | 25.78 |

Legend

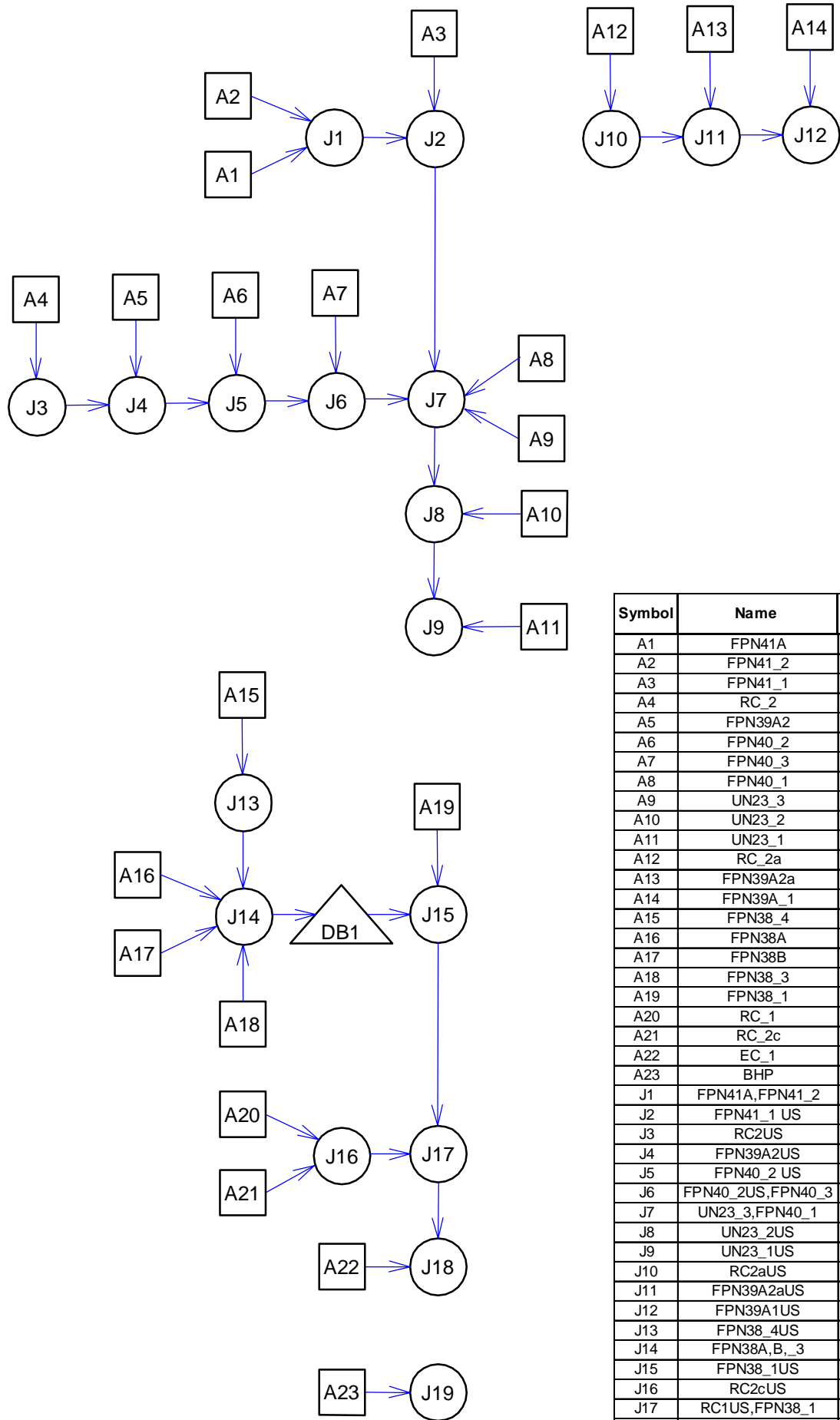
- Basin Areas/Watershed
- Dams/Basins
- Reaches
- Junctions
- Source
- Diversion
- Connecting Lines
- Diversion Dashed Lines

Enchanted Hills System
HEC-HMS Model Layout
and Table
Northwest Region
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-51



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Legend

A1 Basin Areas/Watershed

DB1 Dams/Basins

R1 Reaches

J1 Junctions

S1 Source

D1 Diversions

Connecting Lines

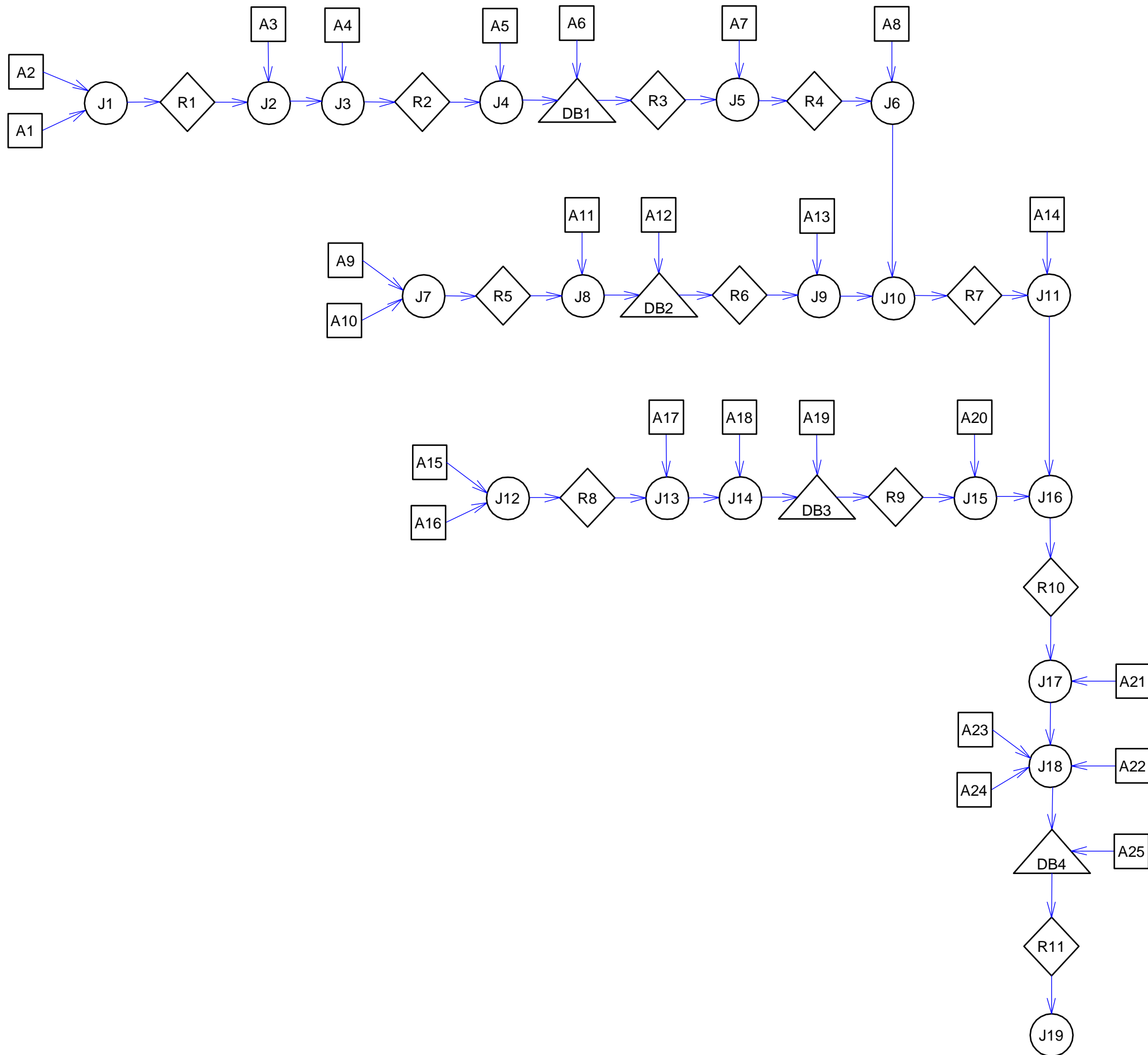
Diversion Dashed Lines

Flow Paths System HEC-HMS Model Layout and Table Northwest Region El Paso Stormwater Master Plan

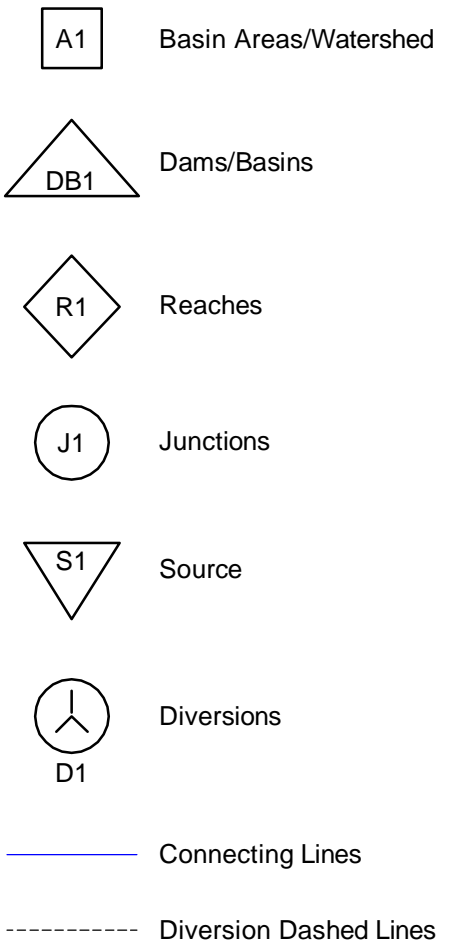
Date: 03/05/2009

Figure A-52





Legend



Keystone Dam System HEC-HMS Model Layout Northwest Region

El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-53



| Symbol | Name | Description | Area (mi ²) | Peak Discharge (cfs) | Volume (ac-ft) |
|--------|-----------------|---|----------------------------|-------------------------|-------------------|
| A1 | A1A | Arroyo 1A Basin | 1.0420 | 1291 | 140.62 |
| A2 | HR_3 | High Ridge_3 Basin | 0.2880 | 429 | 38.87 |
| A3 | HR_2 | High Ridge_2 Basin | 0.3870 | 960 | 55.93 |
| A4 | RV_1 | Ridge View_1 Basin | 1.3000 | 1285 | 181.60 |
| A5 | HR_1 | High Ridge_1 Basin | 0.5420 | 1319 | 73.14 |
| A6 | MD1 | Mulberry Dam 1 Basin | 0.4120 | 972 | 61.58 |
| A7 | MBDO_1 | Mulberry Dam Outlet_1 Basin | 0.2520 | 11 | 1.77 |
| A8 | BLC_3 | Borderland Channel_3 Basin | 0.2950 | 391 | 23.89 |
| A9 | VS_1 | Via Serena_1 Basin | 0.6970 | 977 | 94.06 |
| A10 | ODA_2 | Ojo De Agua_2 Basin | 0.5220 | 785 | 70.45 |
| A11 | ODA_1 | Ojo De Agua_1 Basin | 1.2920 | 2161 | 174.36 |
| A12 | ThoD1 | Thorn Dam_1 Basin | 0.4590 | 1109 | 61.94 |
| A13 | TDO_1 | Thorn Dam Outlet_1 Basin | 0.0690 | 47 | 3.13 |
| A14 | BLC_2 | Borderland Channel_2 Basin | 0.2250 | 500 | 28.29 |
| A15 | GC_1 | Granero Channel_1 Basin | 0.3370 | 915 | 50.37 |
| A16 | BC_2 | Bandolero Channel_2 Basin | 0.8640 | 1087 | 90.03 |
| A17 | BC_1 | Bandolero Channel_1 Basin | 0.3820 | 777 | 55.21 |
| A18 | BDC_1 | Belvidere Channel_1 Basin | 0.9855 | 1449 | 123.92 |
| A19 | MeD1 | Mesa Dam_1 Basin | 0.3140 | 714 | 40.91 |
| A20 | MDO_1 | Mesa Dam Outlet_1 Basin | 0.0360 | 85 | 4.69 |
| A21 | BLC_1 | Borderland Channel_1 Basin | 0.2140 | 689 | 37.57 |
| A22 | A4_1 | Arroyo 4_1 Basin | 0.9700 | 1141 | 105.09 |
| A23 | A5_1 | Arroyo 5_1 Basin | 0.7870 | 1519 | 117.62 |
| A24 | HDC_1 | Highway Diversion Channel_1 Basin | 0.9930 | 2184 | 153.39 |
| A25 | KD1 | Keystone Dam_1 Basin | 0.1430 | 114 | 14.90 |
| J1 | A1A,HR3 | Junction of Arroyo_1A Basin and High Ridge_3 Basin | 1.3300 | 1719 | 179.49 |
| J2 | HR_2,C2 | Junction of High Ridge_2 Basin and High Ridge_C2 Reach | 1.7170 | 2187 | 235.97 |
| J3 | RV1,HR2 | Junction of Ridge View_1 Basin and High Ridge_2 Basin | 3.0170 | 3240 | 417.57 |
| J4 | HR1,LDE1 | Junction of High Ridge_1 Basin and High Ridge_C1 Reach | 3.5590 | 3950 | 491.55 |
| J5 | MD1,MBDO_1 | Junction of Mulberry Dam_1 Basin and Mulberry Dam Outlet_1 Basin | 4.2230 | 205 | 472.98 |
| J6 | BLC_3,C3 | Junction of Borderland Channel_3 Basin and Borderland Channel_C3 Reach | 4.5180 | 482 | 496.06 |
| J7 | VS1,ODA2 | Junction of Via Serena_1 Basin and Ojo de Agua_2 Basin | 1.2190 | 1762 | 164.51 |
| J8 | ER1,ODA1 | Junction of Ojo de Agua_1 Basin and Ojo de Agua_C1 Reach | 2.5110 | 3412 | 339.29 |
| J9 | TDO_1,C | Junction of Thorn Dam Outlet_1 Basin and Thorn Dam Outlet_C Reach | 3.0390 | 155 | 335.55 |
| J10 | BLC3,TDO1 | Junction of Borderland Channel_3 Basin and Thorn Dam Outlet_1 Basin | 7.5570 | 595 | 831.61 |
| J11 | BLC_2,C2 | Junction of Borderland Channel_2 Basin and Borderland Channel_C2 Reach | 7.7820 | 956 | 857.73 |
| J12 | GC1,BC2 | Junction of Granero Channel_1 Basin and Bandolero Channel_2 Basin | 1.2010 | 2002 | 140.39 |
| J13 | BC_1,C1 | Junction of Bandolero Channel_1 Basin and Bandolero Channel_C1 Reach | 1.5830 | 2687 | 196.24 |
| J14 | Before Mesa Dam | Junction of Belvidere Channel_1 Basin and outflow of Junction BC_1, C1 | 2.5685 | 4136 | 320.15 |
| J15 | MDO_1,C | Junction of Mesa Dam Outlet_1 Basin and Mesa Dam Outlet_C Reach | 2.9185 | 207 | 311.19 |
| J16 | BLC2,MDO1 | Junction of Borderland Channel_2 Basin and outflow of Junction MDO_1,C | 10.7005 | 1162 | 1168.91 |
| J17 | BLC2,BLC1 | Junction of Borderland Channel_1 Basin and Borderland Channel_C1 Reach | 10.9145 | 1701 | 1205.54 |
| J18 | BeforeKD1 | Junction of Arroyo4_1 Basin, Arroyo5_1 Basin, and Highway Diversion Channel_1 Basin | 13.6645 | 6544 | 1581.64 |
| J19 | KD_Out | Keystone Dam outlet conduit with Rio Grande | 13.8075 | 534 | 1168.61 |
| R1 | HR_C2 | High Ridge C2 Reach | 1.3300 | 1667 | 180.03 |
| R2 | HR_C1 | High Ridge C1 Reach | 3.0170 | 3194 | 418.41 |
| R3 | MBDO_C1 | Mulberry Dam Outlet_C1 Reach | 3.9710 | 204 | 471.21 |
| R4 | BLC_C3 | Borderland Channel_C3 Reach | 4.2230 | 205 | 472.16 |
| R5 | ODA_C1 | Ojo De Agua_C1 Reach | 1.2190 | 1676 | 164.93 |
| R6 | TDO_C | Thorn Dam Outlet_C Reach | 2.9700 | 154 | 332.42 |
| R7 | BLC_C2 | Borderland Channel_C2 Reach | 7.5570 | 521 | 829.44 |
| R8 | BC_C1 | Bandolero Channel_C1 Reach | 1.2010 | 1910 | 196.24 |
| R9 | MDO_C | Mesa Dam Outlet_C Reach | 2.8825 | 196 | 306.50 |
| R10 | BLC_C1 | Borderland Channel_C1 Reach | 10.7005 | 1012 | 1167.97 |
| R11 | KD_C | Keystone Dam_C Reach | 13.8075 | 534 | 1168.61 |
| DB1 | MD1 Dam | Mulberry Dam | 3.9710 | 204 | 471.67 |
| DB2 | Thorn Dam | Thorn Dam | 2.9700 | 154 | 332.95 |
| DB3 | Mesa Dam | Mesa Dam | 2.8825 | 196 | 306.53 |
| DB4 | KD1 Dam | Keystone Dam | 13.8075 | 534 | 1174.91 |

Legend

- A1

Basin Areas/Watershed
- DB1

Dams/Basins
- R1

Reaches
- J1

Junctions
- S1

Source
- D1

Diversions
- Connecting Lines
- Diversion Dashed Lines

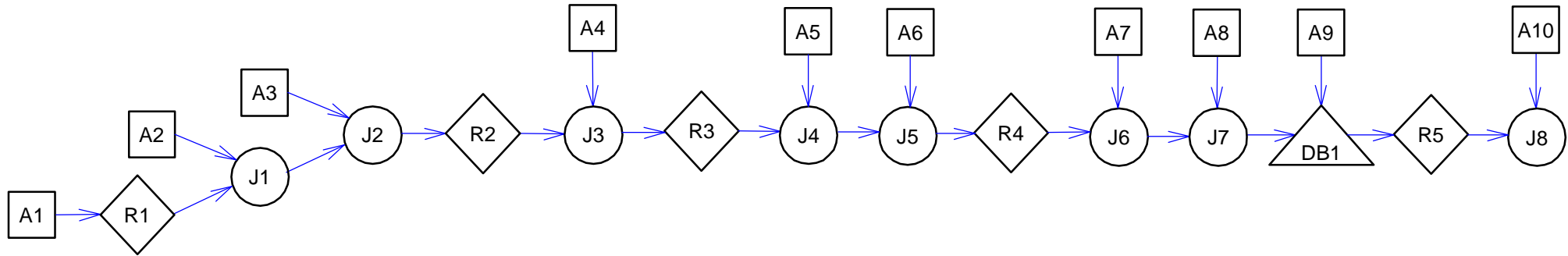
Keystone Dam System
HEC-HMS Model Table
Northwest Region

El Paso Stormwater Master Plan

Date: 03/05/2009

Figure A-54





| Symbol | Name | Description | Area (mi ²) | Peak Discharge (cfs) | Volume (ac-ft) |
|--------|--------------|---|----------------------------|-------------------------|-------------------|
| A1 | SSC_2 | Silver Springs Channel_2 Basin | 0.7370 | 1594 | 99.46 |
| A2 | SSC_1 | Silver Springs Channel_1 Basin | 0.6400 | 868 | 89.40 |
| A3 | SCC_1 | Spring Crest Channel_1 Basin | 0.3210 | 809 | 44.84 |
| A4 | CC_1 | Coronado Channel_1 Basin | 0.1560 | 412 | 26.54 |
| A5 | BVC_2 | Buena Vista Channel_2 Basin | 0.7080 | 1334 | 105.81 |
| A6 | TBV_1 | Thunderbird Valley_1 Basin | 0.8860 | 1359 | 115.45 |
| A7 | BVC_1 | Buena Vista Channel_1 Basin | 0.0160 | 31 | 2.39 |
| A8 | MHC_2 | Mesa Hills Channel_2 Basin | 1.0670 | 2411 | 164.83 |
| A9 | OD | Oxidation Dam Basin | 0.2440 | 667 | 36.47 |
| A10 | OO_1 | Oxidation Outlet_1 Basin | 0.1890 | 244 | 23.76 |
| J1 | SSC_C1,SSC_1 | Junction of Silver Springs Channel_1 Reach and Silver Springs Channel_1 Basin | 1.3770 | 2148 | 189.14 |
| J2 | SCC_1,SSC_1 | Junction of Spring Crest Channel_1 Basin and Silver Springs Channel_1 Basin | 1.6980 | 2957 | 233.98 |
| J3 | CC | Junction of Coronado Channel_1 Basin and Coronado Channel Reach | 1.8540 | 3153 | 261.47 |
| J4 | BVC_2,C2 | Junction of Buena Vista Channel_2 Basin and Buena Vista Channel_2 Reach | 2.5620 | 4328 | 368.34 |
| J5 | BVC2,TBV1 | Junction of Thunderbird Valley_1 Basin and outflow of Junction BVC_2,C2 | 3.4480 | 5687 | 483.79 |
| J6 | BVC_1,C1 | Junction of Buena Vista Channel_1 Basin and Buena Vista Channel_1 Reach | 3.4640 | 5555 | 487.20 |
| J7 | BVC1,MHC2 | Junction of Mesa Hills Channel_2 Basin and outflow of Junction BVC_1,C1 | 4.5310 | 7966 | 652.03 |
| J8 | Ox_Out | Oxidation Dam Outlet | 4.9640 | 398 | 430.38 |
| R1 | SSC_C1 | Silver Springs Channel_1 Reach | 0.7370 | 1470 | 99.73 |
| R2 | CC_C | Coronado Channel Reach | 1.6980 | 2741 | 234.93 |
| R3 | BVC_C2 | Buena Vista Channel_2 Reach | 1.8540 | 2994 | 262.53 |
| R4 | BVC_C1 | Buena Vista Channel_1 Reach | 3.4480 | 5524 | 484.81 |
| R5 | OD_C | Oxidation Dam Reach | 4.7750 | 173 | 406.61 |
| DB1 | OD Dam | Oxidation Dam | 4.7750 | 173 | 407.29 |

Legend

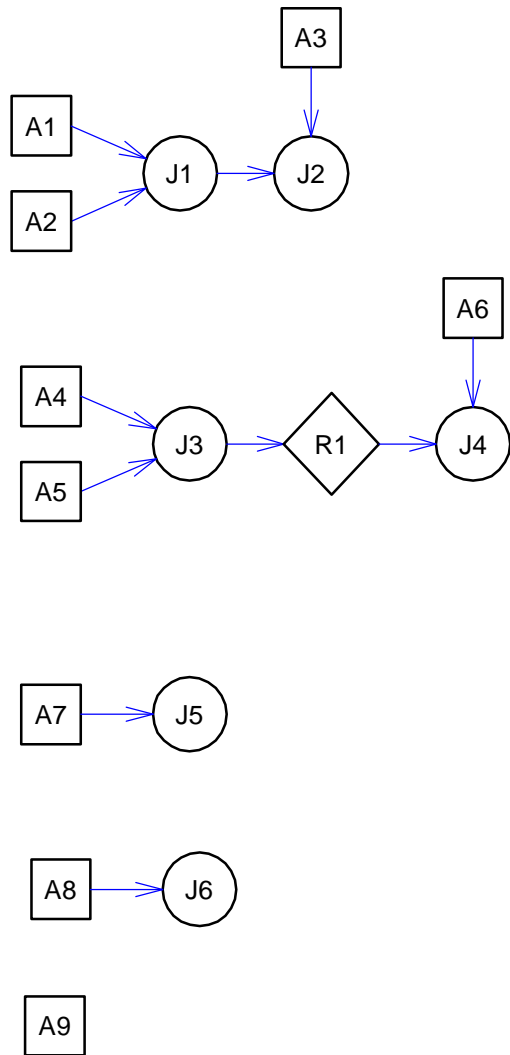
- Basin Areas/Watershed
- Dams/Basins
- Reaches
- Junctions
- Source
- Diversion
- Connecting Lines
- Diversion Dashed Lines

Oxidation Dam System
HEC-HMS Model Layout
and Table
Northwest Region
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-55



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| Symbol | Name | Description | Area (mi ²) | Peak Discharge (cfs) | Volume (ac-ft) |
|--------|-------------|--|-------------------------|----------------------|----------------|
| A1 | PC_1 | Paragon Channel_1 Basin | 1.5489 | 2975 | 239.27 |
| A2 | FPN20_2 | Flow Path Number 20_2 Basin | 1.3208 | 2949 | 197.39 |
| A3 | FPN20_1 | Flow Path Number 20_1 Basin | 0.2074 | 394 | 33.10 |
| A4 | CBC_1 | Canterbury Channel_1 Basin | 0.8860 | 1009 | 132.42 |
| A5 | FPN21_2 | Flow Path Number 21_2 Basin | 1.4140 | 2293 | 171.46 |
| A6 | FPN21_1 | Flow Path Number 21_1 Basin | 0.2440 | 735 | 40.21 |
| A7 | FPN23_1 | Flow Path Number 23_1 Basin | 1.8498 | 3319 | 285.74 |
| A8 | Bcanal | Border Canal Basin | 0.7974 | 1066 | 135.66 |
| A9 | Ind_1 | Industrial_1 Basin | 1.3751 | 1974 | 198.74 |
| J1 | PC1,FPN20_2 | Junction of Paragon Channel_1 Basin and Flow Path Number 20_2 Basin | 2.8696 | 5924 | 436.66 |
| J2 | FPN20_1US | Flow Path Number 20_1 Outlet | 3.0770 | 6318 | 469.75 |
| J3 | CBC1,FPN21 | Junction of Canterbury Channel_1 Basin and Flow Path Number 21_2 Basin | 2.3000 | 2908 | 303.88 |
| J4 | FPN21_OUT | Flow Path Number 21 Outlet | 2.5440 | 3434 | 345.14 |
| J5 | FPN23_US | Flow Path Number 23 Outlet | 1.8498 | 3319 | 285.74 |
| J6 | BCanalUS | Border Canal Outlet | 0.7974 | 1066 | 135.66 |
| R1 | FPN21_C1 | Flow Path Number 21_C1 Reach | 2.3000 | 2700 | 304.93 |

Legend

- Basin Areas/Watershed
- Dams/Basins
- Reaches
- Junctions
- Source
- Diversion
- Connecting Lines
- Diversion Dashed Lines

West Central System
HEC-HMS Model Layout
and Table
West Central Region
El Paso Stormwater Master Plan

Date: 03/05/2009 Figure A-56

